# **NOTICE**

All drawings located at the end of the document.





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Report for the
903 Drum
Storage Area,
903 Lip Area, and
Americium Zone

RF/RMRS-99-427.UN Rev. 0



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Characterization Report for the 903 Drum Storage Area, 903 Lip Area, and Americium Zone

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### **ACRONYMS**

ALF Action Levels & Standards Framework for Surface Water, Groundwater & Soil

Am Americium

bgs below ground surface

C Carbon

CCL<sub>4</sub> Carbon Tetrachloride

CDH Colorado Department of Health

CDPHE Colorado Department of Health and Environment

CERCLA Comprehensive Environmental Response, Compensation and Liability Act

cm centimeter

cpm counts per minute

COC Contaminant of Concern

CRQL Contract Required Quantitation Limit

1,2-DCE 1,2-Cis-Dichloroethylene DER Duplicate Error Ratio

DNAPL Dense Nonaqueous Phase Liquid
DOE U. S. Department of Energy
DOT Department of Transportation
DQA Data Quality Assessment

DOO Data Quality Assessment DOO

EPA Environmental Protection Agency

Eq Equation

FIDLER Field Instrument for the Detection of Low Energy Radiation

FOV Field of View

g/cc density (gram/cubic centimeter)
HPGe High Purity Germanium Detector
IHSS Individual Hazardous Substance Site
IM/IRA Interim Measures/Interim Remedial Action

ISOCS In Situ Object Counting System

kg kilogram

K-H Kaiser-Hill Company, L.L.C.

m meter

MeV Value of Energy mg/L micrograms per liter

MS/MSD Matrix Spike/Matrix Spike Duplicate

OU Operable Unit

PARCC Precision, Accuracy, Representativeness, Completeness, & Comparability

PCE Tetrachloroethene pCi/g picocuries per gram

Pu Plutonium

QA Quality Assurance

QAPD Quality Assurance Program Description RCRA Resource Conservation and Recovery Act

RFCA Rocky Flats Cleanup Agreement

RFETS Rocky Flats Environmental Technology Site

RFFO Rocky Flats Field Office

RFI/RI RCRA Facility Investigation/Remedial Investigation

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Routine Identification Number
Rocky Mountain Remediation Services, L.L.C.
Relative Percent Difference
Radionuclide Soil Action Level
Radiation Work Permit
Sampling and Analysis Plan
Sum of Ratios
Trichloroethene
Total Measurement Uncertainty
Total Propagated Uncertainty
Uranium
Upper Confidence Limit
micrograms/kilogram
microgram per liter
Verification/Validation
Volatile Organic Compound
Waste Acceptance Criteria

P

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#### **EXECUTIVE SUMMARY**

Investigation of soil contamination at the 903 Drum Storage Area (903 Pad), 903 Lip Area (Lip Area), and Americium Zone was performed to provide characterization data for subsequent evaluation of remedial alternatives for site cleanup. Historically, drums which were stored at the 903 Pad between 1958 and 1967 leaked hydraulic fluids and lathe coolant containing plutonium and depleted uranium. This release contaminated surface and subsurface soil with radionuclides and volatile organic compounds (VOCs). The VOCs have migrated into the shallow groundwater system beneath the 903 Pad.

The primary purpose of this investigation was to estimate the volume of contaminated soil above the Rocky Flats Cleanup Agreement (RFCA) Tier I Radionuclide Soil Action Levels (RSALs) and Subsurface Soil Action Levels (SSALs). Another objective of the investigation was to characterize surface soil to 10 pCi/g americium-241 (<sup>241</sup>Am) using gamma spectroscopy field instrumentation. This characterization would allow for identification of surface soils exceeding Tier II RSALs. Remedial alternatives will be evaluated in the Interim Measure/Interim Remedial Action (IM/IRA) Decision Document based on these volume estimates.

Delineation of radiologically-contaminated soil in the Americium Zone was performed *insitu* using gamma-ray spectroscopy methods, which employ a high purity germanium detector (HPGe). The HPGe instrument was used to obtain 1110 contiguous gamma ray measurements with a circular field of view of 10 meters in diameter within the investigation area. Given this coverage, nearly the entire Americium Zone within the investigation area was surveyed for radionuclides.

The HPGe measurement results were correlated with alpha spectroscopy measurements of radionuclides in eight co-located surface soil samples. The resulting best-fit regression model was used to standardize each HPGe <sup>241</sup>Am measurement to a laboratory-derived <sup>241</sup>Am and plutonium-239/240 (<sup>239/240</sup>Pu) alpha spectroscopy measurement. The correlation results for <sup>241</sup>Am and <sup>239/240</sup>Pu were input into the Tier I and II RSAL sum of ratios equations to determine HPGe measurements locations exceeding the respective action levels.

Based on the standardized HPGe results, surface soil at approximately 37% of the HPGe measurement locations within the Americium Zone has radionuclides exceeding the Tier II RSALs. HPGe results that exceed Tier I RSAL are isolated at a cluster of three locations near the northwest corner of the Americium Zone and at one location in the south central portion of the Lip Area. The Tier I and Tier II RSAL exceedances are a result of elevated activities of <sup>239/240</sup>Pu and <sup>241</sup>Am. Within the Americium Zone, <sup>239/240</sup>Pu activities ranged from 6.32 pCi/g to 938.42 pCi/g and <sup>241</sup>Am activities ranged from 4.91 pCi/g to 149.22 pCi/g.

Contamination of surface and subsurface soils at the 903 Pad and Lip Area was delineated with data obtained from borings at evenly spaced grid nodes. Radiological samples from 79 boring locations were analyzed for <sup>241</sup>Am, <sup>239/240</sup>Pu, uranium-233/234 (<sup>233/234</sup>U), uranium-235 (<sup>235</sup>U), and uranium-238 (<sup>238</sup>U) using alpha spectroscopy. VOC samples were collected from 17 boring locations and were analyzed for VOC contaminants of concern which included carbon tetrachloride (CCL<sub>4</sub>), chloroform, cis-1,2-dichloroethene (1,2-DCE), methylene chloride, tetrachloroethene (PCE), and trichloroethene (TCE).

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Based on the data obtained from borings in the 903 Pad and Lip Area, most of the surface soil (0 to 6 inches) is contaminated above Tier I and Tier II RSALs. <sup>239/240</sup>Pu and <sup>241</sup>Am activities within the 903 Pad and Lip Area ranged from 0.82 pCi/g to 152,260 pCi/g and 0.15 pCi/g to 31,670 pCi/g, respectively. Radiological contamination was also detected in the subsurface soil at depths of 6 to 12 inches and 12 to 18 inches within the 903 Pad and Lip Area; however, <sup>239/240</sup>Pu and <sup>241</sup>Am activities decreased by orders of magnitude at progressively deeper soil horizons.

Artificial fill at the 903 Pad is contaminated above the RFCA Tier II RSALs at one location (Boring 91898). Soil at this boring has elevated levels of <sup>241</sup>Am (126 pCi/g) and <sup>239/240</sup>Pu (558 pCi/g). Asphalt samples from the 903 Pad were also collected for waste characterization profiling but were not compared to RFCA Tier I and Tier II RSALs.

Contaminated soil volumes are based on the areas and depths of Tier I and Tier II RSAL exceedances. The total volume of contaminated soil exceeding Tier I RSALs is 2,235 m<sup>3</sup> (2,924 yds<sup>3</sup>). The total volume of soil exceeding Tier II RSALs is estimated at 11,287 m<sup>3</sup> (14,763 yds<sup>3</sup>). Relative to Tier II RSAL exceedances, the amount of radiologically-contaminated soil at the 903 Pad is 1,889 m<sup>3</sup> (2,471 yds<sup>3</sup>); in the Lip Area is 4,027 m<sup>3</sup> (5,267 yds<sup>3</sup>); and in the Americium Zone is 5,371 m<sup>3</sup> (7,025 yds<sup>3</sup>).

No VOCs were detected in subsurface soil above the current SSALs within the 903 Pad and Lip Area. However, PCE, TCE and 1,2-DCE exceeded proposed Tier I and Tier II SSALs in several borings near well 08891. The total volumes of contaminated soil above proposed Tier I and Tier II SSALs are 558 yds<sup>3</sup> and 3,566 yds<sup>3</sup>, respectively. In addition, 138 yds<sup>3</sup> of contaminated soil containing elevated levels of both radionuclides and VOCs are also present.

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#### 1.0 INTRODUCTION

This report summarizes data collected to determine the location, area, and volume of soil potentially requiring evaluation, management, or remedial action at Individual Hazardous Substance Site (IHSS) 112 - 903 Drum Storage Area (903 Pad), IHSS 155 - 903 Lip Area (Lip Area) and Americium Zone, located at the Rocky Flats Environmental Technology Site (RFETS). Figure 1-1 provides the locations of the IHSSs and the Americium Zone. Remedial alternatives will be evaluated in the Interim Measures/Interim Remedial Action (IM/IRA) Decision Document based on these volume estimates.

Previous investigations have been conducted in these areas to evaluate the extent of contamination, and the data collected have been reported in the Operable Unit (OU) No. 2 Phase II Resource Conservation and Recovery Act (RCRA) Facility Investigation/ Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) Remedial Investigation (RFI/RI) Report (DOE, 1995). However, data from these earlier investigations do not provide the resolution necessary to accurately quantify the volume of soils that may require evaluation, management, or remedial action. Furthermore, with respect to VOC contaminated soils, the historical data do not support the presence of a separate phase dense non-aqueous phase liquid (DNAPL) at the 903 Pad, a model convincingly supported by groundwater data collected at this IHSS. Accordingly, the data reported herein were collected to fill these data gaps.

#### 1.1 SITE BACKGROUND

Waste releases at the 903 Pad (IHSS 112) are considered the primary source of radiological contamination in the surficial soil in this part of the RFETS. Drums that contained hydraulic fluids and lathe coolant contaminated with plutonium and uranium were stored at this location from the Summer of 1958 to January 1967. Approximately three fourths of the drums contained liquids contaminated with plutonium while most of the remaining drums contained liquids contaminated with uranium. Of the drums containing plutonium, the liquid was primarily lathe coolant and carbon tetrachloride in varying proportions. Also stored in the drums were vacuum pump oils, trichloroethene (TCE), tetrachloroethene (PCE), silicone oils, and acetone still bottoms (DOE, 1995).

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Leaking drums were noted in 1964 during routine handling operations. The contents of the leaking drums were transferred to new drums, and the area was fenced to restrict access. When cleanup operations began in 1967, a total of 5,237 drums were at the drum storage site. Approximately 420 drums leaked to some degree. Of these, an estimated 50 drums leaked their entire contents. The total amount of leaked material was estimated at around 5,000 gallons of contaminated liquid containing approximately 86 grams of plutonium (DOE, 1995).

From 1968 through 1970, some of the radiologically-contaminated material was removed from the 903 Pad and Lip Area, some of the surrounding Lip Area was regraded, and much of the area was covered by an imported base coarse material. An asphalt cap was placed over the most contaminated area resulting in the 903 Pad. However, during drum removal and cleanup activities, wind and rain (stormwater erosion) spread plutonium-contaminated soils to the east and southeast from the 903 Pad area resulting in IHSS 155 (903 Lip Area). Several limited excavations have removed some of the plutonium-contaminated soils from the Lip Area (DOE, 1995; Barker, 1982; and RMRS, 1997a). However, results from the OU2 Phase II RFI/RI sampling and analysis and this investigation confirm that radiologically-contaminated soils remain.

Surface soils to the east and southeast of the Lip Area also exhibit elevated plutonium-239/240 (<sup>239/240</sup>Pu) and americium-241 (<sup>241</sup>Am) activities. This contamination is primarily attributed to wind dispersion from the 903 Pad with potential contributions from historical fires, stack effluent, and stormwater related surface soil erosion. Areas exhibiting elevated <sup>239/240</sup>Pu and <sup>241</sup>Am activities east and southeast of the Lip Area are known as the Americium Zone.

#### 1.2 ROCKY FLATS CLEANUP AGREEMENT

The Rocky Flats Cleanup Agreement (RFCA) is a legally binding agreement between the Department of Energy (DOE), the Environmental Protection Agency (EPA) and the Colorado Department of Public Health and Environment (CDPHE) to accomplish the required cleanup of radioactive and other hazardous substance contamination at the RFETS. Action levels and cleanup levels for interim remedial actions have been established for surface water, ground water, and soils and are presented in Attachment 5 of RFCA; "Action Levels and Standards Framework

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for Surface Water, Ground Water, and Soils (ALF)" (K-H, 1999a). Surface soil is defined in the ALF as shallow soil to a depth of 6 inches (in) (15 cm). Subsurface soil is defined in ALF as soil deeper than 6 in (15 cm). Radionuclide Soil Action Levels (RSALs) for an open space future use scenario are the same for surface soils and subsurface soils.

Revisions to the Subsurface Soil Action Levels (SSALs) have been proposed which has resulted in revised Tier I action levels and the inclusion of new Tier II action levels for organic compounds. For this site characterization, contaminant concentrations in surface and subsurface soils have been compared to both Tier I and II RSALs, current Tier I SSALs, and proposed Tier I and Tier II SSALs (Kaiser-Hill, 1999a) in order to assist in the development of the best management strategy for site cleanup. In addition, an independent review of the soil action levels is currently being conducted by the Rocky Flats Soil Action Level Oversight Panel. Based on this independent review and the results from soil erosion modeling being performed by the Actinide Migration Evaluation Panel additional revisions to the soil action levels may be proposed in the future.

The parameters of interest include the activity/concentrations of the following radionuclides/compounds:

- Plutonium-239 /240 (<sup>239/240</sup>Pu);
- Americium-241 (<sup>241</sup>Am);
- Uranium-234 (<sup>234</sup>U);
- Uranium-235 (<sup>235</sup>U);
- Uranium-238 (<sup>238</sup>U); and
- VOCs (subsurface soils only).

Metals, semivolatile organic compounds, pesticides, and polychlorinated biphynels were eliminated as potential contaminants of concern based on data evaluation from previous investigations (DOE, 1995).

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**Radionuclides** - Table 1-1 provides the Tier I and Tier II RSALs for an open space future use exposure scenario.

Table 1-1 RFCA Tier I and II Radionuclide Soil Action Levels - Surface and Subsurface Soils

RADIONUCLIDE	TIER I RSAL (pCi/g)	TIER II RSAL (pCi/g)
<sup>241</sup> Am	215	38
<sup>239/240</sup> Pu	1429	252
<sup>234</sup> U	1738	307
<sup>235</sup> U	135	24
<sup>238</sup> U	586	103

If a mixture of radionuclide contaminants a, b, c are present in the soil with activities  $a_a$ ,  $a_b$ , and  $a_c$ , and if the applicable RSALs, are  $A_a$ ,  $A_b$ , and  $A_c$  respectively, then the activity in the soil shall be considered as exceeding the RSALs if the sum of ratios (SOR) is greater than 1, i.e.,

Sum of Ratios (SORs) = 
$$\frac{a_a}{A_a} + \frac{a_b}{A_b} + \frac{a_c}{A_c} > 1$$
 (Equation 1-1)

Volatile Organic Compounds - Table 1-2 provides the current Tier I SSALs and the proposed Tier I and Tier II SSALs for VOC contaminants of concern in soils at the 903 Pad.

Table 1-2 Subsurface Soil Action Levels - VOCs

COMPOUND	Current TIER I SSAL (mg/kg)	Proposed TIER I SSAL (mg/kg)	Proposed TIER II SSAL (mg/kg)
Carbon Tetrachloride	11.00	3.56	0.0356
Chloroform	152.00	21.4	0.214
1,2,-Dichloroethene (Total)	9.51	14.0	0.14
Methylene Chloride	5.77	0.578	0.00578
Tetrachloroethene	11.5	3.15	0.0315
Trichloroethene	9.27	3.28	0.0328

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#### 1.3 EXISTING DATA

Numerous investigations to assess the extent of contamination at the 903 Pad, Lip Area, and Americium Zone have been conducted. These investigations are briefly described below.

#### 1.3.1 Surface Soils

High Purity Germanium (HPGe) Surveys - HPGe surveys conducted in 1990 (EG&G, 1991) and 1994 (DOE, 1995; RMRS, 1997b) provide useful information on the activity of <sup>241</sup>Am in surface soils over the Americium Zone study area. These data were collected on a 150-foot grid to accommodate the HPGe detector's field of view (FOV) of 150 feet in diameter (17,671 ft²) (Figure 1-2). Surveys were not conducted over the 903 Pad and Lip Area and soil samples were not collected to supplement the surveys. The results from these surveys were utilized to define the boundaries of this characterization's investigation area.

Surface Soil Radiological Data - Surface soil samples were collected in support of the OU2 Phase II RFI/RI (DOE, 1995). As detailed in the RFI/RI, samples were collected utilizing two sampling methods; the Colorado Department of Health (CDH) sampling method and the Rocky Flats (RF) sampling method. Surface soil sample results were compared with Tier I RSALs. The results of the comparison indicated that samples collected from five 2.5-acre plots exceed the Tier I RSALs. These plots include two 2.5-acre plots (Plots 28 and 34) sampled using the CDH sampling method and three 2.5-acre plots (Plots 29, 36, and 46) sampled using the RF method (Figure 1-3).

#### 1.3.2 Subsurface Soils

Subsurface Soil Radiological Data - Three data sources were evaluated to determine the depth of radiological contamination within the study area: 1) RFI/RI borehole data (DOE, 1995); 2) RFI/RI soil profile pits (DOE, 1995); and 3) samples collected in support of a 1980 soil decontamination project (Rutherford, 1981). Results from the RFI/RI borehole samples were compared to RSALs and revealed that no samples exceed the Tier I RSALs. However, samples collected from soil profile pit TR08 exceeded Tier I RSALs to a depth of 27 centimeters (cm) (10.6 in). Soil profile pits were sampled at 3 cm (1.2 in) intervals to a total depth of 1 meter (m)

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(3.28 feet). Samples collected at soil profile pit TR06, located adjacent to pit TR08, were not analyzed because activities exceeded the DOT shipping requirements. It is assumed that radiochemical results from pit TR06 would also exceed Tier I RSALs, if analyzed.

Soil samples collected beneath the 903 Pad in support of the 1980 soil decontamination project exceeded Tier I RSALs to a depth of 66 cm (26-in) (RMRS, 1997b). This depth exceeds the thickness of the asphalt pad and the depth of imported base coarse material and indicates radiological contamination of natural undisturbed soils at the 903 Pad. However, no RFI/RI soil borings detected radiological contamination in excess of Tier I RSALs. As a result, a discrepancy with the depth of radiological contamination between these investigations exists.

Subsurface Soil VOC Data - Three sources of data were evaluated to determine the nature and extent of contamination at the 903 Pad: 1) RFI/RI borehole data (DOE, 1995); 2) IM/IRA soil gas survey results (DOE, 1994); and 3) groundwater monitoring well data.

Borehole sample results from the RFI/RI were compared with current Tier I SSALs revealed that no samples exceeded the current Tier I SSALs for organic contaminants. The soil gas survey indicated that the highest VOC concentrations were located immediately south of the southeast corner of the 903 Pad. Tetrachloroethene was detected at 27,000 micrograms per liter (ug/L) at a depth of 5 feet. However, at adjacent soil gas locations and boreholes, tetrachloroethene is either not detected or detected at very low concentrations. Soil gas concentrations for the remaining portion of the 903 Pad ranged from 0-500 ug/L with the highest concentrations around and north of monitoring well 08891 (Figure 1-4).

#### 1.3.3 Groundwater

A VOC-contaminated groundwater plume extends from the 903 Pad area to the east. The highest concentrations are found in groundwater samples collected from wells 06691 and 08891, which are located on the asphalt portion of the 903 Pad. Concentrations of contaminants in groundwater decrease rapidly moving eastward from the 903 Pad area. The primary groundwater contaminant in well 06691 is carbon tetrachloride with concentrations ranging from 51 to 100,000 ug/L. Methylene chloride (150 to 29,000 ug/L) and chloroform (92 to 46,000 ug/L) are also observed.

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Groundwater sample results for well 08891 indicate the primary contaminant as PCE at concentrations ranging from 470 to 27,000 ug/L, along with carbon tetrachloride (290 to 17,000 ug/L), cis-1,2,dichloroethene (94 to 2,900 ug/L) and TCE (210 to 4,600 ug/L). The next highest concentration of carbon tetrachloride in groundwater is found in samples collected from well 13191, which is located west of the well 06691 and off the western edge of the 903 Pad. At this location, observed carbon tetrachloride levels ranged from 122 to 4,800 ug/L.

Concentrations of VOCs in groundwater decrease rapidly eastward from the 903 Pad area (DOE, 1995). For example, during the June 1998 groundwater sampling, well 06991 had 210 ug/L PCE and well 1587 had 880 ug/L PCE which are two orders of magnitude less than the concentration observed in well 08891 with 27,000 ug/L PCE (Figure 1-4).

Because of the complex nature of DNAPL transport and fate, DNAPL may often be undetected by direct methods leading to incomplete site assessments and inadequate remedial designs (EPA, 1992). A guide for estimating the potential for a DNAPL source at a site includes assessing if concentrations of DNAPL-related chemicals in groundwater are greater than 1% of the pure (single) phase solubility of the compound (EPA, 1992).

Table 1-3 provides a comparison of the pure single phase aqueous solubility and concentrations of DNAPL-compounds detected in groundwater at the 903 Pad (wells 06691 and 08891) from a June 1998 sampling event of monitoring wells 06691 and 08891. The comparison indicates that PCE and carbon tetrachloride have been detected in groundwater samples at 13.5% and 10.7% of their aqueous solubilities, respectively. These results and the known historical releases at the 903 Pad indicate there is a potential for pure phase organic contaminants in subsurface soils beneath the 903 Pad.

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TABLE 1-3 Comparison of Pure Single Phase Aqueous Solubilities with VOC Concentrations in Groundwater

Compound	Pure Single Phase Aqueous Solubility at 25°C¹ (mg/l)	Concentration Detected in Groundwater June 1998 (mg/l)	Ratio Groundwater Concentration/ Aqueous Solubility (%)
Carbon Tetrachloride	793	85.0	10.7
Chloroform	7,920	4.4	0.1
cis-1,2,dichloroethene	3,500	1.3	0.04
Methylene Chloride	13,000	29.0	2.2
PCE	200	27.0	13.5
TCE	1,100	1.3	0.12

<sup>&</sup>lt;sup>1</sup>EPA, 1996. Soil Screening Guidance: Technical Background Document

#### 1.4 SURFICIAL GEOLOGY

The surficial geology in the study area consists of Quaternary alluvium, colluvium and slump deposits along with artificial fill, soil and debris deposits, and disturbed soil. The surficial deposits overlie bedrock which consists of weathered claystone and minor bedrock sandstones of the Cretaceous Arapahoe and Laramie Formations. Surficial deposits consist of sandy clay and clayey gravel. Soil developed over the alluvium is rocky and sandy in contrast to the clayey soils developed over the claystone bedrock.

For this investigation, the surface and subsurface soils were subdivided into six soil horizons: (1) the Native 1 soil horizon consists of natural soils from 0 to 6 inches (surface soils); (2) the Native 2 soil horizon designates subsurface soils from 6 inches to 1 foot: (3) the Native 3 soil horizon designates subsurface soil from 1 to 1.5 feet; (4) the Native 4 soil horizon designates subsurface soil from 1.5 to 2.0 feet; (5) the Native group consists of Quaternary alluvium from the bottom of the Native 4 soil horizon (2.0 feet) to the bedrock contact; and (6) the Bedrock group consists of consolidated geologic material from the undifferentiated Laramie/Arapahoe Formations.

Artificial fill is present directly beneath the 903 Pad and in the Lip Area as a result of previous remediation activities. In November 1968 "slightly-contaminated" soil was graded from outside the fence at the 903 Pad into the fenced area to be capped. In September of 1969 a base coarse

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(artificial fill) material overlay, soil sterilant, and asphalt primer were constructed for the 903 "containment barrier" (Pad). The asphalt pad was constructed in October of 1969 and was reportedly 3 in (7.6 cm) thick. The thickness of the base coarse materials beneath the 903 Pad was assumed to be approximately 8 inches (20 cm). In February 1970, operations were initiated to apply additional fill (base coarse) over the Lip Area due to soil contamination. The thickness of the fill material reportedly ranged from 0.8 in (2 cm) to 5.1 in (13 cm) (DOE, 1995; RMRS, 1997b).

#### 1.5 SITE CONCEPTUAL MODEL

The contaminants present in the surface and subsurface soil are primarily a result of drum storage in the 903 Pad area. Drums containing hydraulic fluids and lathe coolant contaminated with plutonium and uranium leaked onto the surface soil. The liquids from the drums may have moved downward towards the bedrock surface, possibly carrying a fraction of the radionuclides into the subsurface along preferential pathways such as rodent holes, desiccation cracks, and/or along decayed roots. High winds and heavy rains spread the surficial radiological contamination outward from the 903 Pad, depositing it on surface soils in the Lip Area and Americium Zone.

Previous HPGe surveys from the study area and surface soil sample data show that, in general, higher concentrations are present near the 903 Pad, and concentrations decrease with increasing distance from the 903 Pad. Immediately east and south of the 903 Pad and Lip Area, there are areas of higher concentrations which may be the result of wind and surface water dispersion of contaminants (DOE, 1995). Accounting for the surface soil and HPGe sampling already collected from the 903 Pad area to Indiana Street, and the direction of surface water flow from the 903 Pad towards the South Interceptor Ditch, it was concluded that hot spots are not likely to be present to the east, outside of the Investigation Area (Figure 1-4).

The source of subsurface VOC contamination is suspected to be present directly beneath the area where drums were previously stored (DOE, 1995; RMRS; 1997b). The liquid contained in the drums may have migrated downward towards the bedrock surface. An east-west paleochannel is cut into the bedrock, with the greatest depth to bedrock located toward the middle of the 903 Pad (DOE, 1995; RMRS, 1997b; RMRS, 1997c). Available subsurface and groundwater VOC data

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(see Section 1.3) indicates that any potential source of DNAPL contamination is limited to the area under the present 903 Pad. The VOC contamination east of the 903 Pad is limited to the dissolved phase in groundwater as supported by groundwater data (see Section 1.3.3) (DOE, 1995; RMRS, 1998e).

#### 1.6 PROJECT INVESTIGATION AREA

Based on the foregoing evaluation of the existing data in the study area, an Investigation Area was defined for this site characterization that represents the area where additional data is required to refine the volume estimate of contaminated soils (Figure 1-4). The Investigation Area represents that portion of the study area which is known, or in which a potential exists, for surface and/or subsurface soils to exceed Tier I RSALs and current Tier I SSALs. These areas include:

- Surface soils exceeding 10 pCi/g <sup>241</sup>Am as identified in the 1990 and 1994 HPGe surveys;
- Areas where artificial fill (and asphalt) has been placed over natural soils including the 903
   Pad, Lip Area, and areas remedied in 1976, 1978, and 1984;
- Five 2.5-acre plots identified as exceeding Tier I soil action levels based on OU2 RFI/RI surface soil sampling results: and
- The 903 Pad and Lip Area where a subsurface VOC source is suspected as the source of a groundwater contaminant plume.

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## 2.0 FIELD INVESTIGATION

#### 2.1 OVERVIEW

The lateral and vertical extent of radiological and VOC contamination was assessed within the proposed investigation area. The lateral extent of radiological contamination in the Americium Zone and a portion of the Lip Area were primarily assessed using a non-intrusive HPGe field method. The HPGe method results were "standardized" by correlation to radiochemical data collected by sampling surface soils from selected HPGe measurement locations, and analyzing these samples for radionuclides using alpha spectroscopy. The lateral and vertical extent of contamination at the 903 Pad and a majority of the Lip Area were assessed utilizing sample collection methods employing a Geoprobe®, and analyzing the samples for radionuclides and VOCs in a laboratory. The data were collected pursuant to the Sampling and Analysis Plan for the Site Characterization of the 903 Drum Storage Area (IHSS 112), 903 Lip Area (IHSS 155), and Americium Zone (SAP) (RMRS, 1998a).

#### 2.2 SURFACE SOIL INVESTIGATION

The activities of <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/234</sup>U, <sup>235</sup>U, and <sup>238</sup>U in surface soils within the Americium Zone and a portion of the Lip Area were measured *in situ* using an HPGe survey together with radiochemical analyses of surface soil samples.

## 2.2.1 HPGe Methodology

The HPGe instrument measures *in situ* activities of <sup>241</sup>Am, <sup>235</sup>U and <sup>238</sup>U. For this investigation, the HPGe measurement had a field of view (FOV) of 10 meters (m) in diameter with the detector placed 1-m over the ground surface. The Compendium of *In Situ* Radiological Methods and Applications at Rocky Flats Plant (EG&G, 1993) provides a detailed discussion on the physics of *in situ* measurement of radionuclides in the environment.

The HPGe survey focused on the Americium Zone (Figure 2-1) and includes all surface soils with elevated concentrations of <sup>239/240</sup>Pu and/or <sup>241</sup>Am identified during the OU2 RFI/RI including:

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- The 35 HPGe measurements which exhibit elevated (above 10 pCi/g) <sup>241</sup>Am activities:
- The area directly below the culvert which drains the 903 Pad and Lip Area where sediments are deposited during surface runoff events; and
- The five 2.5-acre plots where surface soils exceed Tier I RSALs.

The HPGe system used to perform in situ measurements for the investigation employs the Canberra In Situ Object Counting System (ISOCS) software. In order to estimate counting efficiencies, this software requires the entry of various parameters which should accurately represent the actual field conditions at the site. One important parameter is the distribution of contaminants vertically. In the HPGe investigation area, contamination was deposited via airborne and/or surface water releases. This resulted in a distribution with high activities near the surface and decreasing activities with depth, which may follow an exponential function. Surface soil sampling was previously performed in the study area to determine the vertical distributions. In general, the radionuclides are concentrated in the top 5-cm. Based on available data, the ISOCS model assumes all contamination is contained in the top 5-cm, and it is distributed with 66% in the top 3-cm and 33% in the next 2-cm. This distribution was used to be consistent with the surface soil sampling methodologies (RMRS, 1998a), which specifies sampling surface soil to a depth of two inches (5 cm). In addition, the contribution from <sup>241</sup>Am below a depth of 5 cm in soil is quite small. It is possible that the actual distributions in the top 5-cm may be more concentrated near the surface or more uniformly distributed throughout the 5-cm layer. A set of efficiencies with different vertical distributions was prepared and the standard acquisition analyzed.

#### Results:

Default 2 layer 0-3 cm 66%, 3-5 cm 33%	$^{241}$ Am = 12.2 pCi/g
Single layer, 0-5 cm uniform	$^{241}$ Am = 14.3 pCi/g
3 layers, 0-1.5cm 50%, 1.5-3 cm 30%, 3-5 cm 20%	$^{241}$ Am = 11.6 pCi/g
3 layers, default with 1cm grass cover	$^{241}$ Am = 13.2 pCi/g
2 layer with 0-3 cm 60%, 3-5 cm 40%	$^{241}$ Am = 12.2 pCi/g

As can be seen, the overall error of a likely range of possible distributions is about +/- 10 %.

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## 2.2.2 Double Sampling Correlation Technique

To "standardize" the *in situ* method, a double sampling technique was employed whereby soil samples were collected from select HPGe measurement locations (RMRS, 1998a) and analyzed in the laboratory for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/244</sup>U, <sup>235</sup>U, and <sup>238</sup>U using alpha spectroscopy, and <sup>241</sup>Am and <sup>235</sup>U using gamma spectroscopy. [The gamma spectroscopy data was collected by the laboratory to simply "validate" the alpha spectroscopy results, and the two sets of results are comparable as indicated by their linear relationship with a slope of one [(Table 2-1) (Figure 2-2)].

Table 2-1 Laboratory Gamma Spectroscopy Results vs. Laboratory Alpha Spectroscopy Results – <sup>241</sup>Am

HPGe Measurement Location	Laboratory Gamma Spectroscopy Results <sup>241</sup> Am (pCl/g) dry wt	Laboratory Alpha Spectroscopy Results <sup>241</sup> Am (pCl/g) dry wt
30*	3.67	3.67
104	19.08	27.80
265	45.46	49.32
266	21.89	22.60
305	7.45	11.05
406	107.86	77.27
460*	111.09	148.23
669*	57.84	57.85

<sup>\*</sup> Real and Duplicate Sample Results Averaged

In order to acquire a good double sampling correlation over the anticipated range of <sup>241</sup>Am activities, eight HPGe measurement locations were selected that encompass five <sup>241</sup>Am activity intervals; 0-10 (three measurements), 10-20, 20-50 (two measurements), 50-100, and 100-200 pCi/g. These intervals were selected based on detection frequencies of <sup>241</sup>Am activities measured in surface soil samples collected in support of the OU2 Phase II RFI/RI (DOE, 1995; RMRS, 1998a).

Multiple HPGe measurements were taken at some of the double sampling locations for quality control. These results are provided in Table 2-2. In these cases, the measurements at each double sampling location were averaged to create the HPGe data set used in the correlation. Table 2-2 also indicates the HPGe measurements at each double sampling location are relatively uniform.

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locations
Sampling
at Double
241 Am Results
HPGe 241 Am
Table 2-2

HPGe Measurement 30	ement	Measurement 104	ement	Measuremen 265	Gement 5	HPGe Measurement 266	HPGe surement 266	HPGe Measurement 305	HPGe Isurement 305	HPGe Measurement 406	Ge ement 6	HPGe Measurement 460	se ament 0	HPGe Measurement 669	Ge ement 9
Count Juration (sec)	24.Am (pCi/g)	Count 24,4m Count	241 <b>A</b> m (pCi/g)	Count Duration (sec)	"'Am (pCi/g)	Count Duration (sec)	241Am (pCi/g)	Count MAm Duration (pci/g)	241Am (pCi/g)	Count MAm Duration (pCi/g)	<sup>241</sup> Am (pCi/g)	Count 24 Am Count 24 Am Duration (pCi/g)	<sup>241</sup> Am (pCi/g)	Count	24'Am (pCi/g)
006	1.1	006	14.5	006	34.3	900	9.1		7.0		70.5		106.2	28	000
		006	17.6	006	39.0						2.0.6		- 1		32.2
		006	20.6	006	39.1			1200			61.7		-		32.8
		1200	15.5	006	37.3			1200			2. 0		2.00		39.5
		1200	22.6		31.7			1200			0.2.0	000	98.3		35.3
		1200	17.6	006	29.2			1200	5.7		00.00		1.01.1	1200	35.2
		1200	23.0	006	31.3			1200	5.4			000	00.00		A CORP. TO SEE SEE SEE SEE SEE
		900	15.1	006	39.3			1200	40				THE RESERVE AND PROPERTY OF THE PERSON OF TH		
		900	17.6	006	34.4				2						
-		1200	13.0												
		1200	18.6												
		1200	19.4							N Marada Marada					
-		1200	15.8												
		1200	15.8												The state of the s
Verage	1.1		17.6		35.4		7								

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Fifteen (15) grab samples were then collected at each double sampling location; one grab sample from the center; four grab samples collected at 1- m radius, and ten grab samples from 3-m radius. Figure 2-3 provides this surface soil sampling geometry which was developed by the DOE (DOE, 1997) at the Fernald Environmental Management Project site in Ohio in order to correlate HPGe results to surface soil results. The 1-m and 3-m radius grab samples were then composited into a 1-m and 3-m sample representative of each individual band. Therefore, three separate alpha (and gamma) spectroscopy analyses were performed at each double sampling location.

Samples were collected in this "bulls eye" pattern to mimic the averaging done by the field HPGe detector over the instrument's FOV. The HPGe detector receives gamma-ray photons from every point within the circle; however, it receives more gamma rays from soil closer to the detector than from soil further from the detector. If the circle is divided into concentric bands, the relative weighting factor for each band can be calculated based upon the percentage influence of gamma photons at the detector which originates from a given band of soil, assuming a uniform source distribution with depth and a one MeV photon energy. The relative weighting factor is the relative importance of each band with respect to the probability of gamma-rays emitted from within that band being detected by the HPGe (Table 2-3). The sample results were multiplied by the weighting factor per band, then the products were summed to determine the activity of the soils in the FOV area. Tables 2-4 and 2-5 provide the results of these calculations, including adjustment for moisture content in order to report results on a wet weight or "in situ moisture" basis. Note that if field duplicate samples were collected at a given double sampling location, the "real" and "duplicate" data were averaged (denoted as "combined"), and the "combined" data were used in the weighted averaging process to develop the data for the correlation.

Table 2-3 Surface Soil Samples, Weighted Average Calculations

Horizontal Distance from Point Under Detector (m)	Weight (per circle)
0	0.1
1	0.36
3	0.54
Total	1.00

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# Table 2-4 Alpha Spectroscopy Results for <sup>241</sup>Am at Double Sampling Locations

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCi/g)	Moisture Content (%)	Am-241 Weighted Average (pCl/g)	Am-241 Weighted Average Corrected for Moisture (pCi/g)
30	Real	99A5936-002.001	0	2.3659	4.99	.24	.2253
	Real	99A5936-004.001	1	4.6643	4.6	1.68	1.6053
	Real	99A5936-006.001	3	3.574	5.18	1.93	1.8349
		Average		3.535		3,85	3.666
30	Duplicate	99A5936-003.001	0	1.7105	4.99	17	.1629
	Duplicate	99A5936-005.001	1	4.4612	4.6	1.61	1.5354
	Duplicate	99A5936-007.001	3	3.1966	5.18	1.73	1.6412
		Average		3.123		3,50	3.339
30	Combined		0	2.0382	4.99	.2	.1941
	Combined		1	4.5628	4.6	1.64	1.5704
	Combined		3	3.3853	5.18	1.83	1.738
		Average		3.329		3.67	3.503

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCi/g)	Moisture Content (%)	Am-241 Weighted Average (pCi/g)	Am-241 Weighted Average Corrected for Moisture (pCl/g)
104	Real	98A5590-001.002	0	11.2017	4.28	1.12	1.0742
	Real	98A5590-001.004	1	29.3735	3.63	10.57	10.2041
	Real	99A5590-004.001	3	29.824	2.56	16.1	15.703
		Average		23.466		27.80	26.981

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCi/g)	Moisture Content (%)	Am-241 Weighted Average (pCi/g)	Am-241 Weighted Average Corrected for Moisture (pCi/g)
265	Real	98A5590-002.002	0	36.6004	2.34	3.66	3.5764
-	Real	98A5590-002.004	1	70.1548	9.99	25.26	22.9618
	Real	98A5590-002.006	3	37.785	2.83	20.4	19.8424
		Average		48.180		49.32	46.381

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCi/g)	Moisture Content (%)	Am-241 Weighted Average (pCl/g)	Am-241 Weighted Average Corrected for Moisture (pCi/g)
266	Real	98A3372-003.002	0	33.7418	18.91	3.37	2.8376
	Real	98A3372-003.004	1	22.6443	9.6	8.15	7.4379
	Real	98A3372-003.006	3	20.503	12.55	11.07	9.8371
		Average		25.630		22.60	20.113

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Table 2-4 Alpha Spectroscopy Results for <sup>241</sup>Am at Double Sampling Locations (Cont.)

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCi/g)	Moisture Content (%)	Am-241 Weighted Average (pCi/g)	Am-241 Weighted Average Corrected for Moisture (pCl/g)
305	Real	98A5590-003.002	0	9.947	5.04	.99	.947
	Real	98A5590-003.004	1 1	9.2659	1.13	3.34	3.2985
	Real	98A5590-003.006	3	12.4345	1.2	6.71	6.635
10.75		Average		10.549		11.05	10.88

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCl/g)	Moisture Content (%)	Am-241 Weighted Average (pCl/g)	Am-241 Weighted Average Corrected for Moisture (pCi/g)
406	Real	98A3372-001.002	0	101.9353	5.91	10.19	9.6247
	Real	98A3372-001.004	1	77.7979	5.2	28.01	26.6229
	Real	98A3372-001.006	3	72.3595	4.38	39.07	37.4345
		Average		84.031		77.27	73.682

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCl/g)	Moisture Content (%)	Am-241 Weighted Average (pCi/g)	Am-241 Weighted Average Corrected for Moisture (pCi/g)
460	Real	98A3372-002.002	0	90.1227	11.65	9.01	8.0719
	Real	98A3372-002.004	1	151.9866	12.66	54.72	48.5666
	Real	98A3372-002.006	3	137.9899	8.67	74.51	68.5696
		Average		126.700		138.24	125.208
460	Duplicate	99A3372-002.007	0	175.1638	11.65	17.52	15.6887
	Duplicate	99A3372-002.008	1 1	172.9098	12.66	62.25	55.2526
	Duplicate	99A3372-002.009	3	145.2979	8.67	78.46	72.201
		Average		164.457		158.22	143.142
460	Combined		0	132.6433	11.65	13.26	11.8803
	Combined		1	162.4482	12.66	58.48	51.9096
	Combined		3	141.6439	8.67	76.49	70.3853
		Average		145.578		148.23	134.175

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Table 2-4 Alpha Spectroscopy Results for <sup>241</sup>Am at Double Sampling Locations (Cont.)

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Am-241 (pCi/g)	Moisture Content (%)	Am-241 Weighted Average (pCl/g)	Am-241 Weighted Average Corrected for Moisture (pCl/g)
669	Real	99A4878-003.001	0	40.8194	8.62	4.08	3.758
	Real	99A4878-005.001	1	55.0517	10.	19.82	18.0169
	Real	99A4878-007.001	3	60.4235	7.99	32.63	30.2145
		Average		52.098		56.53	51.989
669	Duplicate	99A4878-004.001	0	75.9211	8.62	7.59	6.9896
	Duplicate	99A4878-006.001	1	66.7147	10.	24.02	21.8339
	Duplicate	99A4878-008.001	3	51.0332	7.99	27.56	25.519
		Average		64.556		59.17	54.342
669	Combined		0	58.3703	8.62	5.84	5.3738
	Combined		1 1	60.8832	10.	21.92	19.9254
	Combined		3	55.7284	7.99	30.09	27.8668
	2000 000 000 000 000 000 000 000 000 00	Average	0.26	58.327		57.85	53.166

Table 2-5 Alpha Spectroscopy Results for <sup>239/240</sup>Pu at Double Sampling Locations

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCl/g)	Moisture Content (%)	Pu -239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCl/g)
30	Real	99A5936-002.001	0	12.8235	4.99	1.28	1.2214
	Real	99A5936-004.001	1	21.7524	4.6	7.83	7.4865
	Real	99A5936-006.001	3	23.8498	5.18	12.88	12.2446
	Transfer and the	Average		19.475		21.99	20.953
30	Duplicate	99A5936-003.001	0	8.4155	4.99	.84	
	Duplicate	99A5936-005.001	1	23.1372	4.6	8.33	7.9631
	Duplicate	99A5936-007.001	3	15.5486	5.18	8.4	7.9827
	Million Committee	Average		15.700		17.57	16.747
30	Combined		0	10.6195	4.99	1.06	1.0115
	Combined		1	22.4448	4.6	8.08	7.7248
	Combined		3	19.6992	5.18	10.64	10.1137
		Average		17.588	E.	19.78	18.85

HPGe Measurement Location	Sample Type	, Sample No.	Radius (m)	Pu-239/240 (pCi/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCi/g)
104	Real	98A5590-001.002	0	61.0754	4.28	6.11	5.8569
	Real	98A5590-001.004	1	121.7496	3.63	43.83	42.2946
	Real	98A5590-001.006	3	161.424	2.56	87.17	84.9931
		Average		114.750		137.11	133.145

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Table 2-5 Alpha Spectroscopy Results for <sup>239/240</sup>Pu at Double Sampling Locations (Cont.)

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCi/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCl/g)
265	Real	98A5590-002.002	0	150.7151	2.34	15.07	14.7269
	Real	98A5590-002.004	1	150.3247	9.99	54.12	49.2016
	Real	98A5590-002.006	3	151.1863	2.83	81.64	79.3938
kerona alah		Average		150.742		150.83	143.322

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCi/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCl/g)
266	Real	98A3372-003.002	0	250.0412	18.91	25.00	21.0278
	Real	98A3372-003.004	1	194.6868	9.6	70.09	63.9482
	Real	98A3372-003.006	3	87.7801	12.55	47.4	42.1157
		Average		177.503		142.49	127.092

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCi/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCl/g)
305	Real	98A5590-003.002	0	80.7024	5.04	8.07	7.683
	Real	98A5590-003.004	1	67.9077	1.13	24.45	24.1736
	Real	98A5590-003.006	3	48.3793	1.2	26.12	25.815
		Average		65,663		58.64	57.672

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCi/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCl/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCi/g)
406	Real	98A3372-001.002	0	906.2229	5.91	90.62	85.5654
	Real	98A3372-001.004	1	524.8652	5.2	188.95	179.6117
	Real	98A3372-001.006	3	519.3453	4.38	280.45	268.6784
		Average	le ver	650.144		560.02	533.855

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Table 2-5 Alpha Spectroscopy Results for <sup>239/240</sup>Pu at Double Sampling Locations (Cont.)

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCi/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCl/g)
460	Real	98A3372-002.002	0	554.3172	11.65	55.43	49.6478
	Real	98A3372-002.004	1	1,481.6998	12.66	533.41	473.4706
	Real	98A3372-002.006	3	675.0613	8.67	364.53	335.4496
		Average .		903.693		953,38	858.568
460	Duplicate	99A5936-002.001	0	782.3574	11.65	78.24	70.0723
	Duplicate	99A5936-004.001	1	684.6637	12.66	246.48	218.7812
	Duplicate	99A5936-006.001	3	841.5062	8.67	454.41	418.159
		Average		769.509		779.13	707.013
460	Combined		0	668.3373	11.65	66.83	. 59.86
	Combined		1	1,083.1818	12.66	389.95	346.1259
	Combined		3	758.2838	8.67	409.47	376.8043
		Average		836.601		866.25	782.79

HPGe Measurement Location	Sample Type	Sample No.	Radius (m)	Pu-239/240 (pCl/g)	Moisture Content (%)	Pu-239/240 Weighted Average (pCi/g)	Pu-239/240 Weighted Average Corrected for Moisture (pCl/g)
669	Real	99A4878-003.001	0	265.908	8.62	26.59	24.4806
	Real	99A4878-005.001	1	318.3239	10.	114.6	104.1787
	Real	99A4878-007.001	3	376.36	7.99	203.23	188.1974
		Average .		320.197		344.42	316.857
669	Duplicate	99A4878-004.001	0	525.3358	8.62	52.53	48.3646
	Duplicate	99A4878-006.001	1	435.6164	10.	156.82	142.5654
	Duplicate	99A4878-008.001	3	297.2583	7.99	160:52	148.6429
		Average		419.404		369.87	339.573
669	Combined		0	395.6219	8.62	39.56	36.4226
	Combined		1	376.9702	10.	135.71	123.372
	Combined	1	3	336.8092	7.99	181.88	168.4202
		Average .		369.800		357.15	328.215

# 2.2.2.1 Alpha Spectroscopy/HPGe <sup>239/240</sup> Pu and <sup>241</sup>Am Correlations

The linear regressions (using the method of least squares) between the alpha spectrometry data (<sup>239/240</sup>Pu and <sup>241</sup>Am) and the HPGe data (<sup>241</sup>Am) show very high degrees of correlation (Figures 2-4 and 2-5). The correlation coefficients (R) are greater than or equal to 0.97. The <sup>241</sup>Am (alpha spectrometry) to <sup>241</sup>Am (HPGe) correlation has a slope (1.25) near 1.0 and a small intercept (4.43 pCi/g) near zero as would be expected when correlating the activities of the same radionuclide.

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The <sup>239/240</sup>Pu (alpha spectrometry) to <sup>241</sup>Am (HPGe) correlation has a slope of 8.08 which is within the expected range of <sup>239/240</sup> Pu to <sup>241</sup>Am activity ratios considering the in-growth of <sup>241</sup>Am in weapons grade plutonium over 30 to 40 years (elapsed time since the release). The intercept (3.24 pCi/g) is also small in magnitude. These results indicate the regression lines are appropriate models to correlate HPGe data to alpha spectrometry data.

However, according to the SAP (RMRS, 1998a), the 95% upper confidence limits (UCL) of the linear regressions are to provide the equations to calculate the activities of these isotopes in the surface soils at all *in situ* measurement locations (see Figures 2-4 and 2-5). Examination of the results from using the 95% UCL to determine RSAL exceedances strongly suggest this alternative "model" to be overly conservative. Figures 2-6, 2-7, and 2-8 show RSAL exceedances in surface soils in the Americium Zone based on the direct HPGe results<sup>1</sup>, the least square regression lines ("best fit" lines), and the 95% UCL equations for the "best fit" lines, respectively. Also plotted on these figures are RSAL comparisons for historical surface soil data (0-2 inches) from the OU2 RFI/RI trenching investigations (DOE, 1995) and a surface soil investigation conducted by the Actinide Migration Evaluation Project (RMRS, 1998f). These figures also provided RSAL comparisons for the alpha spectrometry results of surface soil samples collected at the eight double sampling locations for this investigation. Analytical results and RSAL comparisons for these surface soil samples are provided in Tables 2-6, 2-7, and 2-8.

As would be expected, Figures 2-6, 2-7, and 2-8 indicate progressively higher actinide levels in surface soils, i.e. increasing numbers of Tier I, and in particular, Tier II RSAL exceedances. As can be seen, the "best fit" line results (Figure 2-7) are substantiated by the historical data. For example, unlike the HPGe "direct" results (Figure 2-6), the Tier II exceedances plotted using the "best fit" line (Figure 2-7) extend to the south bordering on location TR09 (a Tier II exceedance),

<sup>&</sup>lt;sup>1</sup> Because <sup>239/240</sup> Pu is not measured directly by the HPGe instrument at low levels, the <sup>239/240</sup> Pu data used to determine RSAL exceedances was estimated using the <sup>239/240</sup> Pu to <sup>241</sup>Am activity ratio of 5.8 derived from the slope of the regression line (Figure 2-9) for the <sup>239/240</sup> Pu and <sup>241</sup>Am alpha spectroscopy results from the surface soil samples collected at the eight double sampling locations (using real and duplicate sample results).

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Table 2-6 Alpha Spectroscopy Results of Trench Soil Samples - OU2 RFI/RI	
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Tier II SOR	5.036		-			3 523	í 				4 468	2				2.433					1.424				
Tier I	0.889					0 622					0.789			•		0.429					0.251	-			
Qual				7	1		_		7	١ .				7				•	7	····			_	_	
Units Qual	pCj/a	pCi/a	pCi/g	pCi/a	pCi/a	pCi/a	pCi/a	pCi/a	pCi/d	pCi/g	pCi/q	pCi/q	pCi/g	pCi/q	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g
Result	109.9000	535.3000	1.0080	0.0819	1.3520	63.7300	459.9000	1.2540	0.0359	1.5680	71.1800	646.6000		0.000	2.2070	34.1200	381.3000	1.4260	0.0483	1.6100	23.3700	198.7000	1.1960	0.0636	1.3920
Analyte	Am-241	Pu-239/40	U-233,-234	U-235	U-238DA	Am-241	Pu-239/40	U-233,-234	U-235	U-238DA	Am-241	Pu-239/40	U-233,-234	U-235	U-238DA	Am-241	Pu-239/40	U-233,-234	U-235	U-238DA	Am-241	Pu-239/40	U-233,-234	U-235	U-238DA
၁၉	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL	REAL			REAL
Sampling Interval (cm)	0-3					3-6					0-3					3-6		_			e-0		<del></del> -		
Sample	748884 TR00422WCU2					TR00421WCU2					/48918   TR00367WCU2					TR00366WCU2					748432 I R00300WCU2				
Northing	748884				<b></b>						/48918					<u>.                                      </u>				0,00	748432				
Location Easting Northing	2086630									0000	70865/0									070000	7086350				
Location	TR04									7007	COX-									000	202				

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Table 2-6 Alpha Spectroscopy Results of Trench Soil Samples – OU2 RFI/RI

(Cont.)

Location	Location   Easting   Northing	Northing	Sample	Sampling	၁ဗ	Analyte	Result	Units Qual	Qual	Tier	Tier II
				Interval (cm)						SOR	SOR
TR09	2086350	748432 TR0	TR00299WCU2	3-6	REAL	Am-241	22.2800	pCi/q		0.251	1.422
					REAL	Pu-239/40	204.4000	pCi/g	_		
		,			REAL	U-233,-234	2.0480	pCi/g			
					REAL	U-235	0.0439	pCi/q		- ,	
					REAL	U-238DA	1.6620	pCi/g			
TR11	2086830	748455	748455 TR00284WCU2	0-3	REAL	Am-241	15.5600	pCi/g		0.139	0.785
					REAL	Pu-239/40	88.6500	pCi/g		_	
					REAL	U-233,-234	1.6220	pCi/g			
					REAL	U-235	0.0796	pCi/g	7		
		•			REAL	U-238DA	1.5400	pCi/g			
			TR00283WCU2	3-6	REAL	Am-241	8.3860	pCi/g		0.081	0.461
					REAL	Pu-239/40	53.9900	pCi/g		-	
					REAL	U-233,-234	1.4840	pCi/g			
					REAL	U-235	0.0921	pCi/g	7		
					REAL	U-238DA	1.7660	pCi/g			- · ·
TR12	2087340	749045	749045 TR00267WCU2	0-3	REAL	Am-241	34.1700	pCi/g		0.577	3.271
			,		REAL	Pu-239/40	591.2000	pCi/g			
					REAL	U-233,-234	1.0140	pCi/g			•
					REAL	U-235	0.1239	pCi/g	7		
					REAL	U-238DA	1.8320	pCi/g			
		<u> </u>	TR00266WCU2	3-6	REAL	Am-241	13,5300	pCi/g		0.131	0.743
					REAL	Pu-239/40	93.0900	pCi/g	٠		
',''			-		REAL	U-233,-234	0.7726	pCi/g			
					REAL	U-235	0.0323	pCi/g	7		-
					REAL	U-238DA	1.3680	pCi/g			
SOR = Sum of ratios		Source: DOE	E 1995								

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Table 2-7 Alpha Spectroscopy Results of Surface Soil Samples – HPGe Double Sampling Locations

HPGe Measurement	Easting	Northing	Am-241	Ъ	<b>5</b>	U-235	U-238	Tier1	Tier II
			(Band)	(B/15d)	(b/Ci/g)	(b/i)	(pCi/g)	SOR	SOR
30	2087180.071	749564.78	3.503	18.850	0 784	0.075	1 128	CO	0 7 0
104	2086540 732	748734 16	26.004	_		0.0	1.120	0.0	0.18
100	10000	10.01.10	20.301	133.143	0.899	0.0/2	1.315	0 22	1 26
507	2086703.63	749219.19	46.381	143 322		0.083	1 172	0.00	200
266	2008716 002	740040 50	077			0.00	7/4.1	0.32	Ö.
001	2000/10.303	149249.32	20.113			0.026	0.915	0 18	1 05
305	2087381,285	749310 79	10 880	E7 E70				2	3
907	0000010000	10010	0.00	710.10	0.787	0.041	1.108	0.0	0.53
400	7086548.208	749086.09	73.682	533,855	0 804	0.077	1 671	0.70	00
460	2086554 OF	740006 50	404475	1	5	5.0	1.0.1	0.72	4.08
2	2000004.00	149020.33	134.175	/82./90	0.967	0900	2 197	1 18	22.2
699	2085947.078	748667.47	53.166		0.748	8000	1 400	- 0	0.0
					2	0.040	001.	04.0	7/7

Radionuclide results reported as the weighted averages over the HPGe measurement's field of view. SOR = Sum of ratios. Table 2-8 Alpha Spectroscopy Results of Surface Soil Samples – Actinide Migration Evaluation Project

NA = Not analyzed SOR = Sum of ratios. Source: RMRS, 1998f

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and extend to the east encompassing locations TR12 and AME 5398 (also Tier II exceedances). Also, unlike the 95% UCL results (Figure 2-8), the "best fit" results (Figure 2-7) indicate actinide levels below Tier II to the north at HPGe Measurement Location 30, to the east at HPGe Measurement Location 305, and southeast at TR11. Thus, RSAL exceedances for the "best fit" line (Figure 2-7) are most consistent with the historical and the alpha spectroscopy data, and the best fit line is the chosen model to standardize the HPGe results.

# 2.2.2.2 Alpha Spectroscopy/HPGe <sup>235</sup>U, <sup>238</sup>U Correlations

As shown in Figures 2-10 and 2-11, correlations for the alpha spectrometry/HPGe data for <sup>235</sup>U and <sup>238</sup>U were not performed because in both cases the uranium isotopes were not detected by *in situ* HPGe. The plots show minimum detectable activities when the isotopes were non-detected. Also, alpha spectrometry did not measure detectable levels of <sup>235</sup>U, and only in a few instances was <sup>238</sup>U detected at estimated activities. Therefore, <sup>235</sup>U and <sup>238</sup>U results from the HPGe survey in the Americium Zone were used directly as the surface soil radiological data for these isotopes. The lack of correlation for the uranium data does not impact the findings reported herein because the activities of uranium isotopes are well below the Tier II RSALs throughout the investigation area.

The activity of <sup>233/234</sup>U was calculated based on the fact that <sup>234</sup>U should be in equilibrium with <sup>238</sup>U (the activity contribution of <sup>233</sup>U is insignificant). The equilibrium between the radioactive parent (<sup>238</sup>U) and daughter (<sup>234</sup>U) suggests the activity ratio between these two isotopes should be 1.0. Surface soil data collected in support of the OU2 Phase II RFI/RI supports this relationship with an average activity ratio of 0.97 between the two isotopes. Therefore, the activity of <sup>233/234</sup>U in surface soil was assigned the value measured by the HPGe survey for <sup>238</sup>U.

# 2.2.3 FIDLER Surveys

A FIDLER survey was conducted in a selected area where an isolated HPGe measurement exceeded the 10 pCi/g <sup>241</sup>Am decision level. The FIDLER survey was conducted at HPGe measurement location 301 to determine if the measurement result was caused by the presence of a smaller area containing a hot spot. In addition, two FIDLER surveys were conducted at HPGe measurement locations 460 and 462 where HPGe measurements exceeded the RFCA Tier I

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RSALs based on preliminary results using the sum-of-ratios methodology. The purpose of the survey was to determine whether contamination was homogeneous and widespread as suggested by the conceptual model, or heterogeneous and consists of numerous individual hot spots.

A grid with four-foot spacings was staked in the field to encompass the circular FOV for the HPGe measurement. A total of 37 FIDLER measurements were collected from each selected HPGe measurement location. FIDLER measurements were taken with the instrument placed on the ground surface at each of the four-foot grid nodes for a one-minute count. FIDLER surveys were conducted in accordance with Radiological Safety Procedure, 3-PRO-112-RSP-2.01, Job Aid: 4-JOB-010-RSP-02.01.07, Bicron FIDLER (Kaiser-Hill, 1999b).

#### 2.3 SUBSURFACE SOIL INVESTIGATION

The subsurface soil investigation consisted of two phases. One phase was the radiological investigation consisting of shallow boreholes. The second phase consisted of the VOC investigation.

# 2.3.1 Radiological Investigation

Subsurface soil sampling for radiological characterization was conducted at the 903 Pad and Lip Area. The depth of radiological contamination is required to estimate the volume of soil requiring remedial action. Figure 2-12 provides the radiological subsurface sampling locations for the 903 Pad and Lip Area. Samples were analyzed for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/244</sup>U, <sup>235</sup>U, and <sup>238</sup>U using alpha spectrometry. Boring logs are presented in Appendix A.

903 Pad - Twenty-five shallow boreholes were drilled for the characterization of radionuclide contamination beneath the 903 Pad. Twenty-five boreholes over the 3.4-acre 903 Pad represents a borehole completed at each node of a 23 m by 23 m (75 ft by 75 ft) grid (Figure 2-12). Subsurface soil samples were collected from artificial fill material and natural soils beneath the 903 Pad for radiochemical analysis utilizing a single-tube Geoprobe hydraulic push drilling technique. Soils were continuously cored to a total depth of approximately 1.2 m (4 ft) to ensure core recovery or to a depth where the FIDLER indicated less than 5,000 cpm. Samples were

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collected at approximately 15 cm (6 in) intervals or as appropriate so that the sample intervals coincide with asphalt, artificial fill material, and natural soils. This was done to prevent potential dilution of the natural soil samples below the artificial fill material. Borings and core were checked by engineer's tape for total depth and recovery. Samples for radiological screening were collected as a composite sample from the radiological sample. Soil samples were screened for alpha, beta/gamma, and VOCs using portable field instruments. If VOCs were detected above 10 parts per million by field instrumentation at any sampling location, the VOC subsurface soil sampling program, as described in the SAP (RMRS, 1998a), was implemented to characterize VOC contamination at that location.

Subsurface soil samples for radiochemical analysis were also collected during the VOC subsurface investigation as described in Section 2.3.2. Soil samples were collected from 12 original and three "step-out" boreholes on the 903 Pad, one borehole west of the 903 Pad, and one borehole east of well 07191 in the Lip Area (see Figure 2-13).

Lip Area - A total of thirty-seven boreholes were completed over the Lip Area where artificial fill was placed in 1970 and where surface soils were remediated in 1976, 1978, and 1984. Of the 37 boreholes, 25 borings were original and twelve were "step-out" borings (Figure 2-12). Of the 37 boreholes, two boreholes were completed in the 1976 remediation area, six boreholes were completed in the 1978 remediation area, and three boreholes were placed in the 1984 remediation area.

Shallow soil borings located in the 903 Lip Area and soil samples were collected utilizing single-tube Geoprobe hydraulic push drilling technique. Soils were continuously cored to either a total depth of 0.9 m (3 ft) or 1.2 m (4 ft) to ensure core recovery, or to a depth where the FIDLER indicated less than 5,000 cpm. Samples were collected at approximately 15 cm (6 in) intervals or as necessary so that the sample intervals coincide with artificial fill material and natural soils. This was done to prevent potential dilution of the natural soil sample below the artificial fill material. Borings and core were checked by engineer's tape for total depth and recovery. Samples for radiological screening were collected as a composite sample from the radiological sample. Soil samples were screened for alpha, beta/gamma, and VOCs using portable field instruments.

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A detailed surface soil characterization using HPGe was not performed in portions of the Lip Area where surface/subsurface soils were collected (RMRS, 1998a).

#### 2.3.2 VOC Investigation Boreholes

Investigation of VOC contamination at the 903 Pad, completed per the SAP (RMRS, 1998a), targeted the highest areas of groundwater contamination as well as the anomalous PCE soil gas results, east of groundwater well 07191. Figure 2-13 shows the borehole locations for the VOC investigation. Samples were analyzed for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/244</sup>U, <sup>235</sup>U, and <sup>238</sup>U using alpha spectroscopy and for VOCs using EPA Method 8260B (EPA, 1986). Boring logs are presented in Appendix A.

Subsurface soil sampling was conducted near existing groundwater monitoring wells 06691, and 08891 using an upgradient radial placement geometry with the well location serving as the downgradient location. Boreholes were located approximately 20 ft to the north, south, and west of well locations 06691, and 08891. Six boreholes were placed along the west to northwest side of the 903 Pad on the basis of aerial photographs showing drum storage and surface staining. A total of 15 boreholes were required to investigate the VOC contamination at the 903 Pad, the original 12 boreholes, two "step-out" boreholes (95998 and 97698), and one completion of a shallow subsurface radiological borehole (90998) as a VOC borehole (96498) where VOCs were observed with concentrations greater than 10 percent of the respective current Tier I SSALs.

The soil gas anomaly in the Lip Area at the southeast corner of the 903 Pad adjacent to well 07191 was evaluated. One borehole (97298) was located 20 ft east and 10 ft south of well 07191. A surface area with little or no vegetation and FIDLER readings greater than 10,000 cpm was identified 30 feet east of well 6591, adjacent to the west side of the 903 Pad. One borehole (92598) was completed to evaluate this area.

Soil samples were collected from VOC soil borings located in the 903 Pad and Lip Area utilizing a dual-wall Geoprobe hydraulic push drilling technique. Boreholes were advanced from the surface to either a depth of 0.31 to 0.62-m (1 to 2 feet) below the top of bedrock, or to a depth below the vertical extent of VOC contamination (based on field instruments), whichever was

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greater, provided refusal of the Geoprobe drilling equipment was not encountered. Samples were collected at approximately 1.22-m (4 ft) intervals below ground surface, or at intervals where VOCs were detected with field instrumentation. In general, the VOC samples were collected from approximately the lower 15-cm (6 in) interval and the radiological sample was collected from the 15-cm (6 in) interval above the VOC sample. Samples for radiological screening were collected from the 15-cm (6 in) interval above the radiological sample. Because of the different ionization potential between PCE and CCl<sub>4</sub>, two photoionization detectors were used (10.4 and an 11.7 electron volt bulb). If VOCs were detected above 10% of the current Tier I SSALs, then the sampling grid was extended an additional 6.1-m (20 ft) in an upgradient direction of that location, and additional samples were collected for laboratory analysis.

#### 2.4 903 PAD ASPHALT SAMPLES

Asphalt samples from the 903 Pad were collected to obtain preliminary waste characterization data for disposal purposes. Nine asphalt samples were collected randomly from the following locations over the 903 Pad: 90098; 90198; 90398; 90698; 90798; 91198; 91298; 91898; and 91998 (Figure 2-12). Random sampling techniques are appropriate methods for estimating the population mean and the standard error of this estimate. Locations were determined randomly based on the 903 Pad subsurface soil sampling grid. Samples were collected using a Geoprobe® and analyzed for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/234</sup>U, <sup>235</sup>U, and <sup>238</sup>U using alpha spectroscopy.

# 2.5 WORK CONTROLS

Field activities were conducted in accordance with the procedures detailed in the SAP (RMRS, 1998a), the Task-Specific Health and Safety Plan (RMRS, 1998b) and additional controls summarized herein. Additional work controls implemented for the project included the ALARA Job Review (#903Pad-98-001) for fieldwork performed under job-specific Radiation Work Permits (RWPs). Contamination control included measurement of direct and removable contamination levels on equipment, wind speed monitoring (soil handling activities suspended with two consecutive 15-minute wind speed average of 15 miles per hour), high volume air sampling during soil handling activities, and requirements for personal protective equipment. Fieldwork also could not be performed due to sensitivity of the radiological field instruments

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when the humidity was greater than 90% and ambient temperatures less than 32 degrees Fahrenheit.

# THIS TARGET SHEET REPRESENTS A FOLD-OUT MAP

(The map has been filmed and is placed at the end of the document)

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Figure 2 - 1

# **HPGe Measurement Location Map**

Map ID: 99-0408

September 24, 1999

U.S. DEPARTMENT OF ENERGY ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

ROCKY MOUNTAIN REMEDIATION SERVICES, L.L.C. GOLDEN, COLORADO

AR Document Number: \_\_\_\_-\_

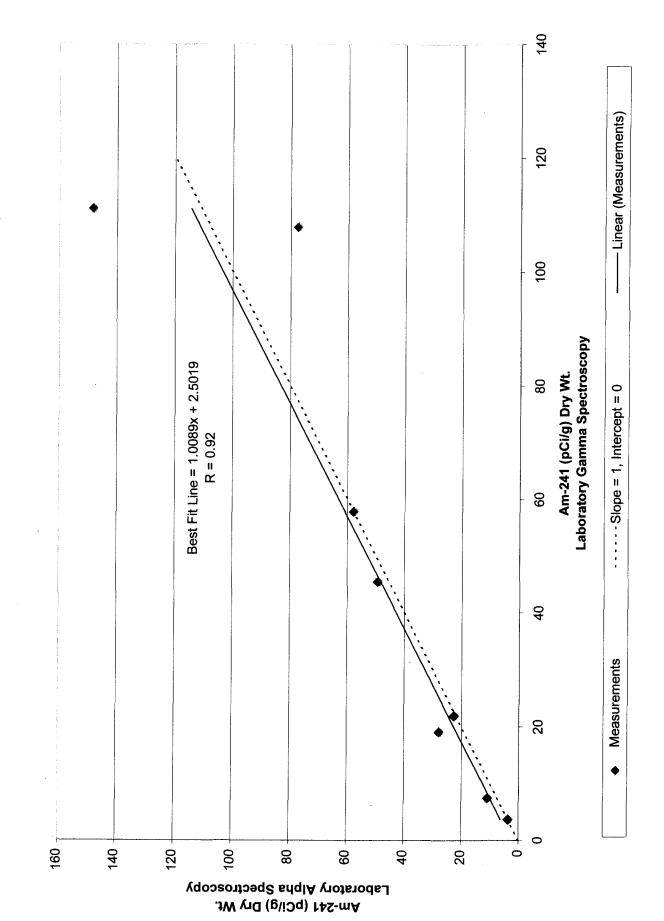
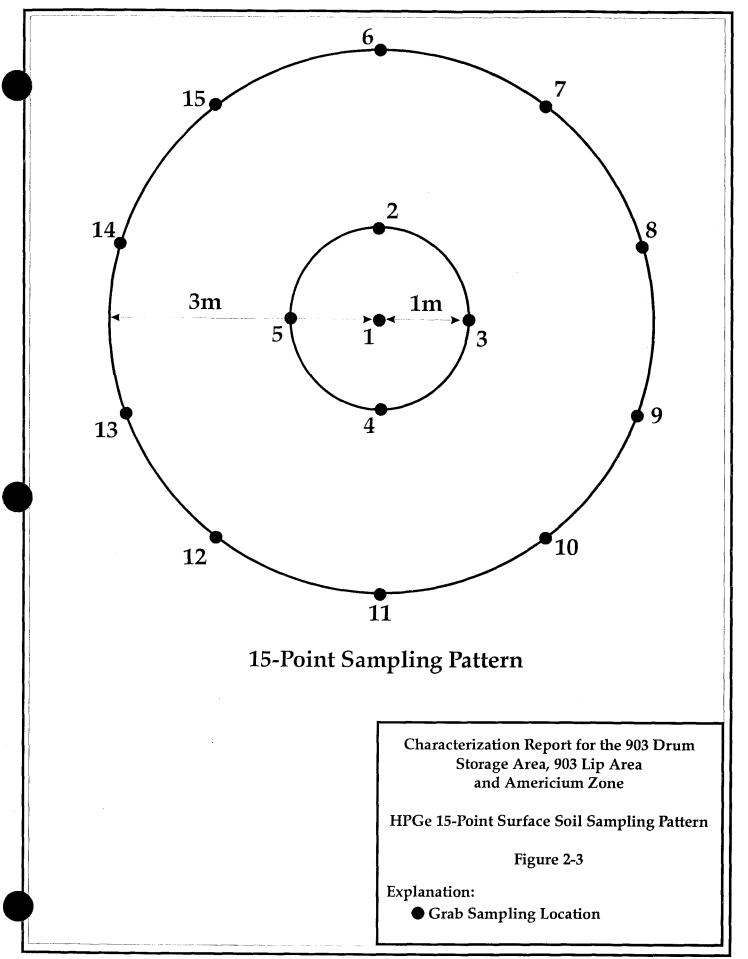


Figure 2-2 Americium-241 Activities in Soil - Gamma Spectroscopy vs. Alpha Spectroscopy Correlation



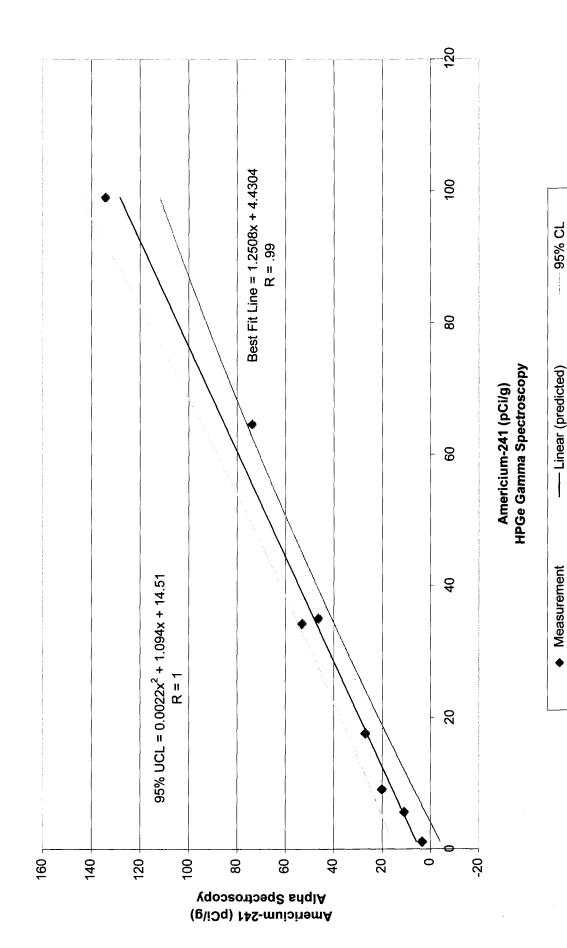


Figure 2-4 Alpha Spectroscopy vs. HPGe Gamma Spectroscopy - Americium-241 Correlation

--- Linear (predicted)

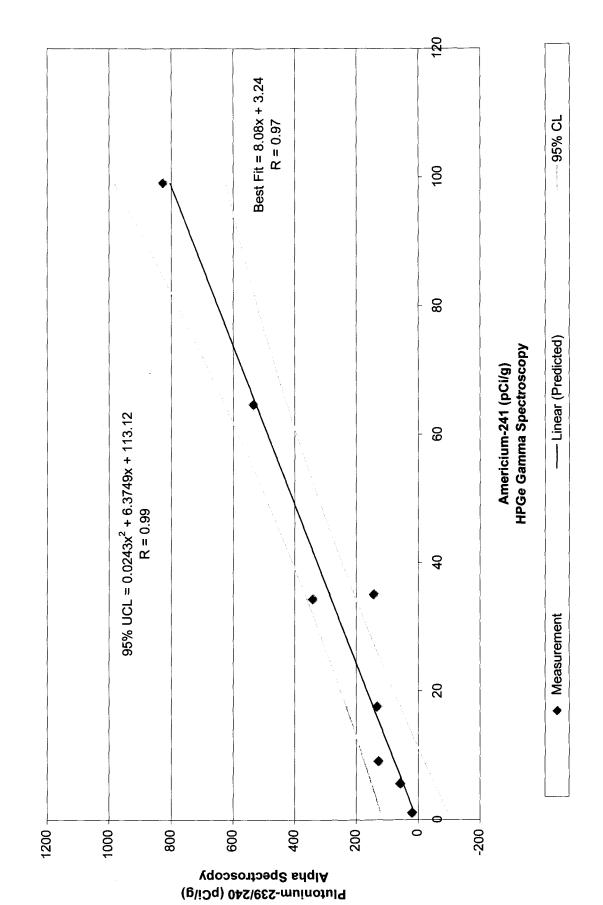


Figure 2-5 Alpha Spectroscopy vs. HPGe Gamma Spectroscopy - Americum-241 vs. Plutonium-239/240 Correlation

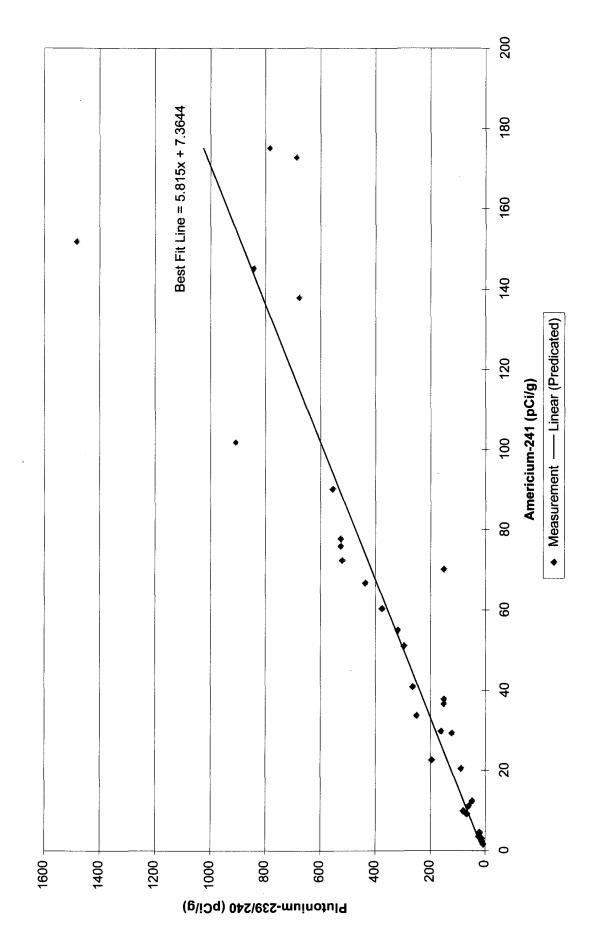


Figure 2-9 HPGe Survey Soil Sample Results- Plutonium239/240 vs. Americium-241 Correlation (Pu/Am Activity Ratio)

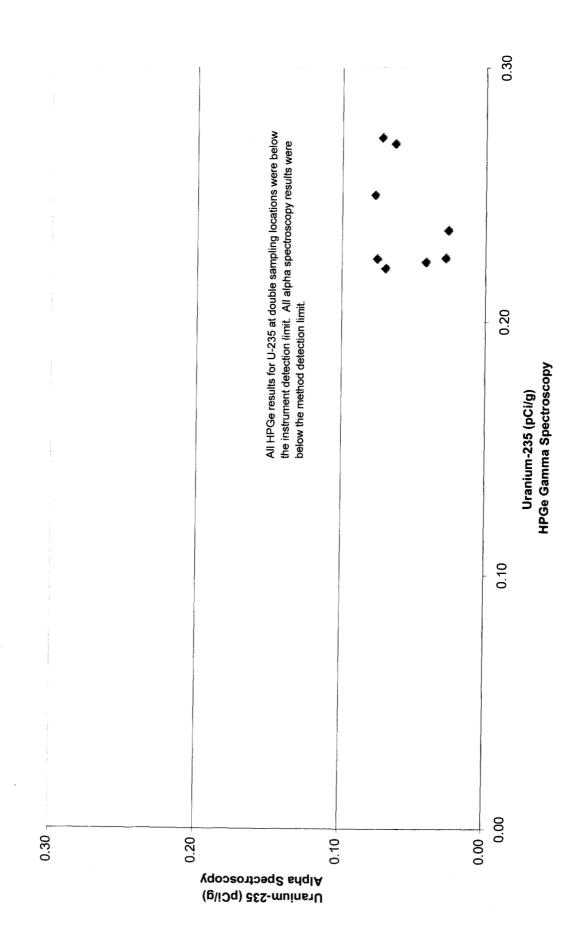


Figure 2-10 Alpha Spectroscopy vs. HPGe Gamma Spectroscopy - Uranium-235 Correlation

◆ Measurement

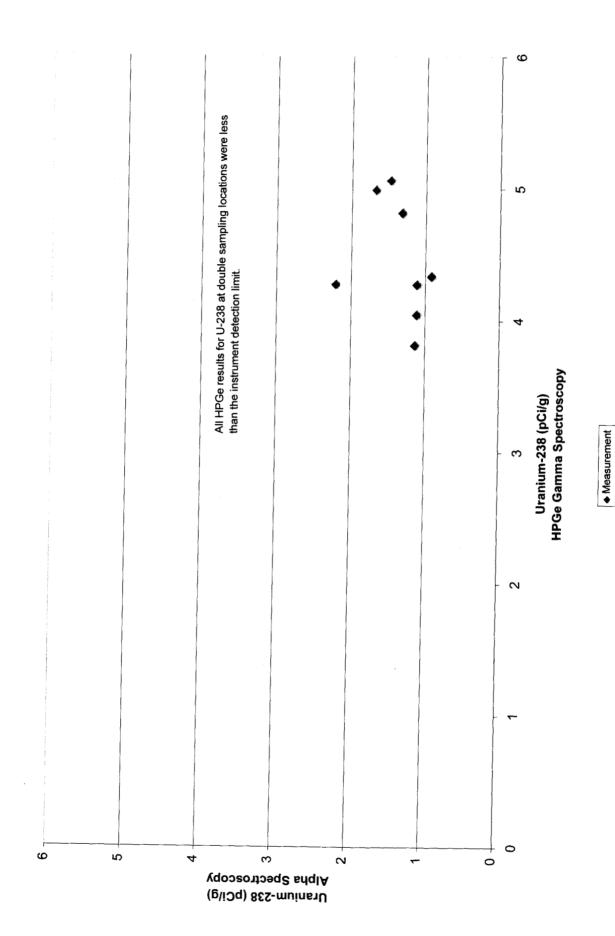


Figure 2-11 Alpha Spectroscopy vs. HPGe Gamma Spectroscopy - Uranium-238 Correlation

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# 3.0 DATA QUALITY ASSESSMENT

This section provides the results of the data quality assessment that was conducted in accordance with the Evaluation of Data for Usability in Final Reports (RMRS Procedure, ER/RMRS-98-200 [RMRS, 1998c]). This assessment ensures that data used in making management decisions for remedial actions is of adequate quality to support the decisions.

As discussed herein, Data Quality Objectives for the project were achieved. A summary of project DQOs and the corresponding project decisions is presented in Table 3-1.

Table 3-1 Sample Types & Data Quality Objectives

Sample Type	DQO	Decision
Actinides in Surface Soils using <i>In Situ</i> Gamma Spectroscopy.	Quantify spatial distribution of RFETS actinide activities that meet or exceed Tier I RSALs to estimate soil volumes requiring remediation. Quantify spatial distribution of <sup>241</sup> Am to 10 pCi/g using HPGe gamma ray survey.	Spatial extent of actinide activities exceeding Tier I RSALs. Volume estimates of soils exceeding Tier I and Tier II RSALs.
VOCs in Subsurface Soils.	Quantify three-dimensional distribution of VOC concentrations that meet or exceed Tier I Soil Action Levels to estimate soil volumes requiring remediation.	Three-dimensional extent of VOC concentrations relative to Tier I soil action levels. Volume estimates of soils exceeding Tier I soil action levels.
Actinides in Subsurface Soils.	Quantify three-dimensional distribution of actinides to estimate soil volumes requiring remediation.	Three-dimensional extent of actinide activities relative to Tier I & II RSALs. Volume estimates of soils exceeding Tier I and II RSALS.

# 3.1 VERIFICATION OF RESULTS

Verification ensures that data produced and used by the project are documented and traceable per quality requirements. Generally, verification consists of reviewing the data to determine whether:

- Chain-of-Custody was intact from initial sampling through transport and final analysis;
- Preservation and hold-times were within tolerance;
- Selected samples underwent analysis at certified labs; and
- Format and content of the data is clearly presented relative to goals of the project.

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In addition to the criteria noted above, verification of the data also included additional checks sometimes acknowledged as within the "validation" category, depending on the type of analysis:

- Surrogate recovery;
- MS/MSD recovery;
- Calibrations;
- · Blanks;
- Sample preparations; and
- Other quality control.

In order to provide an integrated evaluation of the data quality, results of the verification are collectively discussed with validation in Section 3.2.

#### 3.2 VALIDATION

Validation consists of a technical review of the data, or portion of the data, so that any limitations of the data relative to project goals are identified, and the associated data are qualified accordingly. Data were validated relative to the precision, accuracy, representativeness, completeness, and comparability (PARCC) parameters described in the next section. K-H Analytical Services Division also currently performs validation on a site-wide basis at 25% frequency. Satisfactory validation at this frequency indicates that the subcontracted labs are operating competently relative to industry-wide standards, and more specifically, that sample custody and analytical procedures are implemented under defined quality controls. Site-wide data validation coupled with annual lab audits provides the inference that all analytical and radiochemical results not specifically validated, are represented by the percentage that is validated.

Validation by an independent third party was performed on 37 percent of the alpha spectroscopy data and 32 percent of the VOC data, which exceeded the requirement of 25 percent validation by an independent third party. The remaining alpha spectroscopy and VOC data were verified by an independent third party. Original verification and validation (V&V) packages for the project are managed and filed by the K-H Analytical Services Division, Building 881.

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Verification and validation of the project data, summarized in Sections 3.1 through 3.3, included use of the following protocols and guidance:

- RMRS Procedure RF/RMRS-98-200, Evaluation of Data for Usability in Final Reports (RMRS, 1998c);
- USEPA Contract Laboratory Program National Functional Guidelines for Inorganic Data Review, EPA 540/R-94/013, (EPA, 1994b);
- USEPA Contract Laboratory Program National Functional Guidelines for Organic Data Review, EPA 540/R-94/012, (EPA, 1994a);
- Guidance for Data Quality Assessment, Practical Methods for Data Analysis, EPA QA/G-9, (EPA, 1996b);
- Kaiser-Hill Team Quality Assurance Program, Rev. 5, (K-H, 1997); and
- RMRS Quality Assurance Program Description (QAPD), RMRS-QAPD-001, Rev. 2, (RMRS, 1998d).

#### 3.3 PARCC PARAMETERS

#### 3.3.1 Precision

Precision is a measure of the reproducibility of results. Precision is evaluated by comparing results from field duplicate and/or replicate (duplicate/replicate) samples with results from associated real samples. Precision was evaluated quantitatively by using two functions, relative percent difference (RPD), and duplicate error ratio (DER), where the latter function is used to account for the stochastic nature of error of radioactivity.

Equations 3.1 and 3.2 present the RPD and DER equations

RPD = 
$$\frac{|C_1 - C_2|}{|(C_1 + C_2)/2|}$$
 (Eq. 3.1)

where:

C<sub>1</sub>=Concentration of the analyte in the real sample C<sub>2</sub>=Concentration of the analyte in the duplicate sample

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$$|C_1 - C_2|$$
DER = 
$$\frac{|C_1 - C_2|}{\sqrt{(TPU^2_{C1} + TPU^2_{C2})}}$$
where:
$$TPU = \text{total propagated uncertainty}$$
(Eq 3.2)

#### Duplicate/Replicate Sample Collection Methodology

Field duplicate samples collected in support of the surface soil programs were collected as unique samples. The duplicate samples were generated from grab samples of surface soils collected at HPGe measurement locations. The duplicate samples were collected adjacent to the real samples collected over the same HPGe FOV, composited, and placed into sample jars. Replicate and real samples of subsurface soils collected for alpha spectroscopy analysis were generated by splitting the recovered core in half lengthwise. VOC quality control (QC) samples are identified as duplicates because the real and QC samples were collected from adjacent depth intervals (i.e. not split).

The purpose of the field duplicate and replicates are to evaluate the precision of the field sampling process. The QC criterion for RPDs is  $\leq 40\%$ , and for DERs the criterion is  $\leq 1.96$ . Individual RPDs/DERs can be found in Appendix B. Duplicate/replicate samples exceeding the DER QC criterion of 1.96 are interpreted as different at the 5% level of significance. Duplicate/replicate samples exceeding the RPD QC criterion of 40%, indicate that precision does not comply with DQO specifications, and require an explanation and justification for deficiencies, and a determination if additional sampling is required. At least 85% of all quality control samples are required to comply with the established precision or RPD goals. The following sections describe the results of duplicate/replicate sample results for each laboratory analytical program.

#### In Situ Gamma Spectroscopy (HPGe) Program

The gamma spectroscopy unit collected a total of 1,110 in situ measurements. The required frequency of duplicate samples was one measurement for each set of 20 real measurements. A total of 58 duplicate measurements were collected (1 in 19.1) meeting the required collection frequency. All 58 duplicate measurements acquired were within error tolerances (DER  $\leq$  1.96) for <sup>241</sup>Am. This excellent performance by the *in situ* system indicates the large-area, physical-

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averaging is a repeatable method. Appendix B provides the TPU for HPGe measurements used in the DER calculations.

#### Laboratory Gamma Spectroscopy

A total of 24 real and nine duplicate surface soil samples (1 in 2.7) from three double sampling HPGe measurement locations were provided to the laboratory for gamma spectroscopy analysis for <sup>241</sup>Am. The frequency for duplicate sample collection for gamma spectroscopy analysis was met for this program. <sup>241</sup>Am activities were detected above the method detection limit in all samples. As shown in Table 3-2 two of the nine duplicate samples failed DER tolerances for an overall precision of 78%. Because DERs were calculated using the laboratory instrument's counting error as the only source of TPU, this overall precision is considered acceptable.

Table 3-2 Surface Soil Duplicate Assessment – Gamma Spectroscopy Results

Analyte	Total Real Samples Collected	Total Duplicates Collected	Number of Duplicates within DER	Overall Precision Compliance
<sup>241</sup> Am	24	9	7	78%

#### Laboratory Alpha Spectroscopy

As indicated in this section, the precision results for <sup>241</sup>Am and <sup>239/240</sup>Pu did not meet the project goal of 85% compliance. However, as discussed subsequently, the precision results do not compromise the objectives of the investigation.

#### Surface Soils

A total of 24 real and nine duplicate surface soil samples were collected from three double sampling HPGe measurement locations and were provided to the laboratory for alpha spectroscopy analysis for <sup>241</sup>Am, <sup>239/240</sup>Pu, and uranium isotopes. The frequency for duplicate sample collection for alpha spectroscopy analysis was met for this program. <sup>241</sup>Am activities were detected above the method detection limit in all samples. As shown in Table 3-3 eight of the nine duplicates failed DER tolerances for <sup>239/240</sup>Pu with an overall precision compliance of 11%. Five of the nine duplicates failed DER tolerances for <sup>241</sup>Am with an overall precision compliance of 44%. Uranium isotopes met the project's precision compliance goal. As with the laboratory

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gamma spectroscopy, DERs were calculated using the laboratory instrument's counting error as the only source of TPU.

Table 3-3 Surface Soil Duplicate Assessment - Alpha Spectroscopy Results

Analyte	Total Real Samples Collected	Total Duplicates Collected	Number of Duplicates within DER	Overall Precision Compliance
<sup>239/240</sup> Pu	24	9	1	11%
<sup>241</sup> Am	24	9	4	44%
233/234 U	24	9	8	89%
<sup>235</sup> U	24	9	9	100%
<sup>238</sup> U	24	9	8	89%

# Subsurface Soils

A total of 349 real and nineteen replicate surface and subsurface soil samples and asphalt samples were collected from boring locations and were provided to the laboratory for alpha spectroscopy analysis for <sup>241</sup>Am, <sup>239/240</sup>Pu, and uranium isotopes. The frequency for replicate sample collection (1 in 18.5) for alpha spectroscopy analysis was met for this program. As shown in Table 3-4, ten of the replicates failed DER tolerances for <sup>239/240</sup>Pu for an overall precision compliance of 44%. Six of the nineteen samples failed DER tolerances for <sup>241</sup>Am for an overall precision compliance of 68%. All uranium isotopes met the project's precision compliance goal. Again, DERs were calculated using the laboratory instrument's counting error as the only source of TPU.

Table 3-4 Radionuclide Subsurface Soil Replicate Assessment – Alpha Spectroscopy Results

Analyte	Total Real Samples Collected	Total Replicates Collected	Number of Replicates within DER	Overall Precision Compliance
<sup>239/240</sup> Pu	349	19	9	47%
<sup>241</sup> Am	349	19	13	68%
233/234 U	349	19	19	100%
<sup>235</sup> U	349	19	19	100%
<sup>238</sup> U	349	19	. 18	95%

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#### Discussion

One source of the apparent imprecision of the radionuclide data may be attributed to the exclusion of sources of uncertainty beyond the instrument counting error. The DER calculation incorporates TPU that includes all uncertainties introduced from sample collection in the field through radiological analysis. However, the only uncertainty included in the TPU for this data quality assessment is the counting error at the 2-sigma level. This reduction in uncertainty in the TPU term leads to an exaggerated number of samples exceeding the DER of 1.96.

Secondly, when comparing the gamma and alpha spectroscopy DER results there appears to be an increased error associated with analyzing only an aliquot (0.25 to 2.0 grams) of the sample using alpha spectroscopy versus analyzing the entire sample (gamma spectroscopy). The overall precision for <sup>241</sup>Am using gamma spectroscopy was 78% compared to 44% for alpha spectroscopy. Since the duplicate samples were collected from the same locations as the samples analyzed using gamma spectroscopy, a significant portion of difference in overall precision for <sup>241</sup>Am between these two methods may be attributed to the heterogeneous distribution of <sup>241</sup>Am on a small scale, as exemplified by this comparison.

This heterogeneity is also obvious by comparing the surface soil "duplicate" sample results (Table 3-3) to the subsurface soil "replicate" sample results (Table 3-4). As can be seen from the subsurface sample program, the overall precision of "replicate" samples for <sup>241</sup>Am and <sup>239/240</sup>Pu (47% and 68%, respectively) are higher than the overall precision of "duplicate" samples (<sup>241</sup>Am at 11% and <sup>239/240</sup>Pu at 44%). "Duplicate" samples were unique samples collected from adjacent locations whereas "replicate" samples for subsurface soils were splits from the same recovered core. The heterogeneous distribution of <sup>241</sup>Am and <sup>239/240</sup>Pu activities in surface soils is evident at these small intersample distances. Heterogeneity is also observed in the FIDLER survey results (Section 4.1.3).

Although it is clear that micro-scale heterogeneous distributions exist for <sup>241</sup>Am and <sup>239/240</sup>Pu activities in surface soil, the high degree of correlation between the lower precision alpha spectroscopy results and the higher precision HPGe gamma spectroscopy results indicate insignificant impact to the regression "model". With respect to subsurface soils, the distributions

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of <sup>241</sup>Am and <sup>239/240</sup>Pu activities do not indicate patterns anomalous to those expected from the site conceptual model and/or historical data.

#### Volatile Organic Compound Analysis (EPA 8260B)

A total of 86 real and five duplicate subsurface soil samples (1 in 17.2) were collected and provided to the laboratory for analysis of VOCs. Therefore, the frequency for duplicate sample collection for VOC analysis was met for this program. Table 3-5 provides the number of samples collected under this program and the results of the RPD for the duplicate assessment. One sample pair detected VOCs in both the duplicate and associated real sample. The four other RPD calculations were conducted on sample pairs that had VOC detections in the real samples but not in the associated duplicate sample. The method detection limit was used in RPD calculations when no detections were found in the duplicate sample. Overall precision compliance for the VOC investigation was 60% where two of five duplicate sample sets were observed to exceed the RPD of 40%. Although the relative percent differences in concentrations between the real duplicate samples for each of these analytes may be significant, the detected concentrations are all well below their respective current RFCA Tier I soil action levels, i.e. because of the relatively low magnitudes of the concentrations, imprecision does not affect overall project decisions relative to VOC contamination.

Table 3-5 Duplicate Sample Assessments – Volatile Organic Compound Analysis

Analyte	Total Real Samples Collected	Total Duplicates Collected	Number of Duplicates within RPD	Overall Precision Compliance
PCE	86	5	3	60%
TCE	86	5	3	60%
CCL₄	86	5	4	80%
1,2-DCE	86	5	3	60%

Although the overall precision compliance is less than project completeness goals, precision of the VOC results is acceptable. The apparent imprecision noted is limited to values well below the Tier I soil action levels (i.e., between detection limits and 10% of Tier I soil action levels), and, as such, does not impact project decisions relative to nature and extent of VOC contamination in the soil.

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# 3.3.2 Accuracy

Accuracy is a measure of how closely an analytical or survey result corresponds to the true concentration or activity in a sample. Systematic uncertainties that affect accuracy, also known as bias, are also discussed in this section.

#### In Situ Gamma Spectroscopy

The accuracy of *in situ* gamma spectroscopy is corroborated through two methods of validation implemented for the project: systematic validation, and more importantly, performance validation, that is, through the use of comparing and correlating surface soil samples analyzed by laboratory alpha spectroscopy. The quality of the correlation, which exhibited a high correlation coefficient for linearity (Figure 2-5), validate the entire gamma spectroscopy measurement system relative to the site-specific matrix types and radiological levels of interest.

The systematic validation of gamma spectroscopy results yielded no significant qualifications to the data. Detailed technical considerations and their effects on data quality are further detailed in the Appendix C under "903 Pad In-Situ Models and Uncertainties".

Another measure of accuracy is determined by comparing the detection limit proposed to the actual detection limit reported for the sample results. Table 3-6 provides a comparison of detection limits for the *In Situ* Gamma Spectroscopy program.

Table 3-6 Comparison of Detection Limits – In Situ Gamma Spectroscopy

Analyte	Required Analytical Method	Required Detection Limit (pCi/g)	Actual Detection Limit (pCi/g)
<sup>241</sup> Am	In Situ Gamma Spectroscopy	1.0	0.38 - 1.43
<sup>235</sup> U	In Situ Gamma Spectroscopy	0.5	0.36 - 0.72
<sup>238</sup> U	In Situ Gamma Spectroscopy	5.0	1.31 – 6.49

As can be seen in Table 3-6 the lower limit of the actual detection limit was met for all three radionuclides. The required detection limit was exceeded for <sup>241</sup>Am and <sup>238</sup>U in a limited number

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of analyses; however, these exceedances do not significantly impact the results of the HPGe survey nor the resulting volume estimates.

#### Laboratory Alpha Spectroscopy

The accuracy of laboratory alpha spectroscopy data was evaluated with respect to detection limits. Table 3-7 provides a comparison between required detection limits and actual detection limits.

Table 3-7 Comparison of Detection Limits - Alpha Spectroscopy

Analyte	Required Analytical Method	Required Detection Limit (pCi/g)	Actual Detection Limit (pCi/g)
<sup>239/240</sup> Pu	RC01B001	0.3	0.028 - 0.122
<sup>241</sup> Am	RC01B001	0.3	0.0061- 0.168
<sup>233/234</sup> U	RC01B001	1.0	0.015 - 0.472
<sup>235</sup> U	RC01B001	1.0	0.016 - 0.472
238U	RC01B001	1.0	0.008 - 0.643

As can be seen in Table 3-7 the actual detection limit was lower than the required detection limit for all radionuclides. Therefore, accuracy from alpha spectroscopy detection limits were adequate for all sample analyses for decision making purposes.

#### Volatile Organic Compound Analysis (EPA 8260B)

The accuracy of VOC data was evaluated with respect to detection limits. Table 3-8 provides a comparison between required detection limits and actual detection limits.

The method detection limit was revise during the VOC Subsurface Investigation from the midlevel detection limit (740 ug/kg) specified in the SAP (RMRS, 1998b) to a low-level detection limit (5 ug/kg). The required detection limit of 740 ug/kg was exceeded for the target analytes in all samples from boring 96498, and in one sample each from borings 96198 and 96298. The detection limit exceedance in samples from boring 96498 was due to sample analysis using the VOA-CLP, mid level method. However, the actual detection limit is lower than the current Tier I soil action levels for VOCs and therefore did not impact decision making based on current SSALs. Site Characterization Report for the
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Table 3-8 Comparison of Detection Limits - Volatile Organic Compound Analysis

Analyte	Required Analytical Method	Required Detection Limit (ug/kg)	Actual Detection Limit (ug/kg)
Carbon Tetrachloride	8260B	740	5.0 – 1500
Chloroform	8260B	740	0.1 – 1500
Cis-1,2- dichloroetherne	8260B	740	0.1 – 1500
Methylene Chloride	8260B	740	. 1.4 – 1500
Tetracholorethene	8260B	740	0.41 - 1500
Trichloroethene	8260B	740	0.31 - 1500

During review of the data the following biases were noted that cause the data to be qualified. Two other types of QC samples were generated in support of the VOC subsurface soil investigation; equipment rinse blanks and trip blanks. Table 3-9 provides a QC summary for methylene chloride detected in an equipment rinse blank and the associated real samples. Per EPA guidance (EPA, 1989) the methylene chloride detections in the real samples are less than ten times the detection in the associated equipment rinse blank and will be qualified as non-detect. Although trip blanks were submitted and analyzed with real samples, no qualifications were required for the associated real samples.

Methylene chloride was detected at estimated (J) concentrations in 16 samples (0.59 J to 410 J ug/Kg) at less then the method reporting limit. However, the maximum detected concentration in a method blank from the entire sample data set is 860 ug/Kg. Using EPA guidance (EPA, 1989) the concentration in the samples do not exceed ten times the maximum amount detected in any blank. Therefore, methylene chloride detections are considered a result of laboratory contamination.

Acetone was not detected in the associated rinse or method blanks in several samples from boring 97698 (99A8275), however, acetone may not be present in the sample because the continuing calibration verification criteria were not met. Acetone was detected in samples from boring 96398 (99A4102) (ranging from 1,200 up to 3,300 ug/Kg). However, the maximum detected concentration in a method blank from the entire sample data set is 670 ug/Kg. Using EPA guidance (EPA, 1989) the concentration in the samples do not exceed ten times the maximum

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amount detected in any blank. Therefore, acetone detections are considered a result of laboratory contamination.

Table 3-9 Quality Control Sample Summary

QC Sample ID	QC Sample Type	Assoc. Real Sample(s)	Analyte(s) Detected in QC Sample	Detect in Real Samples Associated Method Blank (yes/no)	Comments
99A6650- 007.002	equipment rinse	99A6650- 002.002	Methylene chloride	no	Methylene chloride detections in field
	blank	99A6650- 003.002		no	samples <10 times the detection in the QC
		99A6650- 004.002		no	sample. Result will be qualified as non-detect (U) (EPA, 1989).
		99A6650- 005.002 99A6650-		no	(0) (21 A, 1909).
		006.002		no	

The compound trichlorotrifluoroethane was detected in several samples from borehole 97698 (99A8275). Detections of trichlorotrifluoroethane are not considered repeatable as the dilution results for this sample indicated trichlorotrifluoroethane was no longer present. The results were assigned the J148 qualifier, as the associated value is estimated and the linear range of the measurement system was exceeded. Results were then adjusted with the dilution Contract Required Quantitation Limit and given the qualifier UD, the associated value is considered undetected at an elevated level of detection.

PCE was detected in two samples from boring 95998, at 1,540 ug/kg and 343 ug/kg with an E (estimated) qualifier. When re-analyzed by the lab the PCE results were 3,060 ug/kg and 174 ug/kg, respectively, with a D qualifier (dilution).

Qualifications of VOC data did not affect accuracy or project decision making. VOC samples were analyzed using an expedited turn-around to assist field decisions based on "Form-1's" faxed from the laboratory. Although VOC detection limits varied during the course of the project, the detection limits were lower than the current Tier I soil action levels for VOCs and therefore did not impact decision making based on these action levels.

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# 3.3.3 Representativeness

Representativeness is evaluated by comparing the number and types of samples identified in the SAP with the number and type of samples actually collected. The number of samples required was based on meeting the DQOs of the characterization. Table 3-10 provides a comparison of planned samples vs. actual samples collected in support of the investigation. Table 3-11 provides a comparison of QC samples and real samples collected for the investigation.

As can be seen from Table 3-10, all areas met or exceeded planned sample requirements with the exception of the HPGe survey in the Lip Area and characterization of the asphalt and fill at the 903 Pad by alpha spectroscopy. Surface soils in the Lip Area were characterized by twenty borings completed during the subsurface radiological program. Sample results collected from the 0-6 inch interval were used to characterize surface soils in this area. Asphalt and fill samples were to be collected at all 25 boring locations within the 903 Pad. This number of samples was later determined to be excessive and the SAP was revised to include the collection of samples at nine randomly selected locations.

As can be seen from Table 3-11, the collection frequency of quality control samples was met for all analytical programs with the exception of trip blanks. Detections of VOCs in soil samples shipped without trip blanks are considered actual detections except where qualified previously as a laboratory contaminant.

#### 3.3.4 Completeness

Completeness is typically expressed as a percentage, calculated as a ratio of usable results to the number of samples collected. One hundred percent of the data were verified at the project level based on comparing usable data with unusable data (RMRS, 1998c). Completeness is 100% exceeding the project's goal of 90%. Additional sampling is not required to meet the project objectives of estimating soil volumes exceeding current action levels and characterizing surface soils to 10 pCi/g <sup>241</sup>Am.

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Table 3-10 Planned vs. Actual Sample Comparison

Area (Program)	Analysis	Planned No. of Samples (per SAP)	Actual Number of Samples Collected	Deviation	Justification
Lip Area and Americium Zone	In Situ Gamma Spectroscopy	1,200	1,110	-90	Borehole samples from 0  – 6 inch interval were used to characterize Lip Area east of the 903 Pad. This deviation from the SAP was approved by the agencies.
Americium Zone Surface Soils	Alpha Spectroscopy and Gamma Spectroscopy	18 from 6 FOVs	24 from 8 FOVs	+6	Collected samples from two additional FOVs for correlation of HPGe samples and field quality control locations.
903 Pad Radiological	Alpha Spectroscopy	150	107	-43 -	Original estimate erroneously included samples of asphalt and fill for 25 boreholes. Reduced number of fill samples to same frequency as asphalt samples. This deviation from the SAP was approved by the agencies.
903 Pad Asphalt	Alpha Spectroscopy	9	9	0	
903 Pad VOC (Subsurface VOC)	Alpha Spectroscopy	72	76	+4	Collected additional samples as a result of "stepout" borings.
903 Pad VOC	VOC	72	77	+5	Collected additional samples as a result of "stepout" borings.
903 Lip Area Radiological	Alpha Spectroscopy	100	148	+48	Collected additional samples as a result of "stepout" borings.
903 Lip Area VOC	Alpha Spectroscopy	6	9	+3	Collected additional samples as a result of "stepout" borings.
903 Lip Area VOC	VOC	6	9	+3	Collected additional samples as a result of "stepout" borings.

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Table 3-11 QC Sample Type, Quantity

Sample Type (Program)	Analysis	Number of Investigative Samples	Number of Duplicate/ Replicate Samples	Number of Rinse Blank Samples	Number of Trip Blank Samples
Americium Zone Surface Soils (HPGe)	Alpha Spectroscopy	24	9	3	
Americium Zone Surface Soils (HPGe)	Gamma Spectroscopy	24	9	0	
903 Pad Radiological (Subsurface)	Alpha Spectroscopy	107	6	4	
903 Pad Asphalt (Subsurface)	Alpha Spectroscopy	9	1	. 0	
903 Pad VOC (Subsurface)	Alpha Spectroscopy	76	4	4	
903 Pad VOC (Subsurface)	VOC	77	4	3	2
903 Lip Area Radiological (Subsurface)	Alpha Spectroscopy	148	8	10	
903 Lip Area VOC (Subsurface)	Alpha Spectroscopy	9	0	0	
903 Lip Area VOC (Subsurface)	VOC	9	1	2	1
Project Totals	Alpha Spectroscopy	373	28	21	
	Gamma Spectroscopy	24	9	0	
	voc	86	5	5	3

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#### Deviations

Despite weather constraints and field activities conducted non-sequentially among the subsurface investigations of the 903 Pad, Lip Area, and the VOC program, quality control samples were collected at a frequency of one in 20 during the entire subsurface investigation. Trip blank samples for VOC samples were reduced to a frequency of one trip blank for every 20 real VOC samples, detections not associated with a trip blank will be considered actual detects. Two of the required VOC trip blank samples were missed. This deviation from the SAP is justifiable as the analytical data is adequate to characterize subsurface soil and thus is representative of the subsurface soil conditions. Gamma spectroscopy analysis of aqueous samples could not be performed on rinse blank water samples. Two of the VOC investigation boreholes were not completed to bedrock due to refusal of the geoprobe sampling equipment at boreholes 96798 and 97698. Data collected from these boreholes are adequate and representative of subsurface soil conditions.

### 3.3.5 Comparability

All results presented are comparable with historical sampling and analyses results. This comparability is based on standard methods (EPA-approved methods), systematic quality controls, and thorough documentation of the planning, sampling, and analysis process.

The comparability of two samples were questioned during the investigation. One sample from HPGe measurement location 104 at 3 meters (98A5590-001.006) was reanalyzed as sample 98A5590-004.001 because <sup>241</sup>Am results from the first analysis were elevated and not comparable to the other sample results collected at this location. One alpha spectroscopy sample result from boring 94298 (98A2014-001.002) was rejected due to the MDA exceeding the RDL. However, sample results are reported high and are comparable to other Native 1 soil radiological results and therefore are usable. The remaining soil samples results are comparable because consistent sample collection activities and analysis were performed in accordance with the SAP (RMRS, 1998) and procedures described in Section 2.0.

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# 3.3.6 Sensitivity

Sensitivity was evaluated by comparing actual quantitation limits of the results with the regulatory or project-specific action levels required for decision-making. All analytical and radiological methods achieved adequate sensitivities based on quantitation limits well below regulatory thresholds, typically with a quantitation limit at less than 50% of the threshold.

# 3.3.7 Summary

In summary, the data sets acquired and evaluated for the 903 Pad Project were satisfactory for supporting the Data Quality Objectives proposed in the SAP. The following project objectives were achieved:

- 1) Defining actinide activities that exceed 10 pCi/g <sup>241</sup>Am in surficial soils;
- 2) Defining actinide activities in surface and subsurface soil that exceed Tier I and II RSALs; and
- Defining VOC concentrations in subsurface soil that exceed current Tier I SSALs.

Although not required by the SAP, an additional evaluation was performed to define VOC concentrations in subsurface soils that exceed proposed Tier I and Tier II SSALs (Kaiser-Hill, 1999b). However, proposed Tier II SSALs are below the required detection limit for VOCs identified in the SAP (Appendix D). Although subsurface soils have been characterized with respect to the proposed Tier I SSALs, not all soils have been characterized with respect to proposed Tier II SSALs. Therefore, areas exceeding proposed Tier II SSALs may be underestimated.

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# 4.0 NATURE AND EXTENT OF CONTAMINATION

The nature and extent of soil contamination related to releases from the 903 Pad has been evaluated by analysis of radionuclide and chemical data obtained as described in Section 2. The primary objective of the investigation is to determine the areal extent and depth of radiological and organic contamination above Tier I RSALs and Tier I SSALs, respectively. Another objective of the investigation was to characterize <sup>241</sup>Am in surface soils to 10 pCi/g using gamma spectroscopy field instrumentation. This characterization would allow for identification of surface soils exceeding Tier II RSALs. Remedial alternatives will be evaluated in the IM/IRA decision document based on these criteria.

Detailed descriptions of contamination in surface and subsurface soil are presented in this section. Results of the HPGe survey of the Americium Zone are presented in Section 4.1. Sections 4.2 and 4.3 respectively summarize radionuclide and VOC soil data collected for the 903 Pad and Lip Area. Descriptive summary statistics of the data are presented in Appendix D. Electronic copies of analytical results and Tier I and Tier II RSAL calculations are provided in Appendix E.

#### 4.1 SOIL RADIOLOGICAL CONTAMINATION IN THE AMERICIUM ZONE

Results presented in this section are based on the double sampling technique in which HPGe measurements were correlated to alpha spectroscopy laboratory results. The linear regression between the HPGe results and laboratory results showed a high degree of correlation (R > 0.97), and was therefore used to standardize each HPGe measurement to laboratory derived alpha spectroscopy results (see Section 2.2.2). This provided an accurate model for estimating radiological contamination in surface soil relative to Tier I and Tier II RSALs at each survey location.

#### 4.1.1 Comparison of HPGe Measurements to Tier I and Tier II RSALs

Based on 1,110 HPGe measurements in the Americium Zone (Figure 2-1), radiological contamination appears to extend approximately 1,050 feet east of the Lip Area. Surface soil contamination is defined by Tier I and Tier II RSAL exceedances, which are summarized in Table 4-1. Using the best-fit regression model, nearly 37 % of the measurement locations exceed

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the Tier II RSALs. Less than 1% of the measurement locations exceed the Tier I RSALs. HPGe results and RSAL calculations are presented in Appendix E.

Table 4-1 Frequency of RFCA Tier I and Tier II RSAL Exceedances-HPGe Survey Results

HPGe Survey	Number of Measurements	Number Of Exceedances RFCA Tier I RSALs	Number Of Exceedances RFCA Tier II RSALs
Surface Soil	1110	4	416

The range of measured <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>235</sup>U, and <sup>238</sup>U activities are presented graphically in Figure 4-1. Comparison of radionuclide results to Tier I and Tier II RSALs indicate that RSAL exceedances are due to elevated activities of <sup>239/240</sup>Pu and <sup>241</sup>Am. For <sup>239/240</sup>Pu, activities range from 6.32 pCi/g to 938.42 pCi/g with a mean value of 105.05 pCi/g. Approximately 7% of the <sup>239/240</sup>Pu measurements exceed the Tier II RSAL of 252 pCi/g. None of the <sup>239/240</sup>Pu measurements exceed the Tier I RSAL of 1429 pCi/g. <sup>241</sup>Am activities range from 4.91 pCi/g to 149.22 pCi/g with a mean value of 20.19 pCi/g. Approximately 10% of the <sup>241</sup>Am measurements exceed the Tier II RSAL of 38 pCi/g. Like <sup>239/240</sup>Pu, none of the <sup>241</sup>Am measurements exceed the Tier I RSAL of 215 pCi/g. HPGe measurements for <sup>235</sup>U and <sup>238</sup>U were all below Tier I and Tier II RSALs.

# 4.1.2 Spatial Distribution of Radiological Contamination in the Americium Zone

Figure 4-2 shows the distribution of Tier I and Tier II RSAL exceedances in surface soil within the Americium Zone. The highest level of contamination as indicated by Tier I RSAL exceedances is isolated at a cluster of three locations near the northwest corner of the Americium Zone and at one location in the south central portion of the Lip Area. Tier II exceedances encompass nearly 37% of the Americium Zone Investigation Area. The HPGe data also define the extent of soil contamination by bounding the area with survey results that are below Tier II RSALs (Figure 4-2). The accuracy of the HPGe survey data is corroborated by historical data as discussed in Section 2.2.2.1. The HPGe data also indicate, as expected, noncontaminated areas where clean fill was used for the road south of the cement and wetland areas, and for the road that borders the western and northern perimeter of the Americium Zone.

The Tier I and Tier II RSAL exceedances are associated with elevated activities of <sup>239/240</sup>Pu and <sup>241</sup>Am. The distribution of <sup>241</sup>Am activities is shown in Figure 4-3. The highest activities of <sup>241</sup>Am

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exceed 140 pCi/g near the northwest corner of the Americium Zone. As shown, the distribution of <sup>241</sup>Am Tier II RSAL exceedances trend in a northeast-southwest orientation, which extends from the southwest corner of the Lip Area to the north-central portion of the Americium Zone. The distribution of <sup>239/240</sup>Pu activities in surface soil (Figure 4-4) is similar to that of the <sup>241</sup>Am activities, with the highest activities exceeding 900 pCi/g near the northwest corner of the Americium Zone. The pattern of Tier I RSAL exceedances is also similar to that observed for <sup>241</sup>Am, with a northeast-southwest trend of contamination. This trend is a result of contaminant deposition from the source area. The similar spatial configurations of <sup>241</sup>Am and <sup>239/240</sup>Pu are to be expected because <sup>241</sup>Am is a daughter product of weapons grade plutonium decay.

#### 4.1.3 FIDLER Surveys

A FIDLER survey was conducted at HPGe measurement location 301 (Figure 2-1) where an isolated HPGe measurement (direct field measurement) exceeded the 10 pCi/g <sup>241</sup>Am decision level. The FIDLER survey was used to determine if the result was caused by the presence of a smaller area containing a hot spot. It should be noted that all <sup>241</sup>Am activities discussed in this section are presented as direct field measurements. The activity of <sup>241</sup>Am from the *in situ* HPGe measurement location 301 was 10.977 pCi/g and the surrounding HPGe measurements were less than 10 pCi/g. FIDLER survey results ranged from 1,224 to 2,841 cpm with a mean of 2,056 cpm. Background measurements of 910 and 1,107 cpm for the two FIDLERs used for the survey were taken at the step-off pad on the north side of the Americium Zone, adjacent to the East Access Road. Because of the low level of <sup>241</sup>Am detected in the soil and two FIDLER instruments used for the survey, the results are qualitative at best. However, contamination appears to be homogeneous as would be expected at this distant location from the source where contamination is a result of wind dispersal of plutonium contaminated soil from the 903 Pad and Lip Area.

FIDLER surveys were also conducted at HPGe locations 460 and 462 (Figure 2-1) where surface soils exceeded the RFCA Tier I RSALs. The surveys were conducted to determine whether contamination was homogeneous and widespread as suggested by the conceptual model, or heterogeneous consisting of numerous individual hot spots. The activities of <sup>241</sup>Am from the *in situ* HPGe measurements were 115.74 and 109.04 pCi/g for HPGe measurement locations 460

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and 462, respectively, and the surrounding HPGe measurements were less than 100 pCi/g. FIDLER survey results for HPGe measurement location 460 ranged from 2,928 to 17,039 cpm with a mean of 8,293 cpm. FIDLER survey results for FOV 462 ranged from 3,466 to 15,331 cpm with a mean of 8,729 cpm. Background measurements of 1,430 and 2,127 cpm for the two FIDLERs were taken at the step-off pad on the southwest corner of the Americium Zone, adjacent to the access road for the old firing range. Because two FIDLER instruments were used for the surveys, the results are qualitative. However, contamination appears to be heterogeneous and consists of numerous individual hot spots as might be expected from soil disturbance, localized erosional paths, or depositional areas near the source of contamination.

#### 4.2 SOIL RADIOLOGICAL CONTAMINATION IN THE 903 PAD AND LIP AREA

Surface and subsurface soil samples were analyzed for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/234</sup>U, <sup>235</sup>U, and <sup>238</sup>U using alpha spectroscopy methods. Surface and subsurface soil samples were aggregated into four native soil horizons (Native 1 [0-6 in], Native 2 [6-12 in], Native 3 [12-18 in], Native 4 [18-24 in]), bedrock soil, and artificial fill under the 903 Pad. Artificial fill in the Lip Area was classified as Native 1 soil because native soil and artificial fill could not be differentiated in the field.

Based on the radiological results, contamination appears to be confined to the top 1.5 feet of native soil, and is most extensive in the Native 1 soil horizon. Table 4.2 summarizes the Tier I and Tier II RSAL exceedances. The frequency of Tier I and II exceedances decreases with increasing depth. No samples collected beneath the Native 3-soil horizon exceeded Tier I and Tier II RSALs<sup>2</sup>. Radiological data and RSAL SOR calculations for surface and subsurface soil are presented in Appendix E.

<sup>&</sup>lt;sup>2</sup> Radiological sample results from the subsurface VOC investigation indicate no contamination above Tier II RSALs. Activities of all measured radionuclides from the VOC investigation were below 3 pCi/g.

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Table 4-2 Frequency of RFCA Tier I and Tier II RSAL Exceedances-Native Soil Results

Geologic/Fill Material	Number of Measurements	Frequency Of Exceedances RFCA Tier I RSALs	Frequency Of Exceedances RFCA Tier II RSALs
Asphalt	9	N/A	N/A
Bedrock	12	0	0 .
Fill	12	0	1
Native	72	0	0
Native 1	62	17	34
Native 2	62	5	11 ·
Native 3	62	0	3
Native 4	58	0	0

N/A Not Applicable; Asphalt samples were not comparable to RSALs

# 4.2.1 Radionuclide Activities in Native Soils

The range of activities for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/234</sup>U, <sup>235</sup>U, and <sup>238</sup>U in Native 1, Native 2, and Native 3 soil types are shown graphically in Figure 4-5. As discussed in the following subsections, the amount of contamination decreases significantly with depth.

#### 4.2.1.1 Native 1 Surface Soil Contamination

The Native 1 soil has the most extensive contamination as indicated by activities of <sup>241</sup>Am, <sup>239/240</sup>Pu and <sup>231</sup>U that exceed Tier I and Tier II RSALs (Table 4-2 and Figure 4-5). <sup>238</sup>Uranium activities range from 0.49 pCi/g to 780 pCi/g with a geometric mean value of 1.99 pCi/g<sup>3</sup>. The high activity of 780 pCi/g is the only exceedance above Tier I and Tier II RSALs of 586 pCi/g and 103 pCi/g, respectively. Approximately 44 percent of the <sup>239/240</sup>Pu and <sup>241</sup>Am results exceed Tier II RSALs.

<sup>239/240</sup> Pu activities range from 0.82 pCi/g to 152,260 pCi/g with a geometric mean value of 146.69 pCi/g. For <sup>239/240</sup>Pu, 15% of the samples exceed the Tier I RSAL of 1,429 pCi/g and 44% of the samples exceed the Tier II RSAL of 252 pCi/g. <sup>241</sup>Am activities in Native 1 soil appear

<sup>&</sup>lt;sup>3</sup> The data appear to have a lognormal distribution, and therefore, a geometric mean is a better measure of the central tendency of the distribution.

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more extensive than that of <sup>239</sup>Pu with activities ranging from 0.15 pCi/g to 31,670 pCi/g. For <sup>241</sup>Am activities, 19.1% of the samples exceed the Tier I (215 pCi/g) RSAL and 47.1% exceed the Tier II (38 pCi/g) RSAL.

#### 4.2.1.2 Native 2 Subsurface Soil Contamination

The Native 2 soil horizon is substantially less contaminated than the Native 1 soil horizon but still contains activities above Tier I and Tier II RSALs for <sup>241</sup>Am and <sup>239/240</sup>Pu (Figure 4-5). <sup>239/240</sup>Pu activities range from 0.14 pCi/g to 1,820 pCi/g with a geometric mean of 8.65 pCi/g. For <sup>239/240</sup>Pu, 0.03% of the samples exceed the Tier I RSAL (1,429 pCi/g) and 11% of the samples exceed the Tier II RSAL (252 pCi/g). <sup>241</sup>Am activities range from non-detectable (0.03 pCi/g) to 406 pCi/g with a geometric mean value of 1.79 pCi/g. <sup>241</sup>Am contamination is similar to that of <sup>239/240</sup>Pu contamination as indicated by frequency of exceedances of 0.03% and 11% above Tier I (215 pCi/g) and Tier II (38 pCi/g) RSALs.

#### 4.2.1.3 Native 3 Subsurface Soil Contamination

The amount of contamination in the Native 3 soil is minimal relative to the Tier II RSALs (Figure 4-5). Only one sample for <sup>241</sup>Am exceeds the corresponding Tier II RSAL of 38 pCi/g. <sup>241</sup>Am in the Native 3 soil horizon ranges from non-detectable to 54.40 pCi/g with a median value of 0.23 pCi/g<sup>4</sup>. Activities of <sup>239/240</sup>Pu in the Native 3 soil horizon were below the respective Tier I and Tier II RSALs.

# 4.2.2 Spatial Distribution of Contamination

Examination of the spatial distribution of contamination is useful for evaluating potential sources and contaminant migration pathways. This section discusses the spatial distribution of Tier I and Tier II RSALs for Native 1, Native 2, and Native 3 soil horizons. Also presented are the spatial distributions of <sup>239/240</sup>Pu and <sup>241</sup>Am activities because of their exceedance of Tier I and Tier II RSALs.

<sup>&</sup>lt;sup>4</sup> Due to the negative activities in the data set, the median value was used as a measure of the central tendency of the distribution instead of the geometric mean.

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# 4.2.2.1 Spatial Distribution of Radionuclides in the Native 1 Soil Horizon

As shown in Figure 4-6, Tier I and Tier II RSAL exceedances (>1 for the sum of ratios) in Native 1 soil are located throughout the 903 Pad and Lip Area. There is no distinct pattern to the Tier I and Tier II exceedances at the 903 Pad. Most of the southern boundary and portions of the northern boundary do not exceed Tier II RSALs. For the Lip Area, Tier I exceedances are most prevalent in the center area due east of the 903 Pad, with Tier II exceedances surrounding this area. Relatively "clean" areas as indicated by RSALs less than Tier II are located further to the east and south of the 903 Pad. Apparent spatial gaps in contamination may be explained by past remedial activities. For example, the soil in the Lip Area was graded back toward the 903 Pad during past remedial actions, and therefore the soil closest to the Pad is not as contaminated as the soil near the central portion of the Lip Area. Similar remedial activities in 1984 removed contaminated soil in the western portion of the Lip Area.

The RSAL exceedances are associated with elevated levels of <sup>239/240</sup>Pu and <sup>241</sup>Am. Figure 4-7 shows the distribution of <sup>241</sup>Am in the Native 1 surface soil. The highest <sup>241</sup>Am activities exceed 30,000 pCi/g and are centered near boring 91598 (Figure 4-7). However, as shown in Figure 4-7, the majority of the Native 1 soils in the 903 Pad (approximately half of the Native 1 soil) and Lip Area exceed the Tier II RSAL for <sup>241</sup>Am of 38 pCi/g. The distribution of the <sup>239/240</sup>Pu activities is similar to that of the <sup>241</sup>Am activities, with the highest activities exceeding 150,000 pCi/g at boring 91598 (Figure 4-8). Like <sup>241</sup>Am, the <sup>239/240</sup>Pu activities are elevated with respect to the Tier II RSAL (252 pCi/g) in most of the Native 1 soil within the 903 Pad and approximately half of the Native 1 soil in the Lip Area.

#### 4.2.2.2 Spatial Distribution of Radionuclides in the Native 2 Soil Horizon

Figure 4-9 shows the distribution of the Tier I and Tier II RSAL exceedances (>1 for the sum of ratios) in the Native 2 soil horizon. The RSAL exceedances are not as ubiquitous as in the Native 1 soil horizon. RSAL exceedances are isolated to an area around boreholes 91398, 91598, 91898, and 91998 at the 903 Pad and around several boreholes throughout the Lip Area (boreholes 94898, 94998, 95198, 95398, 95498, 95598, and 97598). Like the Native 1 soil horizon, RSAL exceedances in the Native 2 soil horizon are associated with elevated levels of <sup>241</sup> Am and <sup>239</sup>Pu.

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<sup>&</sup>lt;sup>241</sup>Am activities exceed 400 pCi/g in the 903 Lip Area with the highest activity observed at 95198 (Figure 4-10). The distribution of Pu-239 in the Native 2 soil horizon is very similar to that of <sup>241</sup>Am (Figure 4-11). <sup>239</sup>Pu exceeds 18,000 pCi/g (above the Tier I RSAL) at boring 95198. <sup>239/240</sup>Pu activities exceeding the Tier II RSAL (252 pCi/g) are distributed like the <sup>241</sup>Am activities (Figure 4-11). The <sup>239/240</sup>Pu and <sup>241</sup>Am activities in the Native 2 soil horizon are generally one to two orders of magnitude less than those observed in the Native 1 soil horizon.

Historical grading activity at the 903 Pad likely explains the somewhat different <sup>239/240</sup>Pu and <sup>241</sup>Am distributions between Native 1 and Native 2 soils. For example, grading activities at boring 91998 may have redistributed contamination in Native 1 soil leaving higher contaminated soils in the Native 2 soil horizon. In the Lip Area, the amount of artificial fill in the Native 1 soil horizon would explain higher activities in Native 2 soil relative to the Native 1 soil.

# 4.2.2.3 Spatial Distribution of Radionuclides in the Native 3 Soil Horizon

Figure 4-12 shows the distribution of the Tier II RSAL exceedances (>1 for the sum of ratios) in the Native 3 soil horizon<sup>5</sup>. The amount of radionuclide contamination in the Native 3 soil horizon is significantly less than that in the Native 1 and Native 2 soil horizons. Tier II RSAL exceedances are isolated along the northern boundary of the Lip Area at borings 94898 and 95198. One other isolated Tier II RSAL exceedance is observed east of the 903 Pad at boring 95498. Like the Native 1 and Native 2 soil horizons, the RSAL exceedances within the Native 3 soil horizon are associated with elevated levels of <sup>241</sup>Am and <sup>239/240</sup>Pu.

As shown in Figure 4-13, elevated levels of <sup>241</sup>Am with respect to the Tier II RSAL (38 pCi/g) are observed along the northern boundary of the Lip Area at boring 94898. Another area east of the 903 Pad near boring 95498 shows relatively high activities of <sup>241</sup>Am (up to 26 pCi/g) but these activities are slightly less than the Tier II RSALs<sup>6</sup>. The spatial distribution of <sup>239</sup>Pu in the Native 3 soil horizon is similar to that of <sup>241</sup>Am, (Figure 4-14). Although none of the <sup>239/240</sup>Pu samples exceed Tier I or Tier II RSALs, the relatively high activities near borings 94898 and 95498 contribute to the Tier II RSAL exceedances at these locations.

<sup>&</sup>lt;sup>5</sup> Tier I RSAL exceedances were not observed in the Native 3 Soil horizon.
<sup>6</sup> Tier I RSAL exceedances for <sup>241</sup>Am were not observed in the Native 3 Soil horizon.

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Overall, the area of <sup>241</sup>Am and <sup>239/240</sup>Pu contamination decreases significantly with depth. Despite nearly identical spatial trends, the <sup>241</sup>Am and <sup>239</sup>Pu activities within the Native 3 soil horizon are an order of magnitude less than those within the Native 2 soil horizon.

# 4.2.3 Radionuclide Activities in 903 Pad Asphalt and 903 Pad Artificial Fill

Asphalt samples from the 903 Pad were collected to obtain preliminary estimates of the sample variance and mean for waste characterization purposes<sup>7</sup>. Random sampling techniques were used as an appropriate method to estimate the population mean and to determine the total amount of contamination. Nine asphalt samples were collected from sample locations randomly selected from the twenty-five 903 Pad subsurface soil sampling locations as shown in Figure 4-15. Asphalt thickness ranged from 0.4 to 0.7 feet with an average thickness of 0.5 feet. Twelve artificial fill samples were collected from locations randomly selected from the twenty-five 903 Pad subsurface soil sampling locations as shown in Figure 4-16. Artificial fill thickness ranged from 0.3 to 0.9 feet with an average thickness of 0.5 feet beneath the 903 Pad. Artificial fill results were compared to RFCA Tier I and Tier II RSALs. Samples were analyzed for <sup>241</sup>Am, <sup>239/240</sup>Pu <sup>233/234</sup>U, <sup>235</sup>U, and <sup>238</sup>U, using alpha spectroscopy methods. The descriptive summary statistics are provided in Appendix D.

# 4.2.3.1 Radionuclide Distribution in Asphalt

The radionuclide activities in asphalt were low relative to the activities observed in the Native 1 soil horizon. As shown in Figures 4-15 and 4-17, the activities for <sup>241</sup>Am, <sup>239/240</sup>Pu, <sup>233/234</sup>U, <sup>235</sup>U, and <sup>238</sup>U are all below 1.5 pCi/g. The mean, standard deviation, and other descriptive statistics are summarized in Table 4-3.

Figure 4-15 shows the distribution of radionuclides in asphalt. With the exception of <sup>238</sup>U, the highest radionuclide activities in asphalt are present at boring 91898 (<sup>233/234</sup>U [1.13 pCi/g], <sup>235</sup>U [0.133 pCi/g], <sup>241</sup>Am [0.341 pCi/g], and <sup>239/240</sup>Pu [1.22 pCi/g]). The highest <sup>238</sup>U (0.919 pCi/g) activity in asphalt was reported at boring 90198.

<sup>&</sup>lt;sup>7</sup> Asphalt samples were not comparable to RSALs, which are based the physical and chemical properties of soil. Instead, waste disposal WAC requirements for asphalt will be based on the mean and variance.

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Table 4-3. Descriptive Summary Statistics for 903 Pad Asphalt

Descriptive Statistic	233/234U (pCi/g)	<sup>235</sup> U (pCi/g)	<sup>236</sup> U (pCi/g)	<sup>239/240</sup> Pu (pCi/g)	<sup>241</sup> Am (pCi/g)
Mean	0.81	0.05	0.75	0.16	0.07
Geometric Mean	0.80	0.04	0.74	N/A	0.04
Standard Error	0.05	0.01	0.04	0.13	0.03
Median	0.78	0.04	0.75	0.03	0.04
Standard Deviation	0.15	0.03	0.13	0.40	0.10
Sample Variance	0.02	0.00	0.02	0.16	0.01
Kurtosis	1.70	7.01	-1.60	8.85	8.28
Skewness	1.22	2.46	-0.08	2.97	2.84
Coefficient of Variation	0.19	0.72	. 0.17	2.42	1.46
Range	0.47	0.12	0.32	1.22	0.33
Minimum	0.66	0.01	0.60	0.00	0.02
Maximum	1.13	0.13	0.92	1.22	0.34
Sum	7.27	0.42	6.74	1.48	0.63
Count	9	9	9	9	9
Confidence Level (90.0%)	0.08	0.02	0.07	0.22	0.06

NA Not Applicable.

## 4.2.3.2 Radionuclide Distribution in 903 Pad Artificial Fill

The ranges of activities for the measured isotopes in artificial fill are presented in Figure 4-17. Overall, the radionuclide activities in artificial fill are low relative to the activities observed in the Native 1, Native 2, and Native 3 soil horizons. However, one Tier II RSAL exceedance is observed within the 903 Pad Area at boring 91898 (Figure 4-16). The Tier II RSAL exceedance is associated with elevated levels of <sup>241</sup>Am (126 pCi/g) and <sup>239/240</sup>Pu (558 pCi/g), which both exceed the respective Tier II RSALs of 38 pCi/g and 252 pCi/g. <sup>241</sup>Am activities in artificial fill range from 0.02 pCi/g to 126 pCi/g with a geometric mean value of 1.18 pCi/g. Elevated activities within the artificial fill appear to be isolated around this single boring considering that the highest <sup>233/234</sup>U (2.02 pCi/g), <sup>235</sup>U (0.49 pCi/g), <sup>233/234</sup>U (2.77 pCi/g), and <sup>239/240</sup>Pu (558 pCi/g) activities were also observed at boring 91898 (Figure 4-17). Descriptive summary statistics for the 903 Pad artificial fill are presented in Table 4-4.

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Table 4-4. Descriptive Summary Statistics for 903 Pad Artificial Fill

	<sup>233/234</sup> U	<sup>235</sup> U	<sup>238</sup> U	<sup>239/240</sup> Pu	<sup>241</sup> Am
Descriptive Statistic	(pCi/g)	(pCi/g)	(pCi/g)	(pCi/g)	(pCi/g)
Mean	1.06	0.09	1.15	53.75	12.01
Geometric Mean	1.02	0.06	1.00	5.78	1.18
Standard Error	0.11	0.04	0.18	45.95	10.38
Median	0.98	0.06	1.13	4.48	0.85
Mode	0.84	0.07	1.24	N/A	N/A
Standard Deviation	0.38	0.13	0.61	159.19	35.97
Sample Variance	0.14	0.02	0.37	25340.90	1294.08
Kurtosis	4.79	11.19	5.53	11.88	11.90
Skewness	1.51	3.30	1.72	3.44	3.44
Coefficient of Variation	0.36	1.43	0.53	2.96	2.99
Range	1.61	0.49	2.60	557.99	125.98
Minimum	0.41	0.00	0.17	0.01	0.02
Maximum	2.02	0.49	2.77	558.00	126.00
Sum	12.25	1.00	13.33	642.14	143.51
Count	12	12	12	12	12
Confidence Level (90.0%)	0.18	0.06	0.29	75.59	17.08
Number of Detections Above Tier I	0	0	0	0	0
Number of Detections Above Tier II	0	0	0	1	1

N/A Not Applicable

#### 4.3 SUBSURFACE SOIL VOC INVESTIGATION

Seventeen boreholes were completed to investigate VOC contamination at the 903 Pad and Lip Area, which included the original 13 boreholes and four "step-out" boreholes (Figure 4-18). Subsurface soil VOC contaminants of concern as identified in the SAP (RMRS, 1998a) include carbon tetrachloride (CCl<sub>4</sub>), PCE, TCE, and 1,2-cis-dichloroethylene (1,2-DCE). Despite the absence of DNAPLs during drilling, VOCs were detected at several boring locations. As shown in Figure 4-18, detections of CCl<sub>4</sub> ranged from 2.3 ug/kg in borehole 96698 (22.4 to 22.8 ft) up to 5.3 ug/kg in borehole 96798 (20.4 to 20.8 ft). Detections of PCE ranged from 1.1 ug/kg in borehole 97698 (8.2 to 8.6 ft) up to 6,100 ug/kg in borehole 90998 (3.8 to 4.0 ft). Detections of TCE ranged from 0.89 ug/kg in borehole 96698 (20.4 to 20.8 ft) up to 290 ug/kg in borehole 90998 (3.8 to 4.0 ft). Detections of 1,2-DCE ranged from 1.1 ug/kg in boreholes 96798 (12.5 to

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12.9 ft) and 97698 (8.2 to 8.6 ft) up to 4,400 ug/kg in borehole 90998 (3.8 to 4.0 ft). In general, the majority of the VOC detections were observed in the northeastern quadrant of the 903 Pad at borings 90998, 95998, 96498, 96698, 96798, and 97698. VOC detections were also observed in the 903 Lip Area at boring 97298 and within the central portion of the 903 Pad at boring 96898. The ranges of VOC concentrations are presented in Figure 4-19.

No VOC detections were equal to or greater than the current Tier I SSALs (Table 4-5). However, proposed SSALs are 1 to 4 orders of magnitude less than the current Tier I SSALs (Table 1-2). Given the proposed SSALs, only one value (6,100 ug/kg observed at borehole 90998) exceeds the proposed Tier I SSAL for PCE (3,150 ug/kg). The VOCs that exceed the proposed Tier II SSALs include PCE, TCE, and 1,2-DCE (Table 4-5). As shown in Figure 4-18, the proposed Tier II exceedances are observed at boreholes 97698 (PCE), 96498 (PCE), 90998 (PCE,TCE, and 1,2-DCE), 95998 (PCE), and 96798 (PCE). The proposed Tier II SSAL exceedances occur within a relatively small area around monitoring well 08891. PCE is the most ubiquitous of the contaminants, occurring at five of the borings. The depth of contamination (relative to the proposed SSALs) varies from the 3.8 feet bgs at borehole 90998 to 24.6 feet bgs at borehole 95998. The proposed Tier II exceedances that occur below the water table are observed at borings 97698, 95998, and 96798.

Table 4-5. Frequency of VOC SSAL Exceedances in Subsurface Soil.

VOC	Number of Measurements	Number of Detections	Number Of Exceedances Current Tier I SSAL	Number Of Exceedances Proposed Tier I SSAL	Number Of Exceedances Proposed Tier II SSAL
Carbon Tetrachloride	86	3	0	0	0
PCE	86	19	0	1	7
TCE	86	7	0	0	1
1,2-DCE	32	1	0	0	1

Some of the deeper borehole samples may reflect solute (dissolved) concentrations in groundwater rather than concentrations in soil. Groundwater beneath the 903 Pad is relatively shallow with depth to water averaging approximately 19 feet below ground surface (bgs). During high flow regimes depth to water may decrease to 12 feet bgs. Therefore, it is likely that

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detections of CCL<sub>4</sub>, PCE and TCE observed at depths greater than 20 feet at boreholes 96698 and 96798 may represent partitioning of VOCs between the aqueous and solid phases.

The delineation of VOC contamination was optimized during the field investigation by the "stepout" boring approach (RMRS, 1998a). This decision making process was triggered by detections of VOCs above 10 percent of the respective current Tier I SSALs at any boring location. Such levels required an additional "step-out" boring approximately 20 feet in the upgradient direction from the boring where VOCs were detected at 10 percent of the current Tier I SSALs. Detections above 10 percent of the current Tier I SSALs were observed at borings 90998 and 95998. Borehole 90998 was completed as a shallow subsurface radiological borehole to a depth of 4.0 ft and based on field instrument readings a soil sample for VOC analysis was collected at a depth of 3.8 to 4.0 ft. As summarized above, the highest concentrations of PCE (6,100 ug/kg), TCE (290 ug/kg), and 1,2-DCE (4,400 ug/kg) were observed in borehole 90998. Concentrations of 1,2-DCE and PCE were above 10 percent of the current Tier I SSALs.

Borehole 96498 was completed to bedrock within one foot of borehole 90998 per the SAP (RMRS, 1998a) requiring completion of a shallow radiological borehole as a VOC borehole if VOCs were detected above 10 percent of the current Tier I SSALs. Similarly, borehole 95998 was completed to bedrock 20 ft in an upgradient direction west of boreholes 90998 and 96498. Detections of PCE (3,060 ug/kg), TCE (9.9 ug/kg), and 1,2-DCE (5.4 ug/kg) were observed in borehole 95998 at a depth of 5.0 to 5.6 ft. The concentrations of PCE that were observed in borehole 95998 were above 10 percent of the current Tier I SSAL. Therefore, borehole 97698 was completed in an upgradient direction 20 feet west of borehole 95998 in compliance with the SAP. Although PCE, TCE, and 1,2-DCE were detected in borehole 97698 none of the concentrations met or exceeded 10 percent of the current Tier I SSALs for the respective analytes.

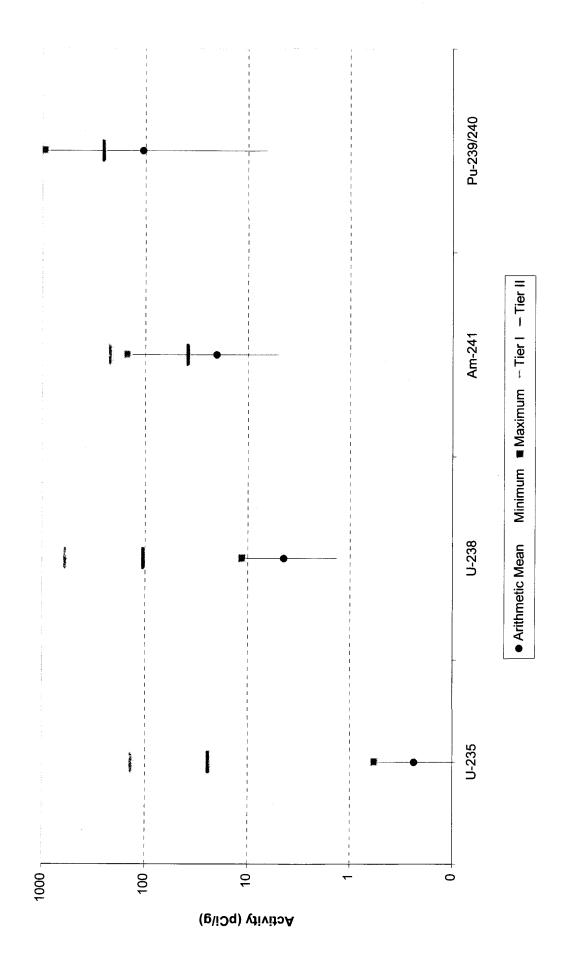
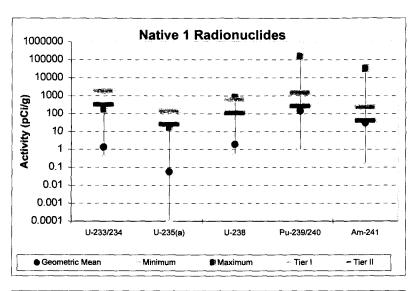
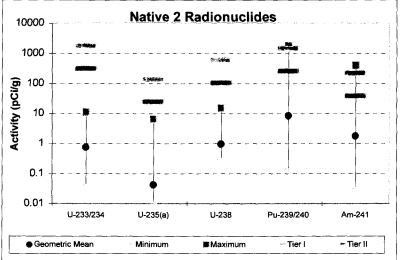
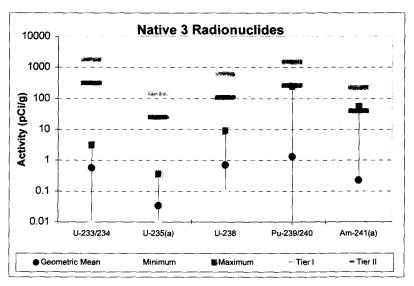


Figure 4-1 Range of Radionuclide Activities in Surface Soil - HPGe Survey

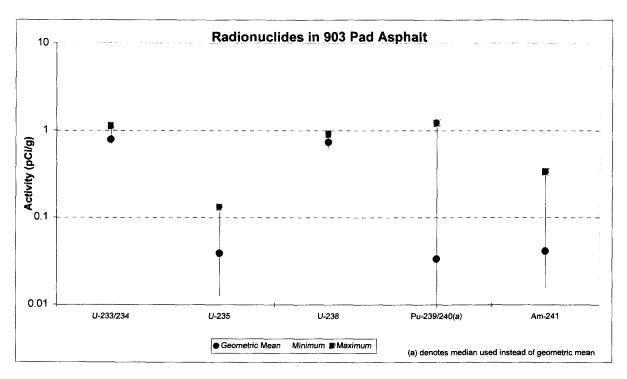






(a) Denotes median used instead of geometric mean

Figure 4-5. Range of Radionuclide Activities in Native 1, Native 2, and Native 3 Soils Horizons.



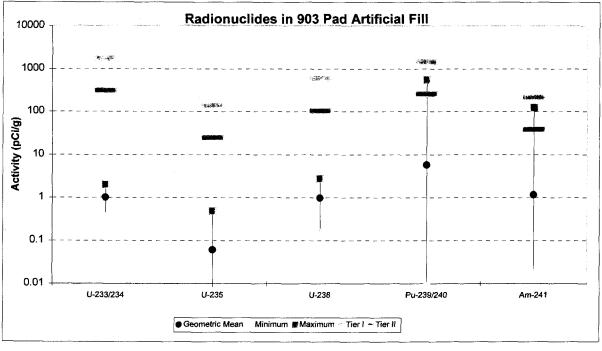


Figure 4-17. Range of Radionuclide Activities in Asphalt and Artificial Fill

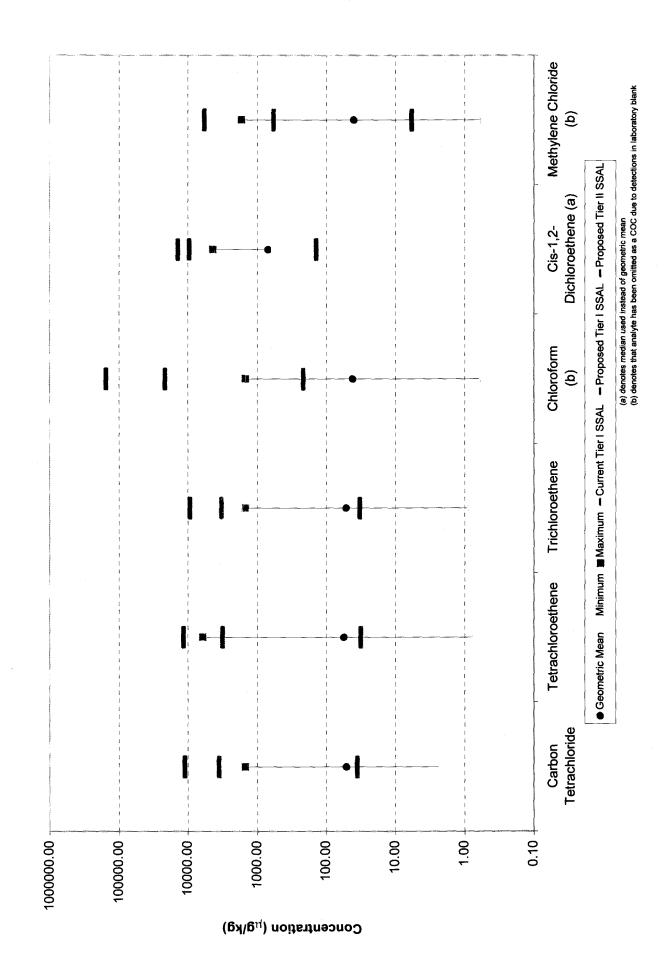


Figure 4-19. Range of VOC Concentrations in Subsurface Soil

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# 5.0 CONTAMINTED MEDIA VOLUME ESTIMATES

Volume estimates of radiological and VOC contaminated surface and subsurface soil are based on the areal and vertical extent of contamination above Tier I and Tier II RSALs and proposed SSALs. An ArcInfo, version 7.2.2, Thiessen polygon command (ESRI, 1999) was used to determine areas exceeding action levels for subsequent in-place volume calculations. Remedial alternatives will be evaluated in the IM/IRA Decision Document based on these volume estimates. In-place volume estimates for the 903 Pad asphalt and artificial fill are also presented.

### 5.1 903 PAD ASPHALT AND ARTIFICIAL FILL VOLUME ESTIMATES

Characterization data for the asphalt comprising the 903 Pad were collected for waste characterization profiling, however, data were not compared to Tier I or Tier II RSALs. The estimated in-place volume of asphalt is 2,743 yds<sup>3</sup>. The estimated in-place volume of artificial fill is 2,743 yds<sup>3</sup>. The amount of radiologically contaminated artificial fill, relative to Tier II RSALs, beneath the 903 Pad is estimated at 104 yds<sup>3</sup>. The 104 yds<sup>3</sup> estimate is based on a 75 ft by 75 ft area surrounding boring 91898 and a 6 inch thickness of artificial fill. Table 5-1 summarizes the estimated areal extent, depth, and in-place volumes of asphalt and artificial fill for the 903 Pad.

Table 5-1 Summary of 903 Pad Asphalt and Artificial Fill Volumes

903 Pad	Depth (ft)	Area (ft²)	Volume <sup>1</sup> (ft <sup>3</sup> )	Volume <sup>1</sup> (yd <sup>3</sup> )	Volume <sup>1</sup> (m <sup>3</sup> )
Asphalt	0.5	148,104	74,052	2,743	2,097
Artificial Fill less than Tier II RSALs	0.5	142,479	71,239	2,639	2,017
Artificial Fill greater than Tier II RSALs	0.5	5,625	2,813	104	80
Total	-	296,208	148,104	5,485	4,194

Volume represents materials in-place

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# 5.2 TIER I RSAL EXCEEDANCE SOIL VOLUME ESTMATES

A composite map of the areal extent of Tier I RSAL exceedances in soil is presented in Figure 5-1. As shown, soil with radionuclides exceeding the Tier I RSALs is located at the 903 Pad, east of the 903 Pad in the Lip Area, and sporadically in the southern portion of the Lip Area and western portion of the Americium Zone. Table 5-2 summarizes the estimated areal extent, depth, and in-place volumes of soils exceeding Tier I RSALs by IHSS. The areal extent of Native 1 radiologically contaminated surface soil (relative to Tier I RSALs) is 120,360 ft<sup>2</sup>. Depth of contamination varies from 0 to 6 inches to 0 to 12 inches throughout the investigation area. Based on the areal and vertical extent of Tier I RSAL exceedances, the total volume of in-place radialogically contaminated soil is 2,924 cubic yards (yds<sup>3</sup>). The in-place volumes of contaminated soil by IHSS are as follows: 1,268 yds<sup>3</sup> for the 903 Pad; 1,598 yds<sup>3</sup> for the Lip Area; and 58 yds<sup>3</sup> for the Americium Zone.

Table 5-2 Summary of Radiologically Contaminated Soil Volumes-Tier I RSAL Exceedances

903 Pad	Depth (ft)	Area (ft²)	Volume <sup>1</sup> (ft <sup>3</sup> )	Volume <sup>1</sup> (yd <sup>3</sup> )	Volume <sup>1</sup> (m <sup>3</sup> )
Native 1	0.5	62,953	31,477	1,166	891
Native 2	0.5	5,532	2,766	102	78
Total			34,243	1,268	969
Lip Area					
Native 1	0.5	54,288	27,144	1,005	768
Native 2	0.5	32,044	16,022	593	454
Total			43,166	1,598	1,222
Americium Zone					
Total	0.5	3,119	1,560	58	44
Grand Total			78,969	2,924	2,235
1					<u> </u>

<sup>&</sup>lt;sup>1</sup> Volume represents materials in-place

#### 5.3 TIER II RSAL EXCEEDANCE SOIL VOLUME ESTIMATES

A composite map of the areal extent of Tier II RSAL exceedances in soil is presented in Figure 5-2. As expected, contamination above the Tier II RSALs is much more extensive than that of the Tier I RSAL exceedances. In general, Tier II RSAL exceedances encompass most of the 903

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Pad, the Lip Area, and the Americium Zone. Tier II RSAL exceedances in two portions of the Lip Area extend down to the Native 3 soil horizon, a depth of 1.5 feet. Figure 5-2 shows the areal extent of the Tier II RSAL exceedances for the Native 1 (0 to 6-inch), Native 2 (6 to 12-inch), and Native 3 (12 to 18-inch) soil horizons. Table 5-3 summarizes the estimated areal extent, depth, and in-place volumes of soils exceeding Tier II RSALs by IHSS.

The areal extent of Native 1 radiologically contaminated surface soil (relative to Tier II RSALs) is 700,698 ft<sup>2</sup>. Depth of contamination varies from 0 to 6 inches to 0 to 18 inches within the investigation area. Based on the areal and vertical extent of Tier II RSAL exceedances, the total volume of in-place radiologically contaminated soil is 14,763 yds<sup>3</sup>. A depth of 6 inches was used to estimate volumes of soil in the Americium Zone. Radiologically contaminated soil volumes based on Tier II RSAL exceedances are summarized in Table 5-3. The in-place volumes of contaminated soil by IHSS are as follows: 2,471 yds<sup>3</sup> for the 903 Pad, 5,267 yds<sup>3</sup> for the Lip Area; and 7,025 yds<sup>3</sup> for the Americium Zone.

Table 5-3 Summary of Radiologically Contaminated Soil Volumes-Tier II RSAL Exceedances

903 Pad	Depth (ft)	Area (ft²)	Volume <sup>1</sup> (ft <sup>3</sup> )	Volume <sup>1</sup> yd <sup>3</sup> )	Volume <sup>1</sup> (m <sup>3</sup> )
Native 1	0.5	111,676	55,838	2,068	1,581
Native 2	0.5	21,738	10,869	403	308
Total			66,707	2,471	1,889
Lip Area					
Native 1	0.5	209,689	104,845	3,883	2,969
Native 2	0.5	52,790	26,395	978	747
Native 3	0.5	21,941	10,971	406	311
Total			142,211	5,267	4,027
Americium Zone					
Total	0.5	379,333	189,667	7,025	5,371
Grand Total	=		398,585	14,763	11,287
17				<u> </u>	

<sup>1</sup> Volume represent s materials in-place

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#### 5.4 SSAL EXCEEDANCE SOIL VOLUME ESTIMATES

VOC contaminants of concern (CCl<sub>4</sub>, PCE, 1,2-DCE, and TCE) did not exceed the current Tier I SSALs. However, as discussed in Section 4.3, PCE exceeds the proposed Tier I SSAL in boring 90998 (Figure 4-18). Proposed Tier II SSAL exceedances for PCE were also observed in five borings east of well 08891. 1,2-DCE exceeds the proposed Tier II SSAL in boring 90998. The areal extent of contamination was bounded one-half the distance between adjacent borings where VOC results were below their respective SSALs, and by the edge of the 903 Pad to the east. Several proposed Tier II SSAL exceedances were observed below the water table (average depth to water is 19 feet bgs) at boreholes 95998, 96798, and 97698. VOC contamination below the water table will be addressed under the groundwater program.

# 5.4.1 Tier I SSAL Exceedance Soil Volume Estimates

A composite map showing the areal extent of contamination as defined by the proposed Tier I SSALs is presented in Figure 5-3. The depth of VOCs that exceed proposed Tier I SSALs is assumed to extend from the natural soil surface below the top of the asphalt to 4.0 feet bgs (a thickness of 3.0 feet). This is a conservative assumption given that VOC samples were not collected above the four-foot sample interval. Based on the areal extent of the Tier I SSAL exceedances (5,017 ft²) and a thickness of 3.0 feet, the total in-place volume of contaminated soil is 558 yds³ (Table 5-4).

Table 5-4 Summary of Radiologically Contaminated Soil Volumes – SSAL Exceedances

Area/Volume	Volume <sup>1</sup> of Soils Greater Than Current Tier I SSALs (yds <sup>3</sup> )	Volume <sup>1</sup> of Soils Greater than Proposed Tier I SSALs (yds <sup>3</sup> )	Volume <sup>1</sup> of Soils Greater than Tier II SSALs (yds <sup>3</sup> )
Area with Soils Greater than Tier I and II RSALs	0	93	138
Area with Soils Less than Tier II RSALs	0	465	3,428
Total	0	558	3,566

Volume represents materials in-place volume.

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#### 5.4.2 Tier II SSAL Exceedance Soil Volume Estimates

A composite map showing the areal extent of contamination as defined by the proposed Tier II SSALs is presented in Figure 5-3. The areal extent of proposed Tier II SSAL contamination is slightly more extensive than that of Tier I SSAL contamination. The depth of VOCs that exceed Tier II SSALs is assumed to extend from the natural soil surface below the asphalt to 13.9 feet bgs (a thickness of 12.9 feet). This includes natural soils from the 1 foot to 4 foot interval where samples were not collected. Based on the areal extent of the Tier II SSAL exceedances (7,464 ft²) and a thickness of 12.9 feet, the total in-place volume of contaminated soil is 3,566 yds³ (Table 5-4).

# 5.5 RSAL AND SSAL EXCEEDANCE SOIL VOLUME ESTIMATES

Two areas within the 903 Pad contain surface soil with elevated levels of both radionuclides (RSALs) and VOCs (SSALs). Soil exceeding proposed SSALs occur in the two areas shown in Figure 5-3. Soil exceeding Tier I and Tier II RSALs are provided in Figures 5-1 and 5-2, respectively. Comparing these figures with Figure 5-3 shows that there are areas where both RSALs and SSALs exceedances overlap. Proposed Tier I SSAL exceedances in natural soils occur to a depth 4.0 feet. Tier I (and consequently Tier II) RSAL exceedances in natural soils are present to a depth of 6 inches in this area. Therefore, an estimated total of 93 yds<sup>3</sup> ([5,017 ft<sup>2</sup> x 0.5 ft]/27 ft<sup>3</sup>/yd<sup>3</sup>) of soils exceed both Tier I (and II) RSALs and proposed Tier I SSALs.

Proposed Tier II SSAL exceedances in natural soils occur to a depth 13.9 feet. Tier I (and consequently Tier II) RSAL exceedances in natural soils are present to a depth of 6 inches. Therefore, an estimated total of 138 yds<sup>3</sup> ([7,464 ft<sup>2</sup> x 0.5 ft]/27 ft<sup>3</sup>/yd<sup>3</sup>) of soils exceed both Tier I and II RSALs and proposed Tier II SSALs.

# 5.6 SSAL EXCEEDANCE SOIL VOLUME ESTIMATES (NON-RADIOLOGICALLY CONTAMINTED)

This section provides volume estimates of VOC contaminated soil (relative to SSALs) below the Native 1 soil horizon where radiologically contaminated soil (relative to RSALs) is not present.

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The total in-place soil volume estimates, therefore, excludes the radiologically contaminated Native 1 soil addressed in Sections 5.2 and 5.3.

Soil exceeding SSALs occur in two areas within the 903 Pad (Figure 5-3). Proposed Tier I SSAL exceedances in natural soils occur to a depth 4.0 feet below the top of asphalt. Therefore, excluding the upper 1.5 feet of radiologically contaminated soil, the artificial fill and the asphalt (2.5 foot depth interval), a total of 465 yds<sup>3</sup> ([5,017 ft<sup>2</sup> x 2.5 ft]/27 ft<sup>3</sup>/yd<sup>3</sup>) of soil is estimated to exceed Tier I SSALs.

Proposed Tier II SSAL exceedances in natural soils occur to a depth of 13.9 feet below the top of asphalt. Excluding the upper 1.5 feet of radiologically contaminated soil, the artificial fill and the asphalt (12.4 foot depth interval), a total of 3,428 yds<sup>3</sup> ([7,464 ft<sup>2</sup> x 12.4 ft]/27 ft<sup>3</sup>/yd<sup>3</sup>) of soil is estimated to exceed Tier II SSALs.

#### 5.7 SUMMARY OF MEDIA VOLUME ESTIMATES

This section summarizes volume estimates of soils exceeding Tier I and Tier II RSALs and SSALs, and includes 903 Pad asphalt and artificial fill volume estimates. Table 5-5 presents volumes of asphalt, artificial fill and soil exceeding Tier I RSALs and SSALs.

Table 5-5 Volumes of Asphalt, Artificial Fill and Soils Exceeding Tier I RSALs and SSALs

Area/Material	Exceedance	Volume <sup>1</sup> (ft <sup>3</sup> )	Volume¹ (yd³)	Volume <sup>1</sup> (m <sup>3</sup> )
903 Pad Soil	RSAL	34,243	1,268	969
903 Pad Soil	SSAL	12,573	465	355
Lip Area Soil	RSAL	43,166	1,598	1,222
Americium Zone Soil	RSAL	1,560	58	44
Total		91,512	3,389	2,590
903 Pad Asphalt	NA	74,052	2,743	2,097
903 Pad Artificial Fill	None	74,052	2,743	2,097
Grand Total		239,616	8,875	6,784

Volume represents materials in-place NA = Not Applicable.

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Table 5-6 presents volumes of asphalt, artificial fill and soil exceeding Tier II RSALs and SSALs.

Table 5-6 Volumes of Asphalt, Artificial Fill, and Soils Exceeding Tier II RSALs and SSALs

Area/Material	Exceedance	Volume <sup>1</sup> (ft <sup>3</sup> )	Volume <sup>1</sup> (yd <sup>3</sup> )	Volume <sup>1</sup> (m <sup>3</sup> )
903 Pad Artificial Fill	RSAL	2,813	104	80
903 Pad Soil	RSAL	66,707	2,471	1,889
903 Pad Soil	SSAL	92,556	3,428	2,620
Lip Area Soil	RSAL	142,211	5,267	4,027
Americium Zone Soil	RSAL	189,667	7,025	5,371
Total		493,954	18,295	13,987
903 Pad Asphalt	NA	74,052	2,743	2,097
903 Pad Artificial Fill <sup>2</sup>	None	71,239	2,639	2,017
Grand Total		639,245	23,677	18,101

Volume represents materials in-place <sup>2</sup> Excludes 104 yd<sup>3</sup> exceeding RSALs

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903 Lip Area, and Americium Zone	Date:	September 28, 1999
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903 Drum Storage Area,	Revision:	0
903 Lip Area, and Americium Zone	Date:	September 28, 1999
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903 Drum Storage Area,	Revision:	0
903 Lip Area, and Americium Zone	Date:	September 28, 1999
	Page:	A-1

Appendix A

**Boring Logs** 

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			LOGO VAL		SUP		SOR	w.	vol		DATE 8/25/98
могтов чог	UF COPE	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD	SAMPLE NUMBER	FRACTURE ARBLE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTH IN	\$011/ 1111/01.0GIC 1.0G	SAMPLE DESCRIPTION
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NCTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

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Materials amounts are estimated by % volume instead of % weight.
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NOTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

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NOTES: General, USOS is modified for this log as follows.

Materials amounts are estimated by % volume instead of % weight.

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

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NCTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

11) Badly proken core, accurate footage measurements not possible.

(2) Core preaks cannot be matched, accurate footage measurements not possible

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NOTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

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									7.0		
									&s		
									9.0		Rs = rad screen
,	10TE	M (1	ateriais 1 Badi	amou broke	nts are n core.	accura	ted by ite foot	% volu age me	me instead easuremen	ts not p	R= rads  Exact last of elevation FIDER earlings reight.

V

THE STREET STREET, AND THE PROPERTY OF THE PRO

<b>)</b> }	Bo Loc	rehole cation	Num	ber:	BH 9/3	9079	8		REHO		Surface Elevation: <u>5917 FF</u> Area: <u>903 Paol</u>
	Ge	ologis	t: عل	1077 Bert Ge	ath_		DEAL	ER	<del></del>		Total Depth: 3.6 A  Company: Tierra Project No.: GE 600000 C  Sample Type: Continuous core
		i&G l PRO			SUP 	ERVI	SOR				DATE 2/23/98
	TOP/BOTTOM OF CUME IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD	SAMPLE NUMBER	FHACTURE ANGLE	even + July BEDRIG ANGRE	GRAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN	\$011/ 1.11+101.0GIC	SAMPLE DESCRIPTION
	0.0	0,0	0.0	0.8	RS R Dup- Rs R	3030	-	PT Gm	0.8		Asphalt Black (10 YR 2/1), gravel, sand, organic binder, gravel to 1.5 cm, rounded fracture, dry Membrane sand Gravel mix, ogle yellow (2.5 y 7/4) gravel to 1.5 cm, subround bround, unconsoldated, moist,
	3.6 A.	3.6ft.	3,1 ft.	1.5	RS R RS RS	3.03 2.016 2.017		G¢	-1.S - -20-		Clay Sand Gravel, mottled-ttop) very dark grayish brown (10 yr 3/2) (middle) very pale Down (10 yr 8/4) (bottom) reddish yellow (5 yr 6/6), gravel to 4 cm, much gravel fractured, unconstidated, slightly moist.
	0,0	111	Recovery	3.5 No	rs r rs r	2.034 2.018 2.031			-2.5 - -33-		No Recovery 3.1-3.6ft.
	3.6			Scriple					4.0		
									5.0-		
									_ 、 _		
									- 60-		
									7.0		
									e.s		
					-				— 9.6— — —		
ا إ									0.5		*
	NOTE					dified fo			ollows: me instead	nt % w	RS = rad screen R = rads

Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

15

Bor Loc Dat Ge	ehole ation e: ologis	Num - Non 4/2	ber: h: -7 ∌/पु? Kol	BH9 4914 ≥HUE	10898 10Ea	} st: <i>≟?</i> }	085			LOG  Surface Elevation: 5977 ft  Area: 903 PAD/LTP max 4/25/98  Total Depth: 4.0 ft.  Company: TIERRA Project No.:GEG00000  Sample Type: CONTINUOUS CORE
		_OG( VAL	_		ERVI	•	Va	d		DATE 8/25/98
TOPBOTTOM OF COME IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE ININTERVAL (FIELD	SAMPLE NUMBER	FRACTURE ANGLE	BEDDING ANGLE	GHAIN SLÆ DISTRIBUTION	USCS	DEPTH IN	SOIL/ LITHOLOGIC	SAMPLE DESCRIPTION
Box lof 1 0:0-4:0 ft.	Run #1 0.0-4.0 A.	Recovery 2.4A.	001 003 004 005 006 008	9 日 4 1 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			NA GC	- 1.5.4- - 1.5.4- - 1.5.4- - 2.0.4- - 3.2.4- - 4.0- - 4.0-		0.0-0.4 Asphalt, black, fractured, mem brane at 0.2 A gravel up to 1 cm - rounded  0.4-0.9, fill, Sand and gravel, lightolive bown (2.575/2)  gravel to 1 scm, rounded med to coarse sand, uncon- Solidated slightly micrecous, moist.  0.9-1.4, Soil, Clay Sand gravel yeary dark graysish  brown (2.573/2), gravel to 3 cm, fractured, ig peous  rock frags-grantic in port, fineto medicing sand,  firm, unconsolidated, moist, arell graded.  1.4-24 Soil, Clay Sand, gravel, Yellow (10 yr 1/6) gravel  to i. Scn, rounded, mixed litterby-sine granitic, medicin  to coarse sand, unconsolidated, fire, moist,  No Recovery 2.4-4.0ft,  Some of gravel  "rotten"  1.0. = 4.0ft,
NOTE	S: Ge	eneral:	USCS	is mod	ified to	or this lo	og as fo	ollows:		

Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

18

HOLD AND ALL SANGERMANTS IN COMMISSION

Boo Loc Da Ge	rehole cation te:	Numb North	er: :5 RF 4/98 K6	BH EHL	Plogo LEas LDRT ER	(8 st: 2 t#	085 1491	41_	,	Surface Elevation: 5976 Ft.  Area: 903 PAD / UP 8/25/53  Total Depth: 1.0ft.  Company: TIERRA Project No.:6E600000
inC	lling Ed	quip.:	GEC	PRO	BE/	MAC	ROCO	RE		Sample Type:CONTINUOUS CORE
ł	3&G L PRO				`	`	0			DATE _ 8/25/98
OF CORE	TOP-BOTTOM Of INTERIVAL	FEET OF COFE IN HATERIVAL FIFED MEASUITEMENTS	SAMPLE NUMBER	FRACTURYE ATKILE	BEDDING ANGLE	GIVAILU SI ZE DISTIRIBUTION	USUS	DEPTH IN	SOILJ LILLKNLOGIC LOG	i
Box 10f 1 0.0-4.0ft,	Run # 10.0-4.04t,	Recovery 3,1 ft.	201 202 203 204 203 207 208 207 208 207 208	0.8 p:27 1.3 p:29 1.8 [0:2] 2.3 10:18 2.8	10:06 09:52 4.0ft. -125	-10:0	56	-0.5 <sup>4</sup> = -0.5 <sup>4</sup>		0.0-0.4; Asphalt black, prittle, rounded gravel up to 1cm, membrane at about 0.24t.  24-0.8; Eill; Sand and Gravel; Bown to develown (1948.4/3), gravel up to 1.5cm, grantic conducts morphic 0.8-3.1: Soil; Trock fragments, coarse sand, Clay-Gravel with minou sandy very derk grayish brown pyrstag gravel up to 3cm, fractured, granitic and quartite? York fragments, granitics votten, coarse sand grantic in party firm, unconsolidated, moist.  No Recovery 3.1-4.0 ft.  T. D.= 4.0ft  Note: Up to 15 ppm Fuxboro TVA and 16 ppm Mini Ree VOC's measured. Some Voc's present throughout Core. Maximum between 1.3 and 1.8 ft.

130

NOTES. General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.
(1) Badly proken core, accurate footage measurements not possible.

(2) Core preaks cannot be matched, accurate footage measurements not possible.

8	orehol	e Nun	nber:	BH	PLA 91098	}		REHO	DLE	LOG Surface Elevation: 5979 Ff Area: 903 PADATEM AL AL
G	ate: eologi: rilling E		35/	98_ iom		oE批i				Total Depth: 6.5ft. Project No. 6E 6 000000 Sample Type: Commons core MACROCORE
- 1	G&G PPAC				EAVI Le v	`		DATE <u>8/25/</u> 98		
10Praof1094 OF COLE	TOPMOTTOM	FEET OF CORE INHIFE AVAI	SAMPLE FRANCE	FLVAC, TURNE ATACH E	BEDDING ANGLE	GFAIN SLZE DISTAIBL/FIQH	USCS	DEPTH 124	SORJ Ulbern Olaic 1083	1
Box lof   0.0-6.54.	Run #2 3.5-6.5A, Run #2 0.0-3.54.	weny 2.8ft.	1.00.1 1.00.2 1.00.1 1.00.1 1.00.1 1.00.8	14 11:52 1:50 2:4 11:48 2:9 11:47 3:4		3.\$	6c 6m	34 34 34 34 34 35 -4.5 -5.5 -5.5 -6.5		D.O-O.5 Aspnatt, black, fractured/brittle.  0.5-1.4 (FILL) Sandard Gravel, olive brown (3.544/3) Gravel fractured to rounded jupto 1.5 Cm, frict oraclium SEND, poorly graded, conconsulated, moist.  1.4-2.6 (Soil) Clay Sand Gravel, dork redalish brown (5 yr 3/3), Gravel fractured to rounded upto 3 cm, Ignerias rock Fires ments (IRF's), fine sand, matrix frin brooks into blocks, slistly plastic, mist, less gravel than BH91593, moist  No Recovery 2.8-3.5 At Clay Sand 2.6-2.8 ft olive sand (2.5 y 6/8) in yellow Socious (10 yr 4/3)  3.9-5.9 ft. Clay/Sand/Gravel mothed light olive brown (2.5 y 5/6) dominant, gravel muchgreeter than clayor sand fractured gravitics up to 3 cm, fine sand, wettered gravitics up to 3 cm, fine sand, wettered massive, moist.
			1.010	20	Rinice			9.c		Diagram: Run #2  Core Liner  Empty top shoved of Burnle wall 1.4-2.67.  A few twice showed of Burnle wall 1.4-2.67.  Collapsed fill from 0.5-1.4ft.  Top of Run #2 in place material

NCTES. General: 'USCS is modified for this log as follows:

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<sup>(1)</sup> Badly proken core, accurate footage measurements not possible.

<sup>(2)</sup> Core breaks cannot be matched, accurate footage measurements not possible.

R	OCI	<b>(Y</b>	FLA	TS	PLA	NT	во	REHO	LE	LOG PAGE 1 OF 3	
Bo	rehole	Num	iber: <u>5</u> th: <u>174</u>	1911	98 1/529	t: -7	085	7-05		Surface Elevation: 5979 ft.  Area: 903 Pad	
Da	te: <u>0</u>	4179	<u>4.02</u>	1878	27 Las					Total Depth: 21.9 ff	
Ge	ologis Ilina E	t: <u>حل</u> auip.:	Baylo	prob		Dua	12			Company: Tiera Project No.: GEG00000 Sample Type: Continuous core	
			SING								
1		VAL		<u></u>						DATE _2/23/98	
M 3	WO -	. ×	ш с	Ψ	۳	₩ º	ā	ž	GG		
TOP/MOTTOM OF CUME IN BOX	OP/BOTTO OF	TOFC NTER FIELD	AMPL	ACTUR ANGLE	BEDDING ANGLE	GPAIN SIZE DISTRIBUTION	USCS	DEPTH	\$0!(7 110! 0(	SAMPLE DESCRIPTION	
0.0	0.0	0.0	Event			Sict	-	0.0	3	the hole and change of the Election manifes a	
	0.0		201/00	175 75			M3.	0,45		Asphalt-dry, chippy. Contain fibrars membrane.	
	,		001/0				SM			Fill-sand ~/ fine gravel, Sl. moist. Dk brown (104 n 3/3) to dk, yellowish bm. (104 n 4/4).	
	Runi	34	001/00	3 rJ		•	54/	1.e.7		Sand-silt mixture "/gravel to gravelly sandy sitt- poets of odi the common below ~ 200 1.8.51. noist.	
		1	001/00 001/02	4 P25			/GM	_	116	Vdk brown (104R 2/2) above 1.8 them mothed below	
	0.0-		001/00	7125				2.0-		"/dk brown (10YR 3/3) caliche (v. palebon, 10YR 5/3).	
	4.0		2.5 Ct. /00	_ 1						and other colors. To 3000 cpm on FIXER @	
		(	00:/07			į			9		
		一	3.1					3D			
			34	33-1				3.4	#IIJ	NO RECOVERY	
0	4.5	ч.	N/A					4.c	$\triangle$	NO RECOVERY	
a	ند)٬	4.0					Sin			Sandy, silty gravel - strong brom	
(	RUN								s E	(7.5 YP-5/6 to 1/6), sl. moist, scattered	
0,0	2:	40						- 5.0-	<b>a</b>	(7.5425/6 to 1/4), sl. moist scattered clay pockets. Abundant shattered gravels. No "hits" Eff color is	
		(-	11/12	[		į			(3	gravels. No "hits" Color is	
	4.0 -		1					, .	<b>a</b> 2	invttlede, but dominantly strong brown	
$  \mathcal{M}  $	ŏ.0							- 60	3) 5		
45									6 0		
0				·				7.0	40		
			7.4	72.S					<b>A</b>		
Box	<b>8</b> .0	. A	05.10	´					P		
改		9.0	0.0					— 62 —	9 6	Some as above 4.0-8.0' w/more rotti ng	
	3.								1	some as above 4.0-8.0, w/more rotting gravels. Color mostly lighter the sold about rock floor, shetted due to some to abondont rock floor, shetted gravels, rotting gravels. St. moist.	
90	8.0-	4.0	W/					q.c		shattered gravels, rothing gravels. St. moist.	
	10.0	Cincl.	ויש								
		Story)									
NOTE	=S+ G	eneral:	USCS	is mod	ifiea fo	r this le	og as f	ollows:	· III	In sample into: Rs = rad screen R = rads	
.,0,,	N	laterials	s amour	nts are	estimat	ted by	% volu	me instead		\frac{1}{2} - \frac{1}{2} \frac{1}{2}	
	(1) Badly broken core, accurate footage measurements not possible. (2) Core breaks cannot be matched, accurate footage measurements not possible.										

R	OCI	(Y)	FLA'	TS I	PLA	NT	во	REHO	LE	LOG PAGE 2 OF 3
Во	rehole	Num	ber: 6	31491	(98					Surface Elevation: <u>5979 ff</u> Area: <u>903 Pad</u>
Da	ite: <u> </u>	2189	8		£_Eas	si. <u>24</u>	785	<del>26-5</del> ——	•	Total Depth: 21.4 F+
Ge	eologis	اt: <u>ـــــا .</u> :quip.:	Boyle	m				<del></del>		Company: Tiera Project No.:GEG00000 Sample Type: Continuous core
<b> </b>				<del></del>	ERVI	SOB				
	PRC		anva	٨	2000	11				DATE
Σ	Z	y z		w .		w Z ₩ O		Z	GIC	
OF COHE	TOP/BOTTO OF OF	25.5	SAMPLE NUMBER	FHACTURI ANGLE	BEDDING ANGLE	GRAIN SIZE DISTRIBUTION	USCS	DEPTH	SOIU 1001 1003	SAMPLE DESCRIPTION
10 3 E	<u> </u>	FEET	κŽ	₹`	3	g G	, "	10.0	- 1 ( <del>- 1</del> (- 1	
1	10.0 RUN	(0.0	1.1/				6M	10.0		game as above, 8.0-10.0' Tone of five ones
	4:	爲	1/A	`				-		Collengavels. Most consumed by samples (1993)
	10.0-	3.1	11.1	2				- 11.C-		Clause sand of gravel - sl. moist.
	12-0		00.16	108 25			SC			Several altered or clayey rotten gravels. Mottled
	12.0	17.0	001/03	5√ m					177	Gentlatered or clayer rotten gravel - sl. moist. Gentlatered or clayer rotten gravels. Mottled colors, but mainly strongbrown (7.5446) of streaks of light olive brown (2.545/3). Some
S,						**		[2.0-		zones to sandy day /grand. Abrupt bottom Contact, fairly sharp upper.
5	RUN Si								1/2	Contact, fairly sharp upper.
	120	3.0					,	<u> </u>	VIII.	
0	14.0							17 5	H	
2							GM	(3.3	THE	Same as above, 8.0-10.0
	14,0	14.0					col	14.0 14.2-	17	and the property of the
8	PUN						SCI			Some as above, 11.1-13.5, w/increased gravel (to 6C)@14.2-14.7. Then SC to 15.7, GC to
1 ,,	6:	2.8	15.0	_				15.0		ιω.o.
15	(6.0)		20/20	9 125 52						
10			001/03		ļ					
×	10.0	ite-D	15.7 N/	~				160		Seme as above, 11.1-13.5. Sl. noist.
30x	RIN									,
	16.0-	2.5						in a		
	13.0	4.5	MA					(7.0 17.2		Sandy clay to clay sand mixture, offrace
17.5			, ,				CYSC			1) Meli stime, St. Small Colors is is
								180		11.1-13.5.
8	km									Same as above but none SC. St. moist. Tr. gravel. Sc portion & base of recovery.
82	8:	\5'	001/0	C (L5				<del>-</del>		1. 12 Recent January
30	180	(1:25) has 1:4	14.1	26 R	-			<u> </u>		12 by Cutter of their
30x		183 Y	00:/0					- 195-		TOP OF BEDRECK = 195
T -		Egytyku)	36.18	ii es				20.0	X	19.5 2000 Su rext program deception.
NOT	ES: G	eneral:	USCS	is mod	dified fo	or this l	og as f	ollows:	<del></del>	

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Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

	R	OCI	<b>Y</b>	FLA	TS	PLA	NT	ВО	REHC	LE	LOG PAGE 3 OF S
	Во	rehol	e Nun	ber:	BHO	11198					Surface Elevation: 5979 ft
'	Loc	cation	- Nor	th: <u>174</u>	906	£_Eas	st: 🅰	28.50	e8.5		Area: 903 Pc4 Total Depth: 214 FF
	Ge	ologis		Bay	an						Company: Tierra Project No.: GE 600000
					oprol						Sample Type: Continuous core
ı	EG	&G	LOG	GING	SUP	ERVI	SOR				, .
	AP	PRC	VAL		M.n	love					DATE 2/23/98
	5 u	WO.	¥ N	E R	ā.	2	GRAIN SIZE DISTRIBUTION		<u>z</u>	GiC	
	OF COME IN BOX	ABOT OF	OF C	SAMPLE	FHACTURE ANGLE	BEDDING	MINS	USCS	DEPTH IN	\$011/ 1111/01 0GIC 10G	SAMPLE DESCRIPTION
L	ģ 5 =	10F	FEET OF CORE ININGERVAL (FIELD	5	1	<b>±</b>	GP DIST	- vs		Ē	f
ſ	1	Ryn		20.2	2 of 3				20.0		Claystone to chystone "/silt-grayish somm (2.57 5/2) St. noist. Traces carbonaceous flicks in some zones,
ľ	4,5	100	3.1	1				1	L -	_==	Sand i gravel streamers@ ~0.7-1,1' below top of
	~ 'V	21.4		N/							core remaining after sampling probably due to gravelse contact falling into hall when core was lost in previous
	30x 3			A					ZI.C-		run. No hits. (Expect sands is rarels noted above to the out of place not inoriginal setting.) See logbook
	21.4	21.4	21.4	21.4					21.3		To recover 213212 not in original setting.) See lighook
Γ											TD=21.4' detailed explanation
									-220-		eflost core recovered
											core inported sands i
											gravels.
							1		230		
1	1										
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									7.4.0	.	
	,	1	1	1	- 1	1	1		30.0	1	

NOTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

EGGG LOGGING SUPERVISOR  APPROVAL  M. Warren  M. Warren  Sample Description  Sample Description  Sample Description  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  DT?  Sample Description  Sample Description  DT?  Sample Description  DT?  Sample Description  Samp		Bo Loc Da Ge	rehole cation te: ologis	Num - Non 0210	ber: h: <u>1</u> 99 Boyl	BH 1906	9120 Z Eas	18_		REHC	•	Surface Elevation: 5978 Ff Area: 903 Pad Total Depth: 3.5 Ff Company: Tierra Project No.: 6E600000 Sample Type: Continuous core	
And off day completes the property of the prop					SING		•	• •				DATE 2/23/98	
And the day Craphics of the Property of the Care of th		TOP/BOTTOM OF COME IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD AEAS! REMENT	SAMPLE NUMBER	FHACTURE ANGLE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIU LITHOLOGIC	SAMPLE DESCRIPTION	
Control of the contro		6.3		2.3	B.n.€	907(9)			PT?			get membrane to cother to book was the single corolise to	مورنغ مراثب
GM GMC 4000 GM GMC 4000 GMC 40			1:	26	1.0	4			5M	(£-		fill-sond of silt farable bower contact not as clear as licerus (17,922.51. most. Dk. yellowish brunchoze 44).	enerk.
10 to the state of		2/			1.5	9(2)			GM		•	to major compount. Very link brown (1042 2/2) above 18	
NO RECOVERY 2.6-3.5'  10-3.5'  Measured TD=3.6'		υπ ( 3,			20	(R, red) (R, dup)		,		z.o		mainly v. pale brown (10 /2 E/4). The pale coloris	
35  -40  -40  -50  -70  -70  -90  -90		× 0			iã	(FC)				2.0		Lowest O.1 shows Strong brown (7.5 425/3) pool which may become chominent color below 2.5!	Ŕ
- 40- - 40- - 50- - 60- - 70- - 90- - 90- - 10- - 90- - 90- - 10- - 90- - 10- - 90- - 10- -	ł	. }			4/2	·				30	X	NO RECOVERY 2.6-3.5'	
- 5.0— - 60— - 7.0— - 7.0— - 9.0— - 9.0— - 9.0— - 10.0— -	)	31.2									/		
	l											Measured 11)=3.6'	
- 7.c										S.O			
										60-			
9.0-										7.0-			
9.0-			-										
10.0										&s			
										9.0			
NOTES: General: USCS is modified for this log as follows:										ادف و بسالت مند بسیا		RS: radignery	

Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

3

Bo Lo Da Ge	ock prenole cation ate: eologist illing Eo	Numit North	er: 1: <u>7</u> 4 7/9	β# 9063 8 (G EHL	9139 Eas VY 4/	8 51: 20 52/98)	858		; -	LOG  Surface Elevation: 5977 F+  Area: 903 PAD / LIPAN  Total Depth: 4.0 ff «les/99  Company: TIERRA Project No.: GE 600000  Sample Type: CONTINUOUS CORE
1	G&G L PPRO	VAL.				- a	lar	S		DATE 8/25/98
TOPBOTTOM OF CORE	TOP-BOITOM Of RHERIVAL	FEET OF CORE INITALITYAL (FIELD) MEASURIEMENT)	SAMITE	FLACTURE ANGLE	BEDDING ANGLE	GHAIRI SLZE DISTRIBUTION	USCS	1999 FEE1	SOIL/ LIDENSEOGIC LOG	SAMPLE DESCRIPTION
Bux 10f1 0.0-4.06t.	Run #1 0.0-4.0A.	Recovery 2.4A.	003 003 004 007 008	5,8 11:12		MA GM GC		-0.4 -0.8 -1.9 -1.5 -1.5 -20 -3.5 -3.5 -3.5 -4.0	9	D.O. O. Y. Appartt, black, membron - Oboat O. 3 ft, ductike breaks into Slobs, rounded gravel up to 1 cm.  O. M. O. S. F. II. Sand and gravel up to 1 cm.  O. M. O. S. F. II. Sand and gravel up to the substitute of the provided of the prov
NO	TES G							tollows: ume instea:	of %	weight.

(1) Badiy proken core, accurate footage measurements not possible.

(2) Core preaks cannot be matched, accurate footage measurements not possible.

	Boo Loc Dai Ge	renole cation te: ologis	Num Non - S	ber: h: 7.4 /4/10 KO	BH 4906 18	9149 6 Eas	st:	2085			Surface Elevation: 5976 ft.  Area: 903 PAD/LTP surfactation: 4.0 8/es/s9  Company: TIERRA Project No.: BE 60000 0  Sample Type: CONTINUOUS CORE
			LOG( VAL			ERVI		al.	I		DATE 8/25/98
Le dedicalitation	OF COFFE INFOX	TOP/BOTTOM OF HITERVAL	FEET OF CORE INIMITERVAL (FIELD	SAMPLE PUMBER	FICK, JUNE ALKNE	BEDDITAG ANGLE	GIMITSIZE DISTRIBUTION	USCS	HEET DEPTH IN	SON/ LIDIOLOGIC	SAMPLE DESCRIPTION
	Box lot 1 0.0-4.0ft	Run #1 0.0-4.0ft,	Recovery 3,2 ft.	001 003 004 005 006 007	0.8 11:3 11:3 11:3 11:3 11:3 11:3 11:3 11:		1	NA 6M 6C	-3.5°	-	0.0-0.4; Asphalt black gravel up to 1.5 cm, rounded, membrane about 0.24t, brittle/fractured.  0.4-0.8; Fill; Sand and gravel; brown of and brown (100 R 4/3), remaining to feel and approximations associated from the consumption of the second second second of the consumption of the second of the consumption of the second second from the second

- (1) Badly broken core, accurate logtage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

Bo Lo G	OCI prehole pcation ate: eologis illing E	9 Num 3 / 3 3 / 3	iber: th: 24 25/9	BH 1898 8	9159 7 Ea R. Ka	0		REHO	DLE	Surface Elevation: 5980 ft Area: 903 PAD (the muxical Page I of I) Company: Tierra Project No. GE 600000 Sample Type: Commons core Microse
	G&G PPRC		GING		ERVI		_0			DATE
OF COLE	TOP/BOTTOM OF INTERIVAL	FEET OF CORE INITERVAL [FIELD	SAMPLE PRIMBER	FIVETURE	BÉDDRAG ANGI É	GIANIA SIZE DISTRIBUTION	USCS	DEPTH IN	SOu7 UD KN OGIC	SAMPLE DESCRIPTION
Box lot 1 0.0-3.54.	Run 14 1 0,0-3,5 ft.	Recovery 2.5A.	1.00.1 200.0 200.1 1.00 1.00 1.00	R 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	12:58 12:58 12:53 12:53		Anota+6 6 6	0.5 - 0.8 - 1.5 -		COO-D.8 ft, Asphalt black, Consolidated at top froctored 1 lower half.  0.8-1.5ft.(Fill) Sand and Grovel, olive bown \$6.594/3  subangular gravel, graviticand metromorphic, up to 1.5cm, finic to Gove sand, well graded, unco-solidated frield, crosist.  1.5-2.5ft (Soil) Clay Sand Gravel, very deal brown (104825) in top half, brown (1.5 yR 4/3) in both half, Gravel, frectured, up to 3cm, gravitic and quantity sees films such spok-lifemory Clay of the move samely clays  This socks top half blacks, well graded, male to  2.5-3.5 No kecoury  TD=3.5ft.

- (1) Badly proken core, accurate footage measurements not possible
- (2) Core breaks cannot be matched, accurate tootage measurements not possible.

							во	REHO		LOG PAGEOF
1	Borehol Location	- Norti	ber: h: 74	1989	11698 Eas	st: 20	856	84	4	Surface Elevation: 5979 FF
	Date: Geologi Drilling E	st: _ <b>R</b> Equip.:	KO SEC	EHLI PRO	ER Be/	MAC	Raco	RE	(	Company: TIERRA Project No. GELODO OO GAMPILE Type: CONTINUOUS CORE
1	EG&G APPRO			SUPI		SOR				DATE 8/25/98
TOPBOITOM	MOLIDAGOI OF	FET OF CORE INTIMETIVAL (FIELD)	SAMPLE NUMBER	PTACAUME ATRICE	BEDDRAG ANGLE	HOHOBRITSHO	USCS	DEPTE IN	SOL/ 111401 OGIC 10G	SAMPLE DESCRIPTION
							NA	0.5		O.D-O.S. Asphatt, black gray, tractived-unusually powdery, fractived gravel up to lory, granitic and metamorphic rock.
Dyn-cy (J') x B	Par #1 0.0 - 4.0A,	1	1	0.9 11:438 1.9 11:38 1.9 11:32 2.9 Red S Rins Rod I	Į.	1	6M 6C	- 1.5.9 - 1.5.9 - 2.6.9 - 2.6.9 - 2.6.9 - 2.5.9 - 3.5.9 - 3.5.9 - 4.5	<b>9 9 9 9 9 9</b>	D.5-0.9: F. II, SIND and Gravel, 113ht yellowish brown look 44, rounded granitic and metamorphic rock frags, rounded, RPK 5/4788 0.9-3.4: [Minconsolidated, dry, Chouse Sound Soil; clay, sout, gravel; very fack grayish brown (DVR 3/2) at top grades to dark reddish brown (54R 3/2) at bottom; gravel to 3 cm, fractured, rottengennitic rock fragments and quartetes, fine said vareconce sand, from to hard, unconsolidated, slightly moist to dry.  No Recovery 3.4-4.0 ft.  T. D. = 4.0 ft.  Note: Sample interval 0.9-1.4 hoch high & and 8-vay readings
							-			8=28,000 countsperminute with fidaller.

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate tootage measurements not possible.

							во	REHO	LE	LOG PAGE OF 1
Lo	cation	- Nort	h: 71	1898	9 Ea:	19 st: 20	085	<del>259</del>		Surface Elevation: <u>5978 FF</u> Area: <u>903 Pad</u>
Da	te: <u>_</u>	) <u>Z ()</u> cit: <u>J</u>	198					-		Total Depth: 3.0 ft Company: Tiera Project No.: GE 6000 00
Dri	lling E	quip.:	Ge	oprot	<u> </u>			<del></del>		Sample Type: Continuous core
EC	3&G (	OGO	SING	SUP	ERVI	SQR		***		
AF	PRC	VAL		W,	No	rel	<u> </u>			DATE 2/23/98
TOP/BOTTOM OF COME IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL	SAMPLE NUMBER	FHACTURE ANGLE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN	SOIL/ LIMPOLOGIC	SAMPLE DESCRIPTION
0.0	0.3 0.3	0.0	NA					0.0	X	NO RECOVERY 0.0-0.3
	RW	0.5	interior in the second	201-6			M.S.	0.5	1	Asphalt - crambly, dry chips,
	2:		1:1	002-R	1		SM	c		Sand of 51H & gravel - dry to sl. moist VF-med sand fine gravel nearly. Bram (vorest/3). Looks like artificial
3.0	0.3 <sup>-</sup> 3.0	2.1	bonze	003-R	>		66	1-1-		Gravel y sand a day to daying fravel. Dry tost no
40.	5.0		Some.	005 - R.						to 14,000+ & @ 19.2.5' Also silty zones. Matrix to vider brown (1042 2/2). Abundant colicus
Box 1	·		2.0	27-29				2.0-		(as discrete poils) below 2.0', where graves is discreased relative to Fires. Almost entirety conscious
Š			2.4	00G-R				2.4.		No Recovery 1971 Sandles Sand South
3.0	3.0	3.0	NA					3D		No receivery by samples. Some portion 2.4-3.0' especially below 20', to GM
										TD = 3.0' (Measured TD = 2.95!)
		-								
							·	4.0		
								5.0		
								_		
					.			6D		
								_		
								7.0		
				İ				7.0		
.								<u> </u>		
								_		
		ĺ								
								9.0-		·
1										
								; o.s		
NOTE				is mod				ollows:	of %	Sangle types: RS= rad screen R= rads

Materials amounts are estimated by % volume instead of % weight. (1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Dr Dr	cation te: cologis	Num - Non - Vor -	Der: h: <u>74</u> 38/ Kol	TS BH 1899.	9189 2 Eas <b>E</b> J	18 st: 2 MAC)	0859 80C6)			Surface Elevation: 5977 FF  Area: 903 PAD/LIP MUSIC/58  Total Depth: 4.0FF  Company: TIERRA Project No.: GE 60000  Sample Type: CONTINUOUS CORE
AF	PERC	VAL		70	<u>en k</u>	- 6	100	d		DATE
TOP-BOTTOM OF COPE HUBOX	TOPAROTTOM OI: WIERVAL	FEET OF COPE INIMERVAL (FIELD	SAMPLE RUMBER	FIM. TURE ARSI E	UEODITIG ANGLE	GHAINSIGE UISTRIBUTION	USCS	OEPTH IN	SOIL/ THERMORIC	SAMPLE DESCRIPTION
			002	10:07			NA	-0.5		approx 0.3ft, gravel to 1 cm, rounded and fractured
off.	#		206	10:04 1.1			<u>C</u> M	1.0,1-	5	10.6-1.1 Fill, Sand and Gravel, lishtyellowish DONI (NYR 6/4), medium-scoorses and donnisatin top nath gravel. to 1.5 cm daminatin butombalt, gravel fractional, granilly
0.0-4.0ft	-d'o	4	න7	10:12 1.4 10:06			60	1.51.5		1.1-2.0 Soil, clay sand gavel ( Un consolicisted, clay to slightly most.) Very dark averich brown (10/23/3), graved to 2.5 cm, fractived, amnitic Ignesia suck frag., medium to coarce. Sand, firm, day to slightly mast.
	4.00-4.00	C.E.	010	2.1 10:24 2.1			SC	<b>- 2.</b> 5.7		20-2.7, Sall, Clay Sand, Vellar (104R7(6), fine tomod. sand, Caliche?, crumbly, slightly moist.
Bux lof 1	Run #1	Recovery	012	10:03 3.1				-3.5 -		No Recovery 2.7-4.0 A.
								-4.0		T.D. = 4.0A.
		The second secon						s.o 		
								<b></b> √.0-	-	
								— o.(—		
		e sum e e e e e e e e e e e e e e e e e e e								
		and the control of th						<b>8</b> .0		
1								<del>_</del> 9.0 —		
	a de la composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della comp		-							

- . 1) Badly proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

m Jog	orenole ocation ate: eologis rilling E	Num - Non 4	ber: 74 297 Kol	BH 18991 18	9199 2 Ea R	8 st: <i>⊒</i> 2	085			Surface Eleva	PAD/LIP 4.0ft. IERRA	8/25/9 Project No.	ECF
1	G&G PPRC		EING		ERVI		1	2	: 	DATE	8/25	5/98	
TOPBOTTOR OF COFE	TOPMOTTOM OF	FEET OF CORE IN IN THE AVAI (FIELD	SAMPLE	FHAC TORE ATAST E	BEDDITAS ARGLE	GIANTSIZE DISTABATION	VSCS SYMBOL	M HEAR	SOIL/ LITERIOGIC LOG			DESCRIPTIO	)
Bux 1061 0.0-4,0A.	J.0-4,0A.	Recovery 2.7ft.	001 002 0034 005 005 005	in t			MA 6M 6C	- 0.5 1.0 1.5		10984/3), mina	sandand grand round land claysand It dark grands I bun (5783/2) yuntette rock f , 5 charally moss sand-TRACE avel to 1 cm, fi	ively Drown to word, med too who had to a so a server work to a server wor	Juithderk 1, moist Juithderk 1, Sincto Medium 0.9-1.9.

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

Bor Loc Dat Geo	enole ation e: ologis:	Numb North	er: : 7 4 2 7 /9 8	BH 8913	9209 _Eas	18 t: <i>2</i> .0	95	·		Surface Elevation: 5980 ff Area: 903 PAD/LIP and 8/25/58 Total Depth: 4.0H. Company: TIERRA Project No.: 6E 60000 Sample Type: CONTINUOUS CORE
EG	&G L	.OGG	ING	SUPS	ERVIS	SOR		d	·	DATE 8/25/98
		VAL.		,,,,,						
101°80110M OL COHE R180X	TOPBOITOM OF RRIERVAL	FEET OF COPE IN HAIERVAL (FIET D AEASUMEMENT)	SAMIY E NY IMBER	LIVA. TURE ATKRE	BEDDING ARSI.E	GPMINSIZE DISTRIBUTION	USCS SYMBOL	OLPW IN	SUIT 1061C	,
							NA	-0.5 -		gravel less than I. och provided, no obvious membrane.
#				0.9			6M	0.9_		05-0.9: Fill, Sand and Gravel; dark yellowish Drownloyry 4) roundedgravel up to Icm, coarse sand, unconsolidated, moist
50	it		००१ ००१	13:37			60			0,9-3.1: Soil, Agravellithology mixed metamorphology and agranitic rock fragments
0.0-4,0,0	to-4.0A	,	003	1.4 13:34				1.61.4=	1	clay, sand, gravel, top is dark reddish brown (5 YR3/7) grading down to white (10 YR8/2) at bottom, gravel up to 3 cm, larger preces fractured, smaller pieces rounded, metamorphic and rotten granitic clasts, medium grained sond, granitic in part, crumbly, slightly moist, caliche heavy in lower 1.5 ft.
00	7-	4	004 005	1.9				-2.o.g-	9	white (loyes/a) at bottom, gravel up to 3 cm, larger
1	0,0	<u>~</u>	oo 6	13:32 2.4				- 2.3.4 <u>-</u>		and with granitic clasts, mediun grained sand, granitiz
to			008 008	12.25				1		I in part, crumbly, slightly moist, calliche heavy in lower 1.5 ft.
	#	RECOVENY		الما				3.0 3.1-	•	
Box 10f 1	Runt	Rec						- 3.5 -	X	No Recovery 3.1-4.0A.
							ļ	4.0	<u> </u>	
								4.5 -		T.D.=4.0ft.
	ı							<u>-s</u> o -		
								- 5.5 -		
								-co-		
								- 6.5 -		
								7.0		
	-							7.5 -		·
								7.0-		
								- 8.5 -	1	
		-						- م		
								- 9.5 -		
NOT	ES. G	! ieneral:	USC	s :s :mo	dified f	or this	log as	tollows:	<u></u>	

Materials amounts are estimated by % volume instead of % weight.
(1) Badiy proken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible

- 1	OCK rehole				2198	NT	ВО	REHO		LOG PAGE LOF L Surface Elevation: 5979 FF
Loc	cation -					t: 20	2856	84		Area: 903 PAD/LIPAW 8/25/90 Total Depth: 4.0ft.
l Ge	te: ologist Iling Ed	:: _ <b>R</b> .	KÓ	EHLE PRO	FR Be/I	MAC	Reco	RE	(	Company: TIERRA Project No.: GE 600000D Sample Type: CONTINUOUS CORE
ı	&G L				ERVIS		u).	2		DATE \$25/98
OF CORE	TOP/BOTTOM OF HHERVAL	FEET OF CORE IN WILLINVAL (FIELD)	SAMPLE NUMBER	FILMC TUPE ATHRI E	BEDDING ANGLE	GRAIN SIZE DISTRUMOR	USCS	DEPTH IN	SOIL/ LIDENIOGIC LOG	SAMPLE DESCRIPTION
		- 3					NA	24		0.0-0.4: Asphalt, black, brittle, tractured, rounded gavel up to 1cm, membrane at 0.2 ft.
			ool	0.7			6M	-0.504 07-	0 9	04-0.7 ft: Fill; Sand and Gravel; dark grayish bown RM/51948 (10 YR4/2) rounded gravely to to
0.0-4,04	T T		003	12				1.2 -		(10 YR4/2), rounded gravel up to 1 cm, gravel graintiz in part, coase Sand, unconsolidated, moist
2-4	4.0	工	205	1.7				1.57-	•	1 3011 Clay.
1	0.0-4.0ft	3.4	007	11:06 11:06				-2.0 2.2-	•	Sandand gravel; dark reddish brown (5483/2-3/3) gravel upto 3 cm, fractured, rotten granitic and micageous metamorphic rock fragments, medium
Box lof			028	2.7				- 2.5 - 2.7 -	•	sized sand_micaceals, unconsolidated, firm, well graded, slightly moist.
X	Rin #1	Recovery						3.0 —	6	
ď	Rich	8					_	- 3.5 <sup>3.4</sup> =	X	No Recovery 3.4-4.0 ft.
								4.0		-D -(1 - G)
								- 4.5 -		T.D. =4.0ft.
								<u> </u>		
								- 5.5 -		
								<u> </u>		
								- 6.5 -		
			-					7.0 —		
								- 7.5 -		
								7.0	-	
		]						- 8.S -		
								aP	1	
								9.5 -	1	
	1 .	<u> </u>	1	<u> </u>	1	<u> </u>		1		

Materials amounts are estimated by % volume instead of % weight.

(1) Badiy proken core, accurate footage measurements not possible.

(2) Core preaks cannot be matched, accurate footage measurements not possible.

	Boo Loc Da Ge	rehole cation te: <u>6</u> ologis	Num - Nort 27.04 t:	ber: h: <u>74</u> 4 <b>98</b> .Boul	B H 8914	92; Ea:	298		REHC		Surface Elevation: 5977 ft  Area: 903 fad  Total Depth: 3.0 ft  Company: Tierra Project No.: 6 E 600000  Sample Type: Continuous core
		&G L				ERVI	_				DATE 2/23/98
TOP/BOTTOM	OF CUPE INBOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD MEASUREMENT)	SAMPI E NUMBER	FHACTURE ANGLE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LIMPOLOGIC LOG	
; / y	0.0-3.0	250 3.0 2.0 3.0 3.0		ALLA EVEN BOTTLE COTTLE COTTLE COTTLE BOTTLE BOTTLE BOTTLE	7= rods 8= rod 5= rod 6= rs. 3= rod 4= rs.	sover	1	Aradel SM GC	0.0	X	NO RECOVERY 0.0-0.3 (solid point bit)  Asphalt-crumbly black.  Fill-send w/silt fire gravel. Light gellandstocom  [C.54 W.S.). Dry.  Smily, silty gravel. Consumed by samples.  Dry. Some to abundant rock flour, abundant shaftered gravels.  Claying gravel to gravelly clay. I allimish recovered by smill tracks. Mode and the state of the solid tracks. Mode and the state of the solid tracks.  NO RECOVERY 2.3-3.0 Stiff Sl. moist.  TD=30'

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

	Bo Lo Da Ge	renolecation te:	Num	ber: h: <u>74</u>  28/  Ko1	134 1891 198 211CE	923° Ea R	98 st: 2	085	REHC 834		Surface Elevation: 5976 Ft.  Area: 903 PAD/LHP 2012 1/58  Total Depth: 4.0ft.  Company: TIERRA Project No.: GE 600000  Sample Type: CONTINUOUS CORE
		&G PRO	LOG( VAL	SING	SUP	ERVI	SOR.	000	l .		DATE 8/25/98
TOPBOTION	OF COLD	TOPAIOT TOM OF	FEET OF CORE INIMITERVAL (FIELD	SAMI'I E RUMBER	FRAL, FURE ATAST E	BÉDDIIAS ARGI E	GHAIN SIZE DISTRUMUTION	USCS	DEPTH IN	\$OII/ 1111#31.0GIC 1.0G	SAMPLE DESCRIPTION
		10h +>0,4-0,0 (#mp)	Recovery 2.9 ft.	001 002 003 004	1.3 13:04 1.8 13:02 13:02 13:58 13:58 13:58	<b>х</b>	4B 1810	NA 6M 6C	1		0.0-0.7 As phalt, black, brittle-fractioned, granel to Icm, randled, Membrane at about 0.2 ft, dry  0.7-1.3 Fill, Sand and gravel, light yellowish bown (10 YRG/4), Minorgravel to Icm-rounded, mcd-consections, chicasolidated, dry  1.3-29 Soil, clay, sand, gravel, brown to druk brown (WYR4/3), fractured gravel to 3cm, granitic rock frag, questet to, minor sand-fine tomadium, firm, unconsolidated, slightly moist  No Recovery 2.9-4.0 ft.  T. D. = 410 ft.

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

	ROCI Borehold location Pate: Beologis Brilling E	Num - Non - Y/	ber. 29/ Kol	B) 4891 48	H92 SEa R	498 st: 2	१०४ ड			Surface Elevation: Area: 903 PA Total Depth: 900 Company: 166	5976 ft. D/LHF max 8/2	No.:GE600000
=	G&G PPRC	LOG	SING		ERVI			2		DATE	-/ /->	
TOP BOTTOM OF COLD	TOPAUTIOM OF UNITED STATES	FEET OF CORE INITERVAL (FIELD	SAMPLE HUMBER	FISAL TURE ALASTE	BEDDITAS ANGLE	GIWITSIZE	USCS	DEPTH IN	SOIL/ LITHOLOGIC LOG		SAMPLE DESCRIP	PTICN
Box 1061 0,0-4,0A	0,0 -4,0tt	Recovery 2.9 ft.	001 002 003 004 005 005 007 007	1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1	reen Ri sotope R	152 40	NA 6M 6C			gravel,  a.s-1.1 Fill, sai  (loyr 5/4), minor  to coarse saho  1.1-2.1 Soil, gravel  gravitic rock fr  moist.  2.1-2.9 Soil, clayrish brown (1048  much less gravel than  to 3 cm, fine	the black, brittle,  and and gravel, yell,  rounded gravel ap  ly, un considered,  avel downing the wift  k grayish brown (10)  agreeds apto 3 cm,  ay sand gravel, 2.  3/2) gradets yellow (2)  1.1-2.1, fractured gr  sand, calliched, fire  2.9-4.0 ft.	tolisch Drown tolisch, medium slightly moist minar clayand (R3/2), fractured crumbly, slightly 1-2.6 very dark .c-2.9 (10 VR VC), amitic fragments my slightly moist.

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

E	oreholi ocation	e Nug	iger in: 47	BH9	2599 Eas	St: 2	0951	REHO	855	Surface Elevation: 5978 ++ Area: 903 PAD/LIP Area
(	ate: 2 leologis rilling E	st: 🚣	3.46	2000 p	?、Kot	Ja/o HLE Dn	R	<u>710</u> Ja11		Total Depth: 18.5 ft  Company: Tierra Project No.: GE 600000  Sample Type: Continuous core Dept Wall
1	G&G .PPRC			SUP	_	SOR ~	1	L		DATE 8/25/98
TOP/BOTTOM OF COME	TOP/BOTTOM OF	FEET OF CORE INITERANI	SAMPLE NIMBER	FINCTURE ANGLE	BEDDING ANGLE	GFMIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LTLIKOLOGIC LOG	SAMPLE DESCRIPTION
Box 10f2 0.0-10,0ft	6 Run # 3 7.0-10.04. 6 Run #2 4.0-7.04. € Run #1 0.0-4.04 (46.5ineles)	Recovery 2,6ft, Recovery 3,0ft, Recovery 2,6ft.	RS RS POARS RS RS 4.0	1.003 1.003 1.003		#s	6 m	- 1.5		DO-03+1. Sand and Gravel, list yellowish brown (8.57/4):  Dis-0-6+15 Rock flow with median sand, quartered amilia Sand and gravel, serving any law inconsolidated,  Oil-3-6+1. (1048/6/2) median sand, is necess rack gravel, sand A.A., gravel apples and is necess rack gravel from to 2.5cm, tactually, fibrous membrane dark yellow unconsolidated, with adhering Caliche brown (10484) dry  Tare yellow (104846); median angular sand quartered to gravel apples 5cm, angular be fractived compaced to 13 rack frags and quartert; clay/sand adhere  No Recovery 2.6-4.041. (rumbly of fractived gravel but Crumbly of fractions of quartered gravel y unconsolidate fines slightly moiot.  TO as of 2/33/48  4.0-7.0 ft; sand and gravel, minar clay; gravish orauge (10487/4) to moderate reddish orauge (NR 6/6), medium angular quartered gravitid.  Sand, gravel up to 2 cm, fractived and angular composed of grantic and quarterite rack fraguest unconsolidated, duy to slightly moiot.  White coust on some gravel may indicate callish orauge (1086/6), medium angular quartered ignesses rack fragment sand, less gravel than about amounted yearl decreates downward, gravel mostly quartered yearl decreates downward, gravel mostly quarter trace vounded, unconsolidated), moist  4.0-9.6 Clay sand, sand dominant, moderate raddish orange, medium angular, quarte and ig rock frags, No Recovery 9.6-10.047.

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

	l Bo	المطعا	a Nun	ahine	RHO	2002			REHC	LE	LOG PAGE 2 OF 3 Surface Elevation: 5978 ff
)	Lo	cation	- Nor	th: <u>74</u>	906	Eas	st: <i>20</i>	985°	560		Area: 903 PAD/LIP Area
	Ge	ologis	st: عط	Boyl	oprot	RIKO	EHLE	X.	الـه		Total Depth: 18.5 ft.  Company: Tierra Project No.: GE600000  Sample Type: Continuous core Dual Wall
		&G PRC			SUP	ERVI	SOR	)	2	·	DATE 8/25/98
	TOP/BOTTOM OF CURE IMBOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD	SAMPLE NIMBER	FHACTURE ANGLE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTIL IN	501.7 1111/01 0GIC	SAMPLE DESCRIPTION
	10,0-8.54.	Run #4 10.0-13.04	Recovery 3.64	13.0 Rs R Voa 13.5	1.497 1. <b>49</b> 33 1.035			SC	12.0		10.0-13.0 Clayey Said, yellowish red (5 yr s/6), medicin to coarse grained, graniticand quartz grais, well graded, firm, plastic (forms Sousage like extrusion on caring), moist.  - 0.1 ft gravel lense, fractured pieces apter &cm. possibly quartite, no fines.  - 0.1 ft gravel lense as above.  13.0-15.5 ft, Similar to above but pgravel appears to be more quartitic than granitic.
	130x 30f2 10,0-8.5.	54 Elun #5 13.0-16.0A	Recovery 3.5ft	16.0° RS RSA YOA-	.003  .033  .036			Sond	14.0 15.0  5.5		appears to be more quarteritie than grantice (quarteritie) throughout.  Gravel fragments up to 2 cm.  15.5-16.0 No Recovery  16.00 = Bedrock Contact.  16.0-18.5 ft. Fine to Mediun grained Sandstone, probably
		FRun#6 16.0-18.5A	Recovery 4.0ft	YOA- Dup 16.75	1.337				- 16.75 17.0		16.0-18.5 ft, Fincto Mediun grained sondstone publishy clayer, yellowish brown (1048 5/6) is dominant, some light gray (1048 7/1) at top, well sorted, unconsolidated to lightly industrial (crumbles easily), dry to slightly amist, massive
  -									20.0		

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

	RC	ROCKY FLATS PLANT BOREHOLE LOG  Borenole Number: BH92698  Location - North: 148971 East: 2685551  Area: 903 PAD/LIP Area													
								585	<u> </u>		rea: 403 PAD/LIP Area				
	Date Geo	e:	<i>- 5/1</i> · R	19798 160	EHLE	:R				7	otal Depth: 3.0ft. company: TIERRA Project No.:GE600000				
	Drill	ing Ec	uip.:	GEO	PRO	BG/I	MACI	१४८०।	RE		ample Type: CONTINUOUS CORE				
		&G L PRO			SUP!			Von	d	·	DATE 8/25/98				
<b> </b>	S E C	TOM AL	OFE VAL WENT	n E	¥	e é	SIZE MION	s č	<u> </u>	) GIC					
	OF CORE	TOP-BOTTOM Of INTERVAL	FEET OF CORE INITIERVAL (FIELD MEASUNGMEN	SAMPLE	FRACTURE ARGE	BEDDING ANGLE	GPWIITSLZE DISTRIBUTION	USCS	DEPTILIN FIEL	SOIL/ LITHOLOGIC LOG	SAMPLE DESCRIPTION				
	4			00) 002	12:05			6M	.A.Y	d b	0.0-0.4 A: Fill: Sandle Gravel: brown (7.5485/3) rounded gravel to 2.5cm, incline grained sand, well graded,				
	Bux 106/ 0,0-30A	-3,04	<b>#</b>	003 004 010	D:03			6c	-0.504-	0/	0.4-2.5 ft: Soil Tgravel in cludes granitic and mater- clay, said, gravel murphic rock frags, unconsolidated				
	0,0	1	24	~~~	12:00			·	1.0.9_	1	doub reddid hand dry, trace root heirs.				
	\frac{1}{2}	Run#10,0	0	007	1.4				- 1.5	<b>6</b> /	(5 YR 3/3) with speckled veddish yellow (5 YR 7/6) between 1. Sanda.2				
	)0	75	Recount	800	1.9				2.09_	8	ft., gravelupto 3cm, functived, mostly quartites, minor mediumato convse. ) sand, pourly graded, firm, unconsolidated, slishtly motet				
	ð	<del>ب</del> ک	(C)						- 2.5 -	0	Min Constitution of the state o				
	8	مکة	8						_3.o	X	No Recovery 2.5-3.0ft.				
				011	12:15	Rns	40ml Ask	Water			T.D. = 3.00%				
				012	12:15		Igall		– 3.s –		1, 0, - 3,0(7,				
							Poly		4.0						
									_ 4.5 _						
									<u></u> حہ						
									- 5.5 -						
									c.o						
					-				- 6.5 -						
									7.0 —						
								i	- 7.5 -						
									<b>7.</b> 0						
									- ۶.۶ –						
									ap						
									- q.5 -						
			·				1		7.3						

Materials amounts are estimated by % volume instead of % weight.
(1) Badiy proken core, accurate footage measurements not possible.

(2) Core preaks cannot be matched, accurate footage measurements not possible

R	OCK	YF	LA				во	REHO		
	renole cation				2798		085	<u>~~</u>		Surface Elevation: 5980 ft.
Da	te:	5/1	8/95	}					7	otal Depth: 3,04.
Dri	ologist Iling Ed	:: _ <b>R.</b> quip.: ;	GEO	PRO	BE/	MAC	Roco	RE		Company: TIERRA Project No.: GEG00000 Sample Type: CONTINUOUS CORE
EG	&G L	.OGG	ing					,		, ,
AF	PRO	VAL.			ma		w	ovol		DATE <u>\$/25/98</u>
TOM VÆE:	110M	CORE NVAL (D MEN)	4 E	1.E	ING St.E	ISIZE	SS	DEPTITE IN	U OGR.	
TOP BOT TOM OF CORE	TOP-BOLTOM OF INTERVAL	FEET OF COPE INTREPOAL (FIELD MEASUREMENT	SAMPLE NUMILER	FLUCTURE APARTE	BEDDING ARSE	GIVIII SIZE PISTI (IBUTION	USUS	OPET	SOIL/ LIPENIOGIC. LOG	SAMPLE DESCRIPTION
		<u>. 3</u>	001 002				6M	0.11	0 8	granitic gravel broker population from 1 (104R 5/3) granitic gravel broker population from 15 medium to Consider Sands unconsolidated trible dvy) root have.
Bux lof 1 0,0-3,09	0.0-3.04		063	0.4			GC	0.4		0.4-2.6ft Soil; dark reddish brown (5/R3/2)
3.	3,6	T	005	0.9				1.09-		grades to reddish gray (5 yr 5/2) at 1.5A., 1.5-244 yellowish red (5 yr 5/c); gravel, sand, clay;
0,0	Ò	3.64	006	1.4				1.4-		Suntry d gravel up to 2. Scm. look (like mostly)
-	1	7.0	003	1.9				1.9_	0	duritate redicin to coare sand not abundant
10	Runt	Recovery						PPK P	40	duantzite nedium to coase sand, not abundant; Caliche - 0.2 A intervals at 1.2 and 2.3 As firm, unconsolidated, well graded, slightly moist
XoX	(2)	eco.						- 2.3]=		to avy.
	CE.	8					ļ		X	2.6-3.0 ft No Recovery
								- 3.5 -		
					·					
								4.0	1	
								- 4.5 -		
								<u>- مک</u>		
								- 5.5 -		
								(.o		
								L.5 -		
								7.0 —		
								7.5 –	1	
								8.0-	1	
								- 8.5 -	1	
								-9.p -		
								<b>- 9.5</b> -		

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							ВО	REHO	LE	LOG PAGE OF 1
Boo	enole ation e:	Numb North	er: i: <b>17</b>	14 (i 38 30	9289 Eas	18 st: <i>20</i>	085	703		Surface Elevation: 5978 Ft. Area: 903 PAD/LIP Area
Dat	e: ologist	5 / <b>5</b>	12/9	§ ≈ 11/4	- -D					Total Depth: 3.0 ft.  Company: TIERRA Project No.: GE 600000
Dril	ling E	inib":	GEC	PRO	BE/	MACH	OCORE			Sample Type: CONTINUOUS CORE
i	&G L					SOR	w	1		DATE 8/25/98
<b> </b>				i			Ī	7 \	<u></u>	
TOP BOTTOM OF CORE BABOX	TOPBOTTOM OF INTERVAL	FEET OF COT INITATIONA (FIELD HEASUNEME	SAMPLE NEWBER	FRACTURE ARBLE	BEDDING ANSLE	GHAIN SIZE DIS FRIBUTION	HSCS SYMBOL	DEPTI IN	Soll Soll	· I
t t				0,5	(	(C)- RPK S/12/98	ZAK	# Hine fu	7	0.0-0.5 ft; Fill, Clay Sand Gravel, derke grayish, brown (10484/2), gravelupto 3 cm, fractourd, gran, tiz in pet, medium to coause sand well graded, frieble, unconsolidated, shishtay
-3.04.	4	,	001 002	11:46		5/12/98	GC	-0.5=	<b>6</b>	O.5-2.4 ft: Soil Timuist to moict clay, sand, grand, darle reddich brown (2.5 YR 2.5/4),
0.0	0-3.0A.	2.4ft.	003	11:44				/. <b>•</b>		gravel to 3 cm tractured, grantical micaceous
-	0.0		005	1.5 11:42				_1.5		gravel to 3 cm, fractured, granitic and mice ceous metamorphic for greents, poorly graded, medium micaceous sand, trace coarse, from to hard, possible caliche is lower 1 ft., slightly moist.
Box lof1	五	Reavery	237	2.0				20		12 lower 1 tt, slightly moist
X 00	Run	ر د در	008	11:39 2.5				_ <b>2.</b> 2.4		
2	∞	R						<b>3</b> o	$\rfloor X$	No Recovery 2.4-3.0ft.
								-35		T.D. = 3.0ft.
								1		
								4.0 -	7	
									1	
									-	
			•							
								-	1	
								<u> </u>	-	
								<u>_</u> .		
						İ				
									7	
								<u> </u>	-	
								-	_	

<sup>(1)</sup> Badly proken core, accurate footage measurements not possible.

<sup>(2)</sup> Core preaks cannot be matched, accurate footage measurements not possible.

	R	ac	KY	FLA				ВС	REH	OLE	LOG PAGE CF
	3o	rehol cation	e Nun	nber: th・ク	BH9	<u>129°</u> 3∕Œa	st:2	085	853		Surface Elevation: 5976 ft  Area: 903 PAD/LIP A can
	Оa	te:	3/83 st:	3/98			EHL				Total Depth: 2.5ft. Company: Tiera Project No.GE 400000
	Ori	iling 8	st. <u> </u>	Ge	oprot		<u> </u>				Sample Type: Continuous core MACKOCOKE
			LOG		SUP	ERVI		W	-l		DATE 8/25/98
TOPABOTTOM	OF COLE	TOP/BOTTOM	FEET OF CORE IN INTERVAL	SAMPLE PUMBER	FILM, Turke ANGLE	BEDDING	GIVAN SIZE DISTRIBUTION	USCS	DEPTH RE	SOIL/ Lifekal Odale, LOSS	SAMPLE DESCRIPTION
		#		1,00)	11:06			GC	0.0	9/2	0.0-2.2 ft; Clay/Sand/Gravel, dark reddist brown (2.5 VR 2.5/4) with mothling of
'	ار د	.a.s#	#	1,003	11: 04				- >.< -	9	Yellow (10YR 8/8) at base. Gravel fractived for 3cm, matter assis sand, graniticall quartite grains, well graded, massive, clayey ports plactic form clu-ps, moist.
-	0	0.0	3.3	1,004	1.05					- 6	to a 3 cm, matter at sale sand, graniticand autotite and so well araded, massive clayer
-	2	2 - 2	very	1,007	1.5				- 1.5 -	<b>1</b>	ports plactic form clu-ps, moist.
_	Sc-0,0 1701 X05	Run#1	Recovery 2.2 ft	1.008	5'e 11:0)				2.2-	9	
	7)	<u>~</u>							- 2.5 -	$\geq$	No Recovery 2.2-2.5th
									3D		TD=2.54.
									+.c		
								I I			
					1	-					
									5.0		
	-										
									60		
			i : :								
			; t	and the state of t					7.3		
								<u>.</u>			
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		-									
									ac		
•						Carried Control			 د.ن		

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

Lo Da Ge	reholication te: ologi	o Nur r - No st:	nber: rth: 7 /-/2 7. /	<u>134</u> 488	1930 17 Ei	98 1st: 2 ER		005	n w	SY SITE BOR Surface Eleva Area:	tion: <u>59</u> 3 <i>PAD</i> 3.6 7 <i>FRRA</i>	58 Ft Lip A:	rea ect No. G	Lof_!
		LOGO		SUPE	RVIS		000	2		DATE	_7/2	/99		
10FB0110M Of CONE HABON	TOP/BOTTOM OF	FEET OF COPE INHITIENAL	SAMPLE NIMBER	FINC HHIL ANGLE	BEDDINAS ANSE	GIVIN SIZE	115C.S	N HEIO	SOIL/ CPD POUGIL		SAMF	PLE DESCR	IPTION	
Bex lor 1 0,0-3,6	Rug # 1 0.0 - 40	RECOVERY 36	001 002 003 004 005 006	RSO RSO RSO TSO TSO DUP. RS TSO		25 00/ 00/ 00/	502)	-1.5 - -1.5 - -2.0 - -3.0 - -4.0 - -3		O.O-2.1/ dank fine gray and grading 2.1-3.6 b ory 1/6, brand A/A angular 3.6-4.0	son, ve sand in rovel, the rovel, the located havely light g	Jesond, some some some some some some some some	to mig	to .

Materials amounts are estimated by % volume instead of % weight.

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(2) Core breaks cannot be matched, accurate footage measurements not possible.

Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Eo Los Da Ge	rehok cation te:/ ologis	→ Nun Nor /3 it:	<b>iber:</b> th: <u>7</u> - 99 Z: 2	BH	951 9E ER	99 est: 2		TECHNO	0L00	GY SITE BOREHOLE LOG PAGE OF I  Surface Elevation: 5956 Ff  Area: 903 PAD Cip Acea  Total Depth: 3.7  Company: TIERRA Project No. 6 E6600 C
RN AP	ARS I	LOGO	GING M	supe ank	RVIS	OR (	2			DATE 7-2-99
TOP-BOTTOM OF CORE INBOX	TOP/BOITOM OF HATERVAL	FEET OF CORE INIMERAL (FIELD	SAMPI E NIMBER	FHACTURE ANGLE	BEDDINAL AND E	GIWIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LHFIOLOGIC	SAMPLE DESCRIPTION
Box 141 0,0-3,7	64-00 14 runs	RECOVERY: 3		R5 150 R5 T50 R5 T50	001 002 001 002 002 002 002	25 201(0 201(0 201(0	540 Sty	-1,0- -1,0- -2,0- -3,7 -4,0- -5,0- -2,0- -2,0- -2,0- -3,0- -2,0- -3,0- -2,0- -3,0- -		on 3.7 Soldy Sand 3 183/2 to 3)83/2  very dash gray to dash known, very  fine, that grand, Sifty, that e  Subansular formed, Sifty, that e  Notice Shaved up to 4 cm,  Thate clay, thace organics, ony  3.7-4.0 No Recovery

Materials amounts are estimated by % volume instead of % weight,

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Date effective: 12/31/98

Lo Da Ge	reholication cation ite: lologi	e Nur T - No /-/2 st:	nber: rth: <u>7</u> 4	1367 1867	1932 LER	- 78 ast: <u>Z</u> ER		755	OLOG	Surface Elevation Area: 203 Total Depth: Company: 203 Sample Type:	on: <u>596</u> PAD Ci 2,4 ERRA	# FF  P Arec  Project	PAGE / R	
		LOGO	GING			OR Sav	L		4-1	DATE _	7/2/90	9		
TOP/BOTTOM OF CORE INBOX	TOP/BOTTOM OF	FEET OF CORE IN INTERNAL (FIELD	SAMPLE NEW NICKES NICKE	ANALY ANALY	BLODIES	CHAIN SIGE	USCS SYMBOL	01 PTN IN	SOR/ LIDIOLOGIC		SAMPLE	DESCRIP	TION	
Bx lof 1 0.0 - 2,4	Run 4 1 00-40	RECOVERY: 2.	601 002 003	RS ISO RS ISO RS ISO	901 902 901 902 902	RS		-1.5 - -1.0 - -1.5 - -2.0 - -3.0 - -4.0 - -5.6 - -7.0 - -8.0 - -9.0 -		0.0-0.6 Very dank and up to 10015, m. 0.6-2-4 from, very 10 angula Silty, mo 2.0-4.0 TAL 1-12-9	Gravely YR 4/3 Lo Fine plo Jesa tely, No Rocar	profit to	un to Syba 25 4	dark Josephore

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Revision 0

Date effective: 12/31/98

Lo Da Ge	reholication te: ologi	e Nun r - Nor <u>/-/2</u> st:	th: <u>74</u> -99 7-2	ENVII BH 1869 UTH	733 8 Ea	\$ 78 st: <u>20</u> ER		<u> </u>	 	Y SITE BOREHOLE LOG Surface Elevation: 5956 Ff Area: 903 PAP Lip A Total Depth: 3.8 Company: 17 FRRA = 20 Sample Type: CONTINUOU	reg lect No. G E6600 00
		LOGO		SUPE Man	RVIS	OR Son	ر کی			DATE _ 7-2-99	
10P-BOTTOM OF CORE HIBOX	TOP/BOITOM OF DIVISERVAL	FEET OF CORE INIMILERVAL (FIELD	SAMPLE	FINCTUME	BEDINAL ANDE	GIWINSIZE DISTRIBUTION	11SCS SYMBOI	N 1311	SOIL/ LITEOLOGIC LOXI	SAMPLE DESC	RIPTION
Box 105/ 26/ 3,8- 7.8	hm # 1 00-40	(PCOVIN) 3.8	001 002 003 004	RS ISO RS ISO RS ISO	7 00 002	P 1-00 2-00	CL 5602 11210 (002) (002)	1.5 -1.0 -1.5 -2.0 -2.7 -3.0 -4.0		ap-29 Silty Clay 2 dark brown with organ to fine Sand, trais up lithic gravel mon to the maist  20-27 Silty Clay 5 yellowish brown, Ala tid plasticity mais	TR 4/6 Happy  moderate to  TAR 5/2 No.

Materials amounts are estimated by % volume instead of % weight.

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Revision 0

Date effective: 12/31/98

Bo Lo Da	rehol catior te:	e Num r - Non	iber: <u>7</u> 4	137. 1 <b>87</b> -99	193 22 Ea	498 ist: 2	3		OLOG	Surface Elevation Area: 90.3	EHOLE LOG tion: 5942 3 PAP Lip 3 2		LOF_[
		Equip.:	GE SING	SUPE	RYIS	€ OR	<del>DU4</del>	L WAD	1/2/90	Sample Type:	CONTINU	rous	
AF	PRC	VAL		Ma	<u>nk</u>	<u>. W</u>	wd			DATE	7-2-9	9	
TOP-BOTTOM OF CORE IN BOX	TOP/BOTTOM OF	FEET OF COPE IN INTERNAL (FIELD	SAMPLE X NIMBER	FILAC TUPIL APAGLE	the country	GOWIN SIZE DISTRIBUTION	USCS	DIPDAM HES	SOIL/ LIFTIOLOGIC		SAMPLE D	ESCRIPTION	
Box lor / 0.0-32	Run # 1 20-40	Recovery S.2"	001 002 003 004	R5 T50 R5 T50 R5 T50 R5 T50	64) 20/ 20/ 20/ 20/ 20/ 20/ 20/ 20/	R5 001	CL SM	-1,0- -2.0- -3.0- -4.0- -5.0-		to made moist 1.0-3.2 prod, very Subança Trace god	pinkish s  aces sand,  navefugi i  sily Sano  figur to fi  an, Silit	may to ve theres be a 3.5 cm hairs from som those	nolong onganics g/A, scoonso

Materials amounts are estimated by % volume instead of % weight,

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Bo Lo Da Ge	rehole cation ite:	Num - Non - 3/	ber: h: 7 23/ 32/	B189.	1935 27 Ear	98 st: 2	085	978	•	Surface Elevation: 5973 ft  Area: 903 PAD/LIP Area  Total Depth: 2,5 ft.  Company: Terra Project No.: 65600000  Sample Type: Commons core
ı	3&G (		SING		EAVI Can K			d		DATE 8/25/98
TOP/MOTTOM OF CONG HIBOX	<del>,</del>	FEET OF CORE IN HOTERVAL (FIELD ALASI WEMEN)	SAMPLE PATMBER	FILM, TUTTE ATKILE	BEDDING ARGI E	GIWINSIZE DISTRIBUTION	USCS	DEPTH IN	\$0it./ 110 kaj 0kir. 106	T
Box lof 10.0-2.5A	Run #1 0.0-2.5tt.	revy 1.4ft.	1.006	04 10:32	7/2019			0.5 - 0.4 - 1.5 - 1.5 - 2.5		brown (104x 3/3), fixesand, sufficiently dark brown (104x 3/3), fixesand, sufficiently 0.4-1.4 Clay, Said, Gravel, dark reddish brown (2.5 YR 3/4) fractured granific IRF up to 3 cm inclay said matrix, angular mediun sand, massive, minor root heir, moist, firm.  1.4-2.5 No Recovery
			010	12.41	Rin 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			- 3.0		7.0.=2.54.

- (1) Badly proken core, accurate lootage measurements not possible
- (2) Core breaks cannot be matched, accurate footage measurements not possible

								ВО	REH	OLE	LOG PAGEOF Surface Elevation: 5972 Ft
	Loc	ation -		er: 14	998 898	9360 8 Eas	10 st: 2	086	153	,	Area: 903 PAD/LIP Area
	Geo	e: <u>3</u> ologist	: R.	Ko	EHL	R				(	Total Depth: 2.5 ft.  Company: TIERRA Project No.: GE 600000
-			quip.:								Sample Type: CONTINUOUS CORE
		eg L PRO	.OGG VAL .			Jose					DATE 4/14/48
	20 35 X	ITOM	COPE NVAI. ID MENT,	I E EA	une it	F. F.	SIZE	S: Bor	DEPTH IN	U OGIC G	
	OF CORE	FOP:BOTTOM OF HHIERVAL	FEET OF COPE IN IFFETIVAL (FIET) MEASUPEMENT)	SAMPLE NEMBER	FILACTURE ALKRE	BEDDING	GHAILLSIZE DISTAIBUTION	USUS	1990	SOIL/ LID KN OGIC LOG	SAMPLE DESCRIPTION
	0.0-2.54			1.005 1.005	R			6c	-0.5	- 6	(0.0-0.8 ft; Clay, Sand, Gravel; dark brown (n. SYR3A), quartists grand up to 3cm, fractured, fine sand, clumpy, plastic, grass shoots and roother, Wisist.
	0.0	4	ft.	1.010	R-Du				0.8		10.8-2.1 ft. Clay, Sandwith some gravel (14 162.14)
	Boxlof1 C	0.0-2.5ft		1.00L 1.00L	R RS				- 1.5		O.8-2.1 ft; Elay, Sand with some gravel (1462.1ft) veddish yellow (5 yr 7/6) fine sand crumbly to unconsolidated, gravel is fractured, quarterto, moist
	, xo	#	Recovery	1'008	g.0				2.o_	1	<u> </u>
-	2	Ran	~ —						2.5	$\perp$	2.1-2.5 ft. N. Recovery
				1.009	Rs	Rus	40m1 VOA VIA-		<u> </u>		T.D. = 2.5++.
				i.012	R	Ris	1501.				
							poly.				
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		1								1	
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				-					1		

- (1) Bacty proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

	Boo Loc Dai Ge Dril	rehole ation e: ologis ling E	Num - Non 3/12 t: quip.:	ber: h: 7 2/98 3-96	8th 4897 2006	937° 6Ea: R. Ka	98 st: 2 SEH(	086	300		LOG  Surface Elevation: 5970 ft  Area: 903 Cip Area  Fotal Depth: 2.5ft  Company: Tierra Project No.:GEG00000  Sample Type: Combinious core Macracon
		i&G ( PRO		SING	SUPE	:JVR: <u>~ ~</u>	50R	2			DATE 8/25/98
TOP/MOFTOM	OF COINE	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD MEAS! REMENT	SAMPLE	FHACTURE ANGLE	BEDDING	GFMIN SI在 DISTAIBLITION	USC\$ SYMBOL	DEPTH IN	\$01.7 (11) (3) 0GIC	SAMPLE DESCRIPTION
-	195.6-0.0   Jox lot   0.0-3.5ft	Rur #1 0.0-2.54. 10	y 1.8ft.	100.1 100.2 100.1 100.1 100.1	Rs Ro.45 Rs Ro.9 Rs		B SIG	GC	0.0 0.1 1.5 - 1.8 - 1.8 - 2.5 - 3.0 - 4.c - - - - - - - - - - - - - -		0.0-0.4 Clay Sand, Gravel, dark brown (7.5483/, gray fractured gravel up to 3 cm, quarteits mayber  Sand Gravel, Yellow Sand Gravel, yellow or Clothy plastic, with a  More of Jest (10 y 8 1/6), gravel concentrated at top (0.4-0.6 ft)  I pick e founded quarteits rest is fractured quarteit gravel to 3 cm, possibly caliche? possible clay  Ro Recovery 1.8-254  T. D. = 2.5 ft.
)									0.0		

16/

NOTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

ROCKY FLATS ENVIR  Borehole Number: BH  Location - North: 74900  Date: 2 17-99  Geologist: T. LUTH  Drilling Equip: 6FOPK	3 East: 2086406 ERER	SY SITE BOREHOLE LOG PAGE OF I Surface Elevation: 5968 FF Area: 703 PAD Lip Area Total Depth: 3.9 Company: TERRA Project No. GEGGO Sample Type: CONTINUOUS
RMRS LOGGING SUPER	RVISOR ank R. Word	DATE 7-2-99
10P-BO110M OF CORE IN BOX TOPBO110M OF INTERNAL FEET OF COPE INTER	GIANNAICE  GIANNAICE  USCS SYMBOI  HIFTH IN  HETTER	No Nois SAMPLE DESCRIPTION  FOR CL SYMBOL
001 RS 002 TSO 003 TSO 003 TSO 05	201 002 001 002 001 002 001 002 001 002 001 002 001 002 001 002 001 002 001 002 001 002 001 002	Rodgish Brown 37R 3/4, stiftly Rodgish Brown 37R 3/4, stiftly ylustic, some pred fine togogs found, ansular to subrounded, I have appealed to subrounded in 3 cm little gravel. Hoist 10-3.7 Cloyer Sound who and components some as a bove. Jan 37-3.9 Gravelly Sound Courant Components Saw 25 above day.  3.9-4.0 No Rocovery
99,44852 001	25 PS 001 (002) 001 (002) 003 (002) 004 (002) 005	

Materials amounts are estimated by % volume instead of % weight.

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(2) Core breaks cannot be matched, accurate footage measurements not possible.

Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Bo Lo Di Go	OCH prehole pcation ate: eologis illing E	Num - Non 3	ber: h: 74 6 [7/ 3-4	BH 912= 98_R	1939 3 Eas PK 31	9 <u>8</u> st: 🚄	2080	REHO		LOG  Surface Elevation: 5973 ft  Area: 903 cip Area  Total Depth: 3.5 ft  Company: Tierra Project No.: GE 600000  Sample Type: Continuous core Macio Con
1	G&G I		SING		ERVIS onk	1	و			DATE 8/25/98
10P/BOTTOM OF COME	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL FIELD	SAMPLE NUMBER	FHACTUME ANGLE	BEDDING ANGLE	GRAIN SIZE DISTRIBUTION	USCS	DEPTICIN FEET	SOIL/ LITHOLOGIC LOG	SAMPLE DESCRIPTION
Bux 10+1 00-2,54	Run #10,0-3,54	14 2.2 ft.	100,1 200,1 100,1 100,1 200,1	R1 R RS R RS	13:02 13:02		SC SC	0.0 0.4 		6.0-0.7+1, Clay Sand Gravel; dauk Drown (10) R 4/3  +0/3); rounded spherical gravelup to 3 cm, granitic IR  0.4-1.7+1; Clay, Sand Gravel; yellow is 1 veol (5) R 4/6 to dark yellow is 1 veol (5) R 4/6 to dark gravel (2 martic IRF) in clay sand partic for sand gravel to 3 cm, well graded, Clulary over 10 tty, mart trace voots at top  1.7-2.2+1; Clay Sand; yellow boun (10) R 5/4) to very palebrown (p) R 8/2, true sand 2.3-d. Stt No Recovery. Calche, clumpy, poorgand, hoist  T. D. = 2.5+1.

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

	Bo Loc Da Ge	reholecation te: tologi:	KY e Num o - Noc O3/ st: _s quip.:	nber: th: <u>7</u> 03/	BH 18 18	940 Z Ea R. KC	98	2081	REHC	•	Surface Elevation: 5971 Ft  Area: 903 Cir Area  Total Depth: 9.0 Ft.  Company: Tierra Project No.: GE-Good OF (MACKOCORE)
1			LOG			ERVI	`	Λ			DATE 8/25/98
1,5	of cure.	1_	FEET OF CORE INIMERVAL (FIELD		FRACTURE	BEDORAG ANGLE	GHAIN SIZE DISTRIBUTION	USCS	OÉPIH IN FEET	\$017 1 HHOLOGIC 1 OS	SAMPLE DESCRIPTION
	0,0-0,047	Run #1	svery stry	11,000	1.2 1.5H	7/20/9°	)	GM GC	0.5		0.0-0.5; Sitt Sond, Gravel: dark relland brown (10) 4/2), fine to nedmine said well graded, unconsolidated dry Abundant Root their  0.5- J. Oft; modurate reddish brown (10 R 4/6)  Clay, sitt said, gravel; gravel and said gravitic in parts slightly plastic - forms saysages in corebarrel moist, root hairs common not stratified, from No Recovery 1.6-2.0ft   gravel lense at top. hildby coarse gravel.
				1.008	1.Sft = Rad				- 3.0		filledby course grands.

- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

	Bo Lo Da Ge	rehole cation te: ologis	- Num - Non 3/1	iber: th: 7 6/98	BH 4912	9419 3 Ea	8 st: <b>∠</b> 2	086	REHC 298		Surface Elevation: Area: 903 C	Sft Proj	ect No.:GE 60000
+		lling E				ERVI	SQR						THEOLOGIC
L		PRO				enle	- W	ı.			DATE	8/25/98	
TOPOSOFICIA	OF COLE	TOP/BOTTOM OF INTEHVAL	FEET OF CORE ININGERVAL (FIELD	SAMPLE	FFWCTURE ANGLE	BEDDING ANGLE	GRAIN SIÆ DISTRIBUTION	USCS	DEPTH IN	\$011/ 111/010GIC		SAMPLE DESC	RIPTION
	0.0-2.5ft	-2.54	1.64	1.00) 1.007 1.004	R Rs R			60	0.5 _		less gravel than ab	rto 2 cm, rod uc mediun grns rul at base, clu d Gravell ros ove pink 17	her mounts and
	Box 10f)	Run #1 0.0	Recovery	1.006	Rs				- 1.5 - 1.6 - 2e-		No Recovery 1.6-2.5ft.	, friable fin	Les clay clasts?  of "chunks" poorly  some root lains
					Rs-R R-Ri		Homl Igall.		30		T.D. = 2.5 A	· ·	
			-						t.c				
									5.0				
									- 60				
							٠		7.0				
					·								
				-					-				
			A STATE OF THE STA					· · · · · · · · · · · · · · · · · · ·	9.0-				

- (1) Badly proken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible

Borehole Number: 8/7 Location - North: 7491/ Date: 2-18-99 Geologist: 7. Luth Orilling Equip.: 6F0PA	2_East: 2086438	SY SITE BOREHOLE LOG  Surface Elevation: 5968 Ft  Area: 703 PAP Lip Acea  Total Depth: 3,85  Company: TIERRA Project No. 6E6600  Sample Type: CONTINUOUS
RMRS LOGGING SUPE	ervisor and wood	DATE 7-2-99
OF COPE IN BOX IN TERVAL FEED OF IN INTERVAL FEED OF IN INTERVAL IN  SOIL HILLS BOILD HILLS SOIL SOIL HILLS SOIL	SAMPLE DESCRIPTION	
905 700	001 -2.0-11111	Brown, 24R 2/5 Soldy judgesson Sandy some mediany to find, have subangular to fight, have abandont up to 3 cm brown angular lattic gravel, trage elay, trace organics, maist.  0.7-3.7 Clayey Sand, color, and components some as glove damp. Trace stave 1 A.A.  3.85-4.0 No Recovery
9924849 00 00 00 00 00 00 00 00 00 00 00 00 00	5.0_ 5.0_ 5.0_ 5.0_ 5.0_ 5.0_ 5.0_ 7.0_	3.7-3.85 Gravely Fand, Color and Component's Same as a bord ory

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Revision 0

Date effective: 12/31/98

Property of the second	Bor Loc Dat Geo	ehole ation e:	Numi	oer: n: <u>14</u> 2//98	BH912 1912 EHL	74399 9 Eas	₹ st: <i>Q(</i>	085	REHO	:	Surface Elevation: 5978 ft.  Area: 903 PAD/LIP Acea.  Total Depth: 3.0ff.  Company: TIERRA Project No.: GELOWOO Sample Type: CONTINUOUS CORE
			LOGO VAL		_	ERVIS		w	) wd	,	DATE 8/25/98
-	OF COME	TOPBOTTOM OF HUERVA	FEET OF COINE IN INTERVAL FIELD MEASUNGMENT)	SAMPLE NUMBER	TIMOTHRE	BEDDING	GHANITSIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LITH KILOGIC LDIS	
	Bux 1 of 1,0,0-3,0ft.	Run #1 0.0-3,0ft.	Recovery 1,4ft, ME	200 200 200 200 200 200 200 200 200 200	110 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			6M 6C	- 0.3 0.5		gravel to 2cm, round and gravely gravish brownfloy R5/2)  gravel to 2cm, round occasionally fractived, grantice and quarte it  0.3-1.4; Soil; Truck fragments medium to finesand,  clay, sand, gravel; unconsolidated, dry, root have.  very dark brown (10 y R2/2), gravel to 3.5 cm, angular-  fractived, granitic in part, medium soullford, poorly gradel,
	NOT	ss c	enera:	USCS	is mor	dified to	or this !	od as	ollows:		

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Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate lootage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Bor Loc Dat Ger	enole ation - e:	Numi North	er: 1: <i>74</i> 8/98 <b>K6</b>	BH9	4493 Eas	} st: <i>20</i>	985.	REHO	; ; ;	LOG  Surface Elevation: 5970 ft  Area: 903 PAD / LIP Area  Total Depth: 3.0 ft.  Company: TIERRA Project No.: GE 600000  Sample Type: CONTINUOUS CORE
	&G L PRO			SUP			love	l .		DATE 8/25/98
TOPROTTOM OF COPE ITBOX	TOPBOTTOM OF HITERVAL	FEET OF CORE INITATENAL (FIELD JEASUITEMENT)	SAMPLE RUMBER	FINCHINE	BEDDING ANGLE	CATAIN SLZE	USCS	DEPTH RI	SORJ UPPOLOGIE. UGG	
0.0-3.04	3.0 ft	) H&	002	12:08 0.8 0.8 12:06				-0.5 - 0.8 -1.•		o: 0-0.3 fills clay sand, g more! dark brownts. Sye 3/2), ground yet a 2cm; rometic and front the distribution, subscirillating and medium sand, unconscillating, martin and the sold plant fings of 3-1.2 ft, soil; clay, sand, gravel; dark brown (7.5/R 3/2), gravel capto 3 cm, angular - fractured, quartite common firm caliche (?) in lower half, sightly moist
	0,0		006	1.3 12:04				1.8		1.2-1.8 ft., So; 1; Clay-Sand, trace gravel, yellow to yellowish Drown (10 YR 8/6 to 10 YR 6/6), finatomedium sand, soft Unconsolidated, slightly mist, 1 cm dia block schooling
Box lofl	Run #1	Recovery						-2.s -	X	No Recovery 1.8-3.0ft.
								- 3.s -		
	-							-4,3-		T.D. = 3.0+1.
				Total Control of the		not all a trep a la des des des des des des des des des des		- 4.5 -	de la contraction de la contra	
						de companyant ou est de compan		-s.s -		
				And the same of th				(o		
								- 6.5 -		
						Parket of the state of the stat		7.5 -		
								7.0		
						and the same management of the same same same same same same same sam		- 8.5 -		
								<u> - م</u>		
								- q.5 -		

- (1) Badiy proken core, accurate footage measurements not possible.
- (2) Core preaks cannot be matched, accurate footage measurements not possible.

Materials amounts are estimated by % volume instead of % weight.

(1) Badiy broken core, accurate footage measurements not possible

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Bo Loc Da Ge Dri	rehole cation te: <u>Dr</u> ologis	Num - Nort - Nor	ber. <b>1</b> h: <u>1</u> : 9.11 R. K Ger	194 1920 0.98 Suppopol	59Ea Samp	st: 20 oled:	9.17.	<u> </u>		Surface Elevation: <u>5976 ft</u> Area: <u>903 Lip Area.</u> Total Depth: <u>3.0 feet</u> Company: <u>STOLLER</u> Project No.: <u>GE 600000</u> Sample Type: <u>Continuous Core</u>
	PRO	VAL		Man	ERVI	SOF	4			DATE 9/30/98
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF COPE ININTERVAL (FIELD MEASUREMENT	SAMPLE NUMBER	FRACTURE ANGLE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTH IN FEET	SOIU LITHOLOGIC LOG	SAMPLE DESCRIPTION
of   0.0-3.0ft.	10.0-3.0ff.	45 to 64	1.001 1.005 1.006 1.003 1.007 1.004 1.008	1029 6.5 1033 10 1022 15 1036	RS R RS R RS R		GM GP	0.5 - 1.0	000	yellowish brown (2.5 y 6/4) 80% medium to coarse sand, arovel mious a sinch subrounded to rounded, dry 1.0-1.5 Gravel, 90% gravel, 10% sand/Rock fragments, poorly graded ye to 1 inch, pinkish gray (5yr 7/2), subrounded to angular, broken, dry 1.5-2.4 Gravel-Clov-Sand, Dredomuk & gravel-to
Box	Run #	Recovery	1.009	20	Dup		GC	2.0 2.5 <sup>24</sup>	0/9	and bottom, clay-sand center, needd, sh brown (5 y & 5/3) gravel subangular moderately gradek, mainly sand and clay 2.0-2.3 ft., damp 2.4-3.0 No Recovery
	- 4		2.601 2.602	Rs R		40ml 41	1043			T.D. = 3, 0 ft.
NOTE	S Ge	neral;	uscs	is mod	ified for	r this lo	og as fo	ollows.		

ROCKY: FL Borehole Number Location - North: ' Date: Drilled: 9. Geologist: R. F.	: <u>B</u> H 9460 149265 E 16:98 San Rupd	18 ast: 208 pled: 9	358	52	7	Surface Elevation: 5975 ft  Area: 903 Lip  Total Depth: 2.0 ft.  Company: STOLLER Project No.: GE 100000
Drilling Equip.:(	<del></del>					Sample Type: continuous Core
EG&G LOGGIN			d			DATE 9-30-98
TOP/BOTTOM OF COPE IN BOX TOP/BOTTOM OF INTERVAL FEET OF COPE IN INTERVAL IN INTERVAL IN INTERVAL MEASUREMENTER	PAACTURE ANGLE BEDDING	GRAIN SIZE DISTRIBUTION	SYMBOL	DEPTH IN FEET	LITHOLOGIC LOG	SAMPLE DESCRIPTION
0x 10f1 .0-2.0ff. un 10f1 0-2.0ff. covery 1.8ff.	001 1408 R 005 0.45 R 006 0.4 R 007 1409 R 007 140 R 007 1.35 R 008 1.80 R		âС	-0.5 -0.5 -1.0 -0.5	00000	0.0-1.8 Clayey Sondy Gravel, 30% clay 50% Sand 20% gravel, Reddish gray (5yx5/z) 80% of sand is medium to coarse grain, gravel is subrounded to engular and broken with fragments cess than 0.1ft diameter, well graded Loose, day. 0.2 ft. of caliche @ 1.5ft.
K				-2.0	$\leq$	1.8-2.0 No Recovery
						T.D. = 2.0 ft. REfusal

- (1) Badiy broken core, accurate footage measurements not possible
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

Bo Lo Da Ga	OCK prehole pcation ate: eologis tilling E	Num	iber: th: <u>74</u> 3-	1926 17-9 UTH	494 <u>ele</u> Ea 9 1 <i>ER</i>	7 98 st: <u>Ze</u> ER	3		wig.	Y SITE BOREHOLE LO Surface Elevation: 597 Area: 903 PAPL Total Depth: 1,0 Company: TIERRA Sample Type: CONTIN	2 Ft D Area Project No	GEOF	
1	MRS I			_	RVIS	•	~~ e	2		DATE			
TOP-BOTTOM OF CORE	TOP/BOI TOM OF	FEET OF COPE INIMITERVAL FIELD	SAMPLE N NIMBER	FIWCHINE ANGLE	14 BEDDING	GIMIN SIZE DISTRIBUTION	USCS SYMBOL	NE PETER IN	SOIL/ FIFFOLDGIC LOSS	SAMPLE	DESCRIPTION	)N	
1201/05/	160 / Hun # 1 0:0 - 4:0'		001 002 004	RS 150 RS 150 RS 150 PS 1001	25 001 002 001 002 001 002	2I (002) (002)		-1.0- -2.0- -3.0- -4.0- -5.0- -7.0- -8.0-		O.O-\$1.0 Sandy STA chay gray, 3YR No Inace up to 3.5 cm with conganics, damp. 1.0-4.0 Clayer San Type 7/8 fine to fine, some sulan sular to ans clay blos locally 6 cm A/A, silty	medium lage fin dage fin do by R medium alan, 5%	g pless other for our to con- tral sel	ticilo navel nse so

Materials amounts are estimated by % volume instead of % weight.

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(2) Core breaks cannot be matched, accurate footage measurements not possible.

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Date effective: 12/31/98

Loc Dat Ge Dri	rehole cation te: <u>dic</u> ologist lling Ed	Numb North Illed: R. Juip.:	er: 1 1: 740 9·2 Ruy Geo	# 92 24- 3-98 P Prob	Eas Samp	8 st: 20 sled:	8601	49	<u>.</u>	Surface Elevation: 5970 Ft  Area: 903 Lip  Total Depth: 2.6 ft.  Company: STOLLER Project:No.: GE600000  Sample Type: continuous Core
	PRO			SUPI	, ,		1			DATE _9-30-98
TOP/BOTTOM OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD MEASUREMENT)	SAMPLE NUMBER	FRACTURE	BEDDINÁ ANGLE	GRAIN BIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN	SOIL	SAMPLE DESCRIPTION
, <del>1</del> 4,	, <del>1</del> 7.	Z.0 ft.	1.601 1.605 1.602 1.006	1472 0.5 1414	RS RS RS R		GM	- 0.5 -		0.0-1.0 Sitt, study, gravely 60% sitt, 20% sindi 20 mgravel, light gravy Eyr 6/1) medium to very coarse sond, subrounded gravel, broken quarteite, Poorly graded, loose, drey, with abundant roots to 0.2 ft.
Box 1 of 0.0 - 2.6	RUN #12 0.0 - 2.6	RECOVERY	1.003 1.007 1.604 1.008	1410 15 1406 20	RS R Rs R		GC	- 1,5 - - 2,0-	0/0	1.0-2.0 Gravel, Chyry, Silty, 50% gravel, 25% and, 25% clay; reddish gray (5 yr 5/2) to Reddish Grown (5 yr 4/3) poorly graded coarses and and gravel; broken vock up to 0.15 ft. diameter; 0.3 ft clayer section at 1.7-2.0 ft. minor to no gravel, loose, dry, clay section damp.
600	160	Rec					:	- 2.5 <u>-</u>	X	2.0-2.6 No Recovery
										T.D.=2,6 ft.
		•								
							-			
										t and the second of the second
						****				
		-		is mo						

Materials amounts are estimated by % volume instead of % weight.
(1) Badiy broken core, accurate footage measurements not possible.

	Bor Loc Dat Geo Dril	ehole ation e: <u>dri</u> ologist ling E	Numi Norti Iled: : _ P quip.:	er. 1 1: 74 9.23 Ru Ger	3H 9 924 98 SI PP prob	490 HEas ample	18 d: 9	084 <b>28</b>	,298	<b>Q</b>	-4	Surface Elevation: 5968 FF  Surface Elevation: 5968 FF  Area: 903 Li?  Total Depth: 2.0 FF.  Company: STOLLER Project:No.: 6F-600000  Sample Type: CONTINUOUS CORE
		&G.L PRO			Ma				1	-4		DATE <u>9-30-98</u>
	OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF COPE IN INTERVAL (FIELD MEASUREMENT)		FRACTURE	BEDDING	GRAIN SIZE DISTAIBUTION	USCS SYMBOL	DEPTH IN FEET		POG LITHOLOGIC SOIL	SAMPLE DESCRIPTION
	10t1 -2.0ft	v #2 2.0 ft.	15 1.7 th.	1.001 1.005 1.002 1.004 1.004	1022 0.4 1021 0.8 1023 1.2	RE BE RE		GM GP	- 0.5 1.0	5.9	00.00	Light brownish gray(104R 6/2) Low plasticity, sand coarse,
ķ	0.0	5 6 K	Recovery	1.008	1024	Rs R	. T.	GC	1.5		/s/ /6	Reddish brown (5 ye 4/3) boarse sand, angular gravel, 1005e, day
ŀ		0	B				*		2.0.	_	$\geq$	1.7-2.0 No Recovery
												T.D.= 2.0ft. Refusal
										_		

Materials amounts are estimated by % volume instead of % weight.

(1) Badiy broken core, accurate footage measurements not possible.

Boreh Locati Date:	pie Num pn - Noi pist:	nber. th: 7 2~	1971 1992 1976	95 43Ea 9 1ER	09 { st: <u>Z</u> FR	}			SY SITE BOREHOLE LOG PAGEOF /_ Surface Elevation: 59&7 F + Area: 903 PAP Lip Acea Total Depth: 3, 4' Company: 11 FRRA = rolect No. GE6600 Oct Sample Type: CONTINUOUS
RMR:	LOGO					Q			DATE 7-2-99
OF CORE INBOX TOPBOTTOM	FEET OF COPE IN INDERVAL (FIELD	S SAMPLE TO NIMBER	FELACTIFIE ANGLE	S BEDDINA	GIVAIN SIZE DISTRIBUTION	USCS	DIPTH IN	50k/ 1215-03 0Git. 1083	SAMPLE DESCRIPTION
0	7 . 7	002	RS 150	001 002 001 002 001 002		SC CL	1,5 -1,0 1,5 2.0 2.2 -3.4 -4.0		Journ 3 TR 3/4 Very fine to fine sound, locally to course, Suffergular to substant sound, locally sites, share to fine sound, locally sites, shared up to 30 to 100
99	448		001 002 003 004	25 001 061 001 001	904 002) 102)		3.0 -5.0 -7.0 -3.0		Sample Same as Q 0.0-0.5 Trace clay, dry

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

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Revision 0

Date effective: 12/31/98

	Bo Lo Da Ge	rehole cation te: <b>dr</b> cologis	Num Nortifed: t: R	ber: h: <i>740</i> <b>9·11</b> Ru	311 9 188 98	519 Ea 50mp	<u>8</u> st: 2€	1861	49	ا ا	Surface Elevation: 5970 ft  Area: 903 LiP  Total Depth: 2.7 ft.  Company: STOLLER Project:No.: 6-600000000000000000000000000000000000
			LOG( VAL		SUP				ay in a count,	<u>-</u>	DATE 9-30-98
	OF CORE	TOP/BOTTOM OF INTERVAL	FEET OF CORE ININTERVAL (FIELD MEASI REMENT	SAMPLE NUMBER	FRACTURE	BEDDINA	GRAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN	SOIL/ LITHOLOGIC	
, 0	0+/+ -2.7+	42	14.5 Kg	J.001 J.005 J.002 J.006 J.003 J.007	1435 1435	RS RS RS RS RS		GM GM	- 0.5 - 1.0	10/0	0.0 - 0.5 S. Ity GRAIEL, brown (7.5 ye 5/3): TO GRAY (7.5 ye 5/0) 60% siff 10% sond 30% gravel, coarse sand, subrounded gravel, well graded, day, 70075 0.5 - 1.0 Sitty Gravel, 70% gravel 30% sift, brown (7.5 ye 5/3) sybrounded to angular gravel, 0.1 ft. broken Rock fragrents, fines are mainly broken Rock, poorly gradel, day
20	0.0	8417 0.0	Recovery	1.008		Rs R			2.5 2.4 2.5 2.7	0/0	1.0-2.4 Clay, sandy, gravely; 40% clay, 30% sard, 30% gravel, dark brown (7.5 yr 4/3) Low Plasticity, sand grains medium to coarse, Loose, dry; gravel fractured and angular 2.4-2.7 NO Recovery
											T.D.= 2.7 ft.

Materials amounts are estimated by % volume instead of % weight.

(1) Badiy broken core, accurate footage measurements not possible.

	Log Da Ge Dri	renole cation te: Di ologis	Num - Non -	h: 74 h: 74 Ru Geo	241 9 9/2= 3.98 PP PProb	52° Eary Sarry EBMI	18 st: Z pled: 9	086 <b>1·28</b>	2066		Surface Elevation: 5972 ff Area: 903 Lip Total Depth: 2.95 ft. Company: STOLLER Project:No.: GE GOLDON Sample Type: Continuous Corc  DATE 9/30/98
100000	OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF COPE ININTERVAL (FIELD MEASUREMENT)	SAMPLE NUMBER	FRACTURE ANGLE	BEDDING ANGLE	GPAIN 812E DISTAIBUTION	USCS	DEPTH IN FEET	SOIL/ LITHOLOGIC	The second secon
	44	<i>t</i> +.	#	1.005 1.005 1.006	1109	PS PL PS PL		GM	09	000	0.0-0.9 5, ity sandy Gravel; 40% sand, 40% silt, 20% grave darkgray (10ye 4/1) medium to coarse sand; gravel is minus 1/2 inch, Rounded, pebbly, Loose, deg, abundant Roots to 0.5 ft.
	10+1	47	7 2.6	1.003	1325 15 1327	Rs R Rs R		GP GC	-1·5 -	000	0.9-15 Gravel, SANDY; 90% gravel, 10% sand; light gray (10 yr 7/1); sand pebby; gravel minus 1 inch, argular, broken, poorly graded, loose; dray 1.5-22 Gravel, clayey, sandy; 70% gravel 20% clay 10% sand, Reddish brown (5 yr 4/3) medium to coarse sand, angular gravel, broken, well graded, compact, damp
	0 0 0 0 0 0	0.50	Recovery	1009	20 '	Duf		GC	-2.5 -2.5=	10/9	gravel, broken, well graced, compact, damp  2.2-2.6 Caliche, sandy, grayely; 50% fines 20% gravel  Publics, pinkish white (5) R 8/2) To white (5) R 8/1); Rounded  Publics, friable, compact, dry  2.6-2.95 No Recovery
				2.00/ 2.002	R Rs	RNS RHS	4L 40ml	1335 1337	295	<b>×</b>	T.D = 2.95 ft.
							in A	y và		-	
							·				
										-	
										1 <b>1</b> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

- (1) Badiy broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible

Bo Lo Da Ga	reholication te: ologi	Y FL.  Non  Non  Non  The Non	iber. <sup>7</sup> th: <u>7</u> ≿-99	953 4912 UTH	98 0 Ea	st: <u>2</u> ER			m(s)	Surface Elevation: 5970 F+ Area: 903 PAP Lip Area Total Depth: 40 TAL 38 Company: TIERRA TOTAL 38 Sample Type: CONTINUOUS
		LOGO				OR.	vel			DATE 7-2-99
TOP/BOTTOM OF CORE	10P/BO110M OF	FEET OF COPE IN INTERVAL (FIELD	SAMPLE NIMBER	FINCTUME	TANGE SOTT	GIWIN SIZE DISTRIBUTION	USCS SYMBOL	DI PTR IN	SOIL/ LIPENGGIL	SAMPLE DESCRIPTION
1 10x 10x 10x 10x 10x 10x 10x 10x 10x 10	Run X 1 0.0-38'	RELOVERY: 3.2	001 002 003 004	RS TSO RS TSO RS TSU RS TSU RS	7 00 002 001 002 002 002 004	es 1 001 3 001 3 - 26	(002) (002) (002)			100-10 Silty Sand very dark grassed hown 3/8 3/2 prod very fine to fing some my dark grassed, some my to coarse, Subansula, Salty, Some apto 6 cm, Subansula, dry 10-32 (layer sand/sendy (lay apolited light hownish gray to reddish brown 4/8 4/3 + 6/8 pred. very fine to fing some med + coarse, subansula, low plastic clay, there to some up to 4 cm gravel ony 3,2-3,8 No RECOVERY

Materials amounts are estimated by % volume instead of % weight.

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	Bor	ehole	Numl	per:	KH 4	549	18		REH <b>O</b> 018 18		LOG Surface Elevation: 5973 ff  Area: 903 Lip  Total Depth: 2.35 ff
	Ge	ologist	:	R.A	upp apm	<u> </u>					Company: STOLLER Project:No.:GE 600000 Sample Type: Continuous Core
		&G.L PRO'		AING	SUPI	ERVI		/ /	1		DATE 9/30/98
	TOP/BOTTOM OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE ININTERVAL (FIELD MEASUREMENT)	8 AMPLE NUMBER	FRACTURE	BEDDINÁ ANGLE	GPAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN FEET	BOIL LITHOLOGIC	SAMPLE DESCRIPTION
	+7+	-44.	75 H.	1.005 1.005 1.002 1.006	1429 085 1431	かんなん	,	GM	0.5	14 6 7 8	0.0-0.8 gRAVEL, SILTY, SOWDY; 50% gravel 40% silt 10% saind dark gravis histain (10 yr 4/2) sand medium to coarse; gravel subangular, poorly graded, Loose, dry, very heavy roots
	1 of 1 - 2.35	1 #1	17	1.003	0.9 1425 1.35	RS R	25	GP CC	10 7.1	00.0	long with the state of the same and anti-counted as the at the
K	0,0	Pu,	Recovery	1.008	1427 1:75	RS R		GC	-1.5 - -2.0-	/o/·	Grading to light gray (10 yr 7/1) pebbycalithe, boose dry
									2.35	<u> </u>	T.D. = 2.35 ft.
			-	·	•						and ref <sub>acts</sub>
									: -	.3	
						٠	-				
			•								
				-							
										n erve	

- (1) Badiy broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible

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Lo Da Ge	rehole cation te: ologis	e Num	ber: th: <u>74</u> 3 - 2	13H 1898 4-9 UTH	933 4Ea	598 ist: <b>2</b> 6		ZZ9	mw	SYSITE BOREHOLE LOG PAGEOF  Surface Elevation:S972
5		LOGO	ING	SUPE	RVIS	OR W~	کے			DATE 7-2-99
TOP-BOTTOM OF CORE IN BOX	10P/BOTTOM OF INTERVAL	FEET OF COPE IN INTERVAL FIELD	SAMPLE NIMBER	FINCTURE	TAX OF THE STATE O	GIMIN SIZE DISTRIBITION	USCS	OFFIN IN	SOIL) LIPPOLDGIC LOSS	SAMPLE DESCRIPTION
BOX 10x1 0.0- 2.85	Rut 1 0.0 - 4.0	MECOVERY: 2.85	001 002 003 004	RS 150 RS 150 RS 150 RS 150 000 000	001 002 001 002 901 002	QI (002) (002)	SM	-1,0 -1,5 -2.0 -2.5 -3.0 -4.0 -5.0 -7.0 -8.0 -9.0		O.O-O.9 Clayer Silly Sand, dank Yolowish brown, 37R 3/4, pred. Very time and fine, some moderand Coarse, Silly, medium plassifity with mp to 5cm angular lattic, gravel, erganics, damp at 8,0thewis dry O.9-285 Gravelly Silly Sond, very, pole brown 27R 8/3 pred. very free to 5ilt, some time tocoarse, with up to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel ap to 4cm subangular littic savel
NOTE	ES: Ge	eneral:	uscs	is mo	dified fo	or this lo	og as fo	ollows:		Procedure No. RMRS/OPS-PRO.101

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Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

Bo Loc Da Ge	OCKY rehole ation te: ologisi lling E	Numl North	per: h: <u>74</u> 8 - 99	BH 924.	956 8 Ea: ERI	98 st: <b>Z</b> L			-	Y SITE BOREHOLE LOG PAGE OF 1 Surface Elevation: 5971 Ft Area: 703 PAP Lis Area Total Depth: 4' Company: TIERRA Project No. 6E66000 Sample Type: CONTINUOUS
1	ARS L				RVISO		000	<u>J</u>		DATE 7-2-99
TOP:BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF COPE ININTERVAL (FIELD MEASUREMENT)	SAMPLE S NUMBER	FINCTURE ANGLE	TAL BROWN THE	GPAIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LIPPOLOGIC LOX	
Bay 1001	104-00 1 # 100-40	Mounty; 3,2	001 002 004 004	RS 130 RS 150 RS 150 RS 150 RS 150	001 002 001 001 001 002 002	2I 002 002 002	64	-1,0 -2.0 -3.0 -4.0 -5.0 -7.0 -9.0		0.0-3.2 Gravelly Satty Spind, very dustry red to very pale brown 2,5 yr to 87R 3. 0.0-0.9 prod. very fine to fine becoming coarser w/depth, trace to some organics locally clayer, trace to some Sub- angular lathric gravel up to 5cm, 0.0-0.9 damp, 0.9-3.2 day  3.2-4.0 No Recovery

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Bo Loc Da Ge Dri RN AP	rehole cation te: ologis Iling E ARS L	Numl - Nortl	n: 74 3-17 7. 20 6E	13.119 1926 199 174 10 P.K	579 8 Eas ER 18 RVISC	SE TOR		48 	4 mis	Surface Elevation: 5910 Ff Area: 903 PAD Cip A ceq Total Depth: 4' Company: TIERRA Project No. 6E6600 Oc Sample Type: CONTINUOUS  DATE 7-2-99
TOP/BOTTOM OF COPE IN BOX	TOP/BOITOM OF INTERVAL	FEET OF COP IN INTERVA FIELD WE ASUMEME	BILLING KVENT	FINCTUME ANGLE	H BEDDING	GIMINSIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LITHOLOGIC	SAMPLE DESCRIPTION
		Recovery: 3,3'	002 003 005 006 006 001 002 003 004 005 006	25 150 100 ( 00 ( 00 ( 00 (	2 1 02 1 00 2 00 2 00 2 00 2 00 2 00 2	AL	Sc	- 1.0 - 1.0 - 1.2 - 2.0 - 3.0 - 3.3 - 4.0 - 4.0 - 7.0 - 8.0 - 9.0		1.0-0.8 Clayry Sond, dash, brown 3/R 3/3 pod fine to very fine, some medium tocoasse, suboms an trace stackty plastic day, ytrace to some mp to 4 cm amsular to subrounded lethic cravely durch ped, 3/R 3/6 solly, sow to medium prostaces some maist @ 1.0 trace sond trace some 1.2-33 Sondar (for, logally sandings to clayer sand Jisht brown to a 3.3-4.0, No Recovery to daist yelow 6/R 6/3 to 6/R 6/3 prodictly, with up to 4 cm angula to coarse, subapsular, stackto me plosticity, with up to 4 cm angula to subround, of littic scavel day
NOTE	ES: Ge	neral:	uscs	is mod	ified fo	r this lo	og as to	oliows:		Procedure No. RMRS/OPS-PRO.101

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Bo Lo Da Ge	OCK: prehole cation ite: eologis illing E	Num - Non	ber: h: 74 -//)-9	BH: 192: 19 UTH	958 2 YYEa ERI	98 st: <u>20</u> e <sub>R</sub>		2/9		Surface Elevati Area: <u>903</u> Total Depth: _ Company: 77	on: 5969 Ft PAD Lip Are:	PAGE <u> </u> OF <u>/</u> RO. <u>G.E6600</u>	-00
1	MRS L		ING 1	SUPE (a)	RVISC	SR W	æ			DATE	7-2-99		
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE ININTERVAL (FIELD	WINDER SAMPLE	FINCTIAL	4. BEDDING	GIANN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL) LIFFOLOGIC LOXI		SAMPLE DESCRIF	NOIT	
Bax 10x1 0.0-2.9	hin # 1 0.0 - 9.0	-	001 002 003 004	85	001 002 001 002 001 002 001		CL	i,o -2.o -3.o		dank Bro traces for to salvan damp to 1.6-29 6. 87R 8/2, to coarso, 5-14, Mp.	un slight to s a to coarse sam some up to b solar, pay, da	on Subso my Subso pinkish whi to fione, som mun dod, for	- 1. L
997	458 Samj			001									

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Boo Loc Dal Ge	rehole ation te: ologis	FLA Numi - Norti - 3 - t: quip	ber: 14 h: <u>74</u> -99 -	BH]5 9 140 -> THE	998 Eas 6-7 RER	st: <u>20</u> - 99	85			Y SITE BOREHOLE LOG PAGE 1 OF 3 Surface Elevation: 5976 ft Area: 703 PAN Total Depth: 25.0 ft Company: 116884 Project No 6E600000 Sample Type: CONTINUOUS
		.OGG VAL					2			DATE 7-6-99
TOPBOTTOM OF COPE HTBOX	TUPBOTTUM OF INTERVAL	FEET OF COPE INITATIONAL (FIELD) AE ASTABEMENT	SAMPLE PULMBER	FRACTING ARKIE	tit Utura. Arası E	DIMIN SIZE DISTRIBUTION	1151.5 5 TM(RI)1	1111 1111	\$011/ 111/4/11/05/11	SAMPLE DESCRIPTION
	, &									0.0-4.0 s.m.lan to BH 90998 see log
	0.0- 3.	2:35'				,		2.0_		
	lan # /:	Rocoun				:		3.0_		
	2,38-6.8	·	002 903	5.6	RS ISO VOA		SC	5.0_		3.8-6.8 (loyer Sand, brown 7.5 Th 5/4 fine to course, Sub- angular to bleomydod, lithic sayof, low plustic clay, some solt, worth mg to 4cm broken to submission
	Court	lacore	994	779	1900	71 ×	×X	7,0		lithic gravel, domp
	Rant 36.8-8.8	200 yes 1,55	001 003 99 A	779	9 04	<b>8</b> × ≤	Sc Y			6.8-8.8 Clayer Sand, A/A
	Ru-474 V	Recovery 2.4 6	002	, ,			SC	<u>-9,0-</u>		8.8-10.8 Clayer Sand A/A

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(2) Core breaks cannot be matched, accurate footage measurements not possible.

Bor Loc Dat Geo	ehole ation e: <u>6</u> ologist	Numb North	er. 1: 74 99-	BH 9140 -> 6	959 Eas - 2-	9 <u>8</u> t: <u>20</u> 99		793	S A	SITE BOREHOLE LOG  Surface Elevation: \$976 ff  Area: 903 PAD  Sotal Depth: \$25.0 ff  Company: \$\frac{17ERRA}{ONTIVIOUS}\$  Project No.:6\frac{60000}{6000000}
I	IRS L PRO		ING S	UPEF Lan	RVISC	DR Wo	v D			DATE 7-6-99
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE ININTERVAL (FIELD JEASUREMENT)	SAMPLE	FRACTURE ANGLE	BEDDING	GRAIN SIZE DISTRIBUTION	SYMBOL	DEPTH IN	SOIL/ LITHOLOGIC LOG	SAMPLE DESCRIPTION
	Run # 4 8.8-10.8	Riveres 2.4					Sc	10.0 108		Clayof Found A/A
	8.2		I	77	99 00	93 X	XY SC	/.0		10.8-12.5 Clapy Sand
	Run X 5	Racover	001 ,003 002	12.2	RS TSO VOA		CL	-20-		12.5-12-8 Clay, light-gollowish brown 2.576/8
	8-51-	, 6					SC	-13.0-  -14.0-		where fine to course tithic + carros so also up traces fine up to 1,5 cm subsound could down to maist
	20 H 6:12.8	Recover; 2	001 002 003	14.6 14.8 15-2 15.4 77:	Ł.	14 4		- -/50		12-8-15.8 Clayer Sand A/A,
	Rungy 1	Recovery:	~	7 7 7	1 00	04 5	£	16.0-		15.8-17.0 (loger Sand A/A
	Run 8 8.8.8	Recovery.	001 003 002	17.3 17.7 12.7 18.2	9 00	95 ×	Sc	/S,C	<b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> / <b>6</b> /	17.0-18.8 (layer Sand A/A
	Kun#9 18.8-200	Russery,					Ść	-19.0-		18.8-19.9 (Payey Sand A/A) = 196 6-24-99 19.9-20.0 No Brover

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Revision 0

Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate footage measurements not possible.

Date effective: 12/31/98

Boreh Locati Date: Geolo	KY FL.  ole Num  on - Non  - 3  gust: g Equip.	ber: // h: 74 - 79	BH9 146 THE	9 5 9 0 Eas 0 E R	98 st: Z. 299		<u>89</u> 3	,	Total Depth:	On: 597 PAD PS.D FF TERRA	- Project	No GEO	
	S LOGO ROVAL	ING SI	UPEF	VISO Van	OR L	alo	od		DATE .	7-6-9	79		
IN COLE	EET OF COPE HANDE AVAI PEET OF COPE (FIETO)	SAMPLE PUBLICE	FIRM THIS	Mitable	GIWIUSIZ INSTINBUTION	1,51.5	1111 1111	SOR/ LITTER COLIN			DESCRIP		
Run X 10	20.0-21,5 Recourt:	003				SC BR 0189 0375		0	20.0-20.5 20.5-20.6 massive, massive, phoder 20.6 TAL 6- 21.8-22.	Clayor Claysto dense y asticity, 29-99 Top	sand.  no, lig  nuis to  mais i  of Bed	A/A Sould Soul	vet . 2.57 5.71, 20.5 FA
Run X 1							220						
Run 2 12	7 182		24.6	00 R5	7 00 7 00Z 7 06Z	RS Wan	1 24.0 25.0		22.8-24.8 weathering	r, olive,	Yo Vow	2.57 6	16.
	:	ales:		<sup>7</sup> 00]	002	VOA VOA VOA			10:	25.0			

h S Materials amounts are estimated by % volume instead of % weight.

(1) Sadly broken core, accurate tootage measurements not possible.

(2) Core preaks cannot be matched, accurate tootage measurements not possible.

Procedure No. RMRS OPS-PRO.101-

Revision 0

Date effective: 12/31/98

Bo Lo	rehole cation	Num - Nort	ber: h7 <u>49</u>	BH 2	960	98 st:, <b>2</b>		REHO		Surface Elevation: <u>5978 F+</u> Area: <u>703 PAD</u>
Ge	ologis	t: <u> </u>	T. Li	THE	RER	<del>/                                    </del>	ua/	Well		Total Depth: 17.0ff Company: TIERRA Project No.: 6E 60000 Sample Type: CONTINUOUS
1	AG L			SUP	ERVI		Ivd	/		DATE
TOP/BOITOM OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL FIELD JEASUREMENT	SAMPLE	ANGE OF THE STATE	BEDDING ANGLE	GRAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN	SOIL/ LITHOLUGIC LOG	
	So			ANNE				- 1,0-		0.0-3.8 See Bowhole log of BH 90098
	1.0-3	3.4	·			·		-2.0-		
	Jun # 1	acovery:						3, <i>O</i> 3,4		3,4-3,8 No Russey
		1	001	RS ISO VOA			SC	-43 -43 -45		3.8-7.0 Sand Light Brown to
	3.8-7.0	30	993		002			-9.8 -5.0 		Strong Brown 7,5 TR 6/3 to 7,5 TR 5/6 fine to coarse, Subangular to Subrounded, Some to object and subcingular
	Runt 2	Berouns	_				5c	-6.0		to angular little gravel some to some to
	0.0-20	30						-/.O		grading to Clayer Sand Day to Ram with some powdery believe white; 1/8,5/16 7,0-9.0 Sand locally grading to Clayer Sand A/A damp
	Bunk 3	Perany	-	RS ISO UOA			SC	8-2 8-5		
	hunt 4						CL			9.0-12.0 Clay A/A with sand A/A with traces course, rounded Calicles con Lithic subungula fine to course some

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Bo Lo Da Ge Dri	cation cation ite: eologis illing E	- Nor (0) st:	nber: nh:14 29/9 7: 4 : 68	BH 9211- 18 → UTH EOPK	9609 TAVE 110/ ELEC OBE	\$ 20 \$1: 20   30   19   13	085 98 VAC	OREHO 6/2 WALL		LOG  Surface Elevation: 5978 Ff  Area: 903 PAD  Total Depth: 17.0 Pf  Company: TIERRA Project No.: 6E600000  Sample Type: CONTINUOUS
ı	a&G PRC			SUP Man				d		DATE 7-6-99
TOP/BOTTOM OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD	MEASUREMENT SAMPLE NUMBER	FRACTURE	BEDDING ANGLE	GPAIN SIZE DISTRIBUTION	USCS	DEPTILI IN	SOIL/ LITHOLOGIC LOG	SAMPLE DESCRIPTION
	Rund 4 9.0-12.0	Recover 40	21)				CL	11.0		locally grading to Sand, Clar
	Runx 5 120-150	Browny 4.0	003 009 704 015	R5 130 va1			CL	-12.3 -12.5 -13.0 -14.0		12.0-15.0 Clay; locally grading to Sandy Clay A/A
	1923 (50-16.3	KROVI	004	R5 750 VO4	,	- 6	BR.	-15.6 -15.8 -16.0 -16.3 11.25		15.0-15.8 (lay; locally grading to fandy lloy A/A  (5.8-17.0  Sandstone; Tollow 'OTR 8/8 fine to grading, Sombrough of mostly unconsolid highly fright, oxidized, quanty, saturated thanks (lay 45-14  Bedrock contact: 15.8  Th: 17.0
								 _9.ù		

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a Lided	ocation ate: Ateologis	Num - Non - Non - 1727	oer: h: <u>74</u> 103 79 R	B1 921. 3/9 KO OPAU	† 961 3 Ea 8 /2 EHU BE -	98 st: 20 -2-98 FR - Du	850 8-3, AL W	0REHC 087 02-3-98 MIL		Surface Elevation: 5977 f f Area: 903 PAD Total Depth: 18.8 f t. Company: TIERRA Project No GE 600000 Sample Type: CONTINUOUS
	PPRO									DATE 7-7-99
for BOTTORA OF COME	TOPRIOTION OF	FEET OF CORE HURTHANAL (FIELD)	SAMITE PRIMITE	XX AIKSIE	BEHBRA	THE HEALTHOIL	USCS 5 (1480)	DEPTH #4	SON / THEN OUR: LOSS	SAMPLE DESCRIPTION
75	Rust 1 0.0-3.35	PEWENY: 2.0								FOR INTERVAL 0.0-3.35 SEE LOG OF ROREHOLE BH90198
10f3 0.0-9.5	Rux 2 335-65	RECOVERY: 3.0'	- :	99A 1106 1107 1108	8210- Rad 5 I 50 VX	40 42 44	XXX SC	-4.6- -5.0-		3.35-6.35 Clayer Sand, Strong Brown, 7.5 YR 5/6; fame to modimon, locally course sond, subnounded to suban gular the lathic, very slight to mon plasting sond, clay, truck from to course gravel, dang.  35-6.50 No Recovery
B OX	RUN#3 (.5-9.0A.	RECOVERY 3.64+ including 0.74+ slowerh	09: <i>(</i> 3	99A3 002 008 014	KadS	n.s	6C	- 6.5 - -7.0 - -7.7 - -7.7 - -8.18.6 - -8.18.6 -		6.5-9.0ft; Clayer-sandy gravel; very pale brown (10487/4) grades down to lisht reddish brown (5486/4), quartrite gravel up to 2 cm, fructured, fine to medium subround to subanjular sand, firm, not plastic, slightly moist.
9.5	Run # 4					-	6C SC	7.5 9.5		9.5-9.5 As above 6.5-9.0ft. 9.5-11.5ft; Clayey sand (vare gravel); Continued next page

<sup>(1)</sup> Bacty proken core, accurate footage measurements not possible.

<sup>(2)</sup> Core breaks cannot be matched, accurate footage measurements not possible.

10 G	ROCI orenole ocation ate: leologis rilling 5	Num Non 10	noer: th: <u>74</u>	BH 1921 KUE	9619 3 == HLEA	18 st: Z	085			LOG PAGE 2 OF 2 Surface Elevation: 5977 Ft. Area: 903 PAD Total Deoth: 18.8 H. Company: TIERRA Project No. GE 600000 Sample Type: CONTINOUS
	G&G PPRC				,	SOR	love	l_		DATE 7-7-99
TOP BOLYON OF COPE	TOPMOTION OF	FEET OF CORE	SAMUE	XXX Allest	BETHHRE	SIZIS HIMOLD SIZIS HUMBILI SICI	USCS 5.1ABOL	OLPTO IN	SORT UIINA GGR.	
4	RUN #4	RECOVERYHOR					SC	-11.0-		light reddish brown (SYR 6/4), fine to medicin sand, subvoined to subangular, firm, slightly moist, gravel may be in lenses.
9.5-17.0A	11.5-14.0A.		10:59 10:53	∞9 015	Rads Iso Voc	12.0	SC	-12.5		As above 9.5-11.5 ft.
of 3	RUN #S	RECOVERY	99	A321	0-∞	3•X)		13.0- - 140-		
Box 2	HS-91-0:H1 9	RY 3.0 ft.	1		ð-∞ RaJS	·~ 3	XX GC		<b>S</b>	114.0-16.5 Similar to RUN#3 6.5-9.0ft. Pinkish clayey-sandy gravel, quarteile gravel to 2 cm.
	RUN #6	~ 四	13:19	010	Iso VOC	15.8		- 155 - -15.8 -16.0 -162 -16.5	9	
€ \$ \$ \$	RUN#9 16.5-18.89F.	8% 4.0ft.						120 	0 0 0	Bedrock contact 16.6ft.  16.6-18.8ft; Clayey sand, list-yellomish brown to yellow (104R 6/4-104R7/6), fine sand, firm to hard, slightly moiot.
Box 3063	RUN#1)	RECOURRY							00	TD 18.8 ft.
NO.	TES. G	eneral.	SCS	is mod	uñec (c	er this l	00 ES 10			

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184

m line	orenoi ocation ate:	e Nun 100 - 12 12	noer: th: <u>7</u> 9 /04	BH 1913.	962 5 E=	.98 1st: Ze	B0 0850 08LW1	<del></del>		LOG PAGE LOF 2 Surface Elevation: 5979 Ff Area: 003 PAD Total Depth: 16,544 Company: TIERRA Project No.6E600000 Sample Type: CONTINUOUS
E		LOG	GING	SUF	ERY	ISCR	, ,	2	· ·	DATE 7-6-99
tor BOHORA OF CODE	TOPMOTTOM OF	FEET OF CORE	SAMA E	XFIGGING.	BETHNIAG	OTWINSTEE DISTRIBUTION	uscs Setabor	1 663	SOH / UH KA GGR.	SAMPLE DESCRIPTION
OF 2 0.0-10.7 4.	Run#2 3.8-6.54. Run#1 0.0-3.84.	Recovery 2,8A. Recovery 3,1A.	10:46 10:46	02)	Rad S Isó VOC	3.8 4.0 4.3 4.7	6C	-3.0 -4.3 -4.5 -6.0		0.0-0.4 ft: Asphalt  0.4-3.8 ft; Clayey-sandy gravel;  yellowish rcd (5 yr 5/6), quartite  gravel up to 2 cm (most about 0.5 cm),  fractured to subround, fine to  medium sand - subangular to subround  fivin, slightly moist,  As above 0.4-3.8 ft.
o − ×o ⊕	Run # 3 6.5-9.0A.	Recovery 2.7 A.	11:16 11:15 11:17 11:11		Reds Iso Dup Iso Voc Dup		sc 60	8.0 - 8.5 _		As above 0.4-3.8ft.  7.5-8.0tt.; Clayer sand; clay.white 10 YR 8/2, sand-apolicy 10 YR4/11 weathered cobble?, fine As above 0.4-3.8ft.
	Run # 4 9.0-11.5R.	Recovery 3.1At.					66	—9.0 — —	<b>9 9 9</b>	As above 0.4-3.8ft.

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m Lipg	orenole ocation ate: eologis	e Num - Nom l	nber: th: <b>75</b> L/04	BH 1913 1918 DEH	962° 5 Eas	98 st: <u>2</u>	085	<del></del>		LOG PAGE 2 OF 2 Surface Elevation: 5979 Ff Area: 903 PAD Total Depth: 16.5 ft Company: TIERRA Project No. GE600000 Sample Type: CONTINUOUS
1	G&G PPRC				ERVI		ho	L		DATE 7-6-99
TOPEBOTTON OF COME	TOP/MOTTOM OF	FEET OF CORE	SAMILE SAMILE	X PINCTURE.	BEDDING ANGLE	CHAIRVII ION	115 C.S. 5 7 FABOL	OCPHH (N	SOIL/ 1111 SH OGIC 10G	SAMPLE DESCRIPTION
20/1/48	Run#4 9.0-11.5	Reaven 3.1 ft.								See privious page 10.5-11.5 Clayey sand; yellowish red (SYR 5/6) fine sand, slightlyplastic, slightly muist, firm.
2 10.0-11.88ft	Run #5 11.5-14,0ft.	7.4	11:53		160 VOC	12.75	SC	12.95 12.95 12.95 13.95		11.5-14.0 Clayey sand as above 10.5-11.5 ft  I cm gravel, subvound from 13.5 to 14.0 ft.  matrix is clayey said
BOX 20F	Run # 6 14.0-16,544	sesory 2 9 ft **	p:34 18:33	004	Rads. Iso.	5.7	xxx	-14.0 -15.0 -15.7 -15.3 -16.3 -16.5	000000000000000000000000000000000000000	14.0 ft. BEDROCK CONTACT  14.0 ft. BEDROCK CONTACT  14.0 ft. BEDROCK CONTACT  14.0 ft. BEDROCK CONTACT  16.5 ft. Stone  16.5 ft. Send, from, slightly  16.5 ft. TD
13:15 13:15 13:15	Rad So Isot	veenf pe-Ri	lihse Kse	99A3 79 <i>A</i> 33	10-00 110-00 110-00	ж,ос О,ж	) 12	19.0 19.0 19.0		** On removing the outer steel core liner from the hole about 1 ft of additional cored material was found. Evidently this instrict fell aut at the plastic Core liner, somegles from culting shoe. This Material was port into core look.

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					_		~ ~	_	DREHO	LE	
	loreh ocati				1900	496.			5610		Surface Elevation: 5979 Ft  Area: 903 PAD.
	ate:				8 -		-8-	98	<u> </u>		Total Depth: 16.5 F f
						ERE	R	Ot			Company: TIERRA Project No.: 6E600000
	rilling	Equ	ip.:	6E	OPR	OBE		NAL	WALL		Sample Type: <u>CONTINUOUS</u>
ı	G&C			ing		Par			d		DATE 7-6-99
-	72	Jyr.	, É		<del></del>	<del></del>				٠ ا	
TOP/BOTTON OF COPE	TOP/BOTTO	INTERVAL FEET OF COS	MEASUREME	BAMPLE NIMBER	FRACTURE	BEDDING	GRAIN SIZE DISTRIBLITION	USCS BYMBOL	DEPTH IN FEET	BOIL/ LITHOLOGIC	SAMPLE DESCRIPTION
											0.0-3.8 See Borohde leg et
	,								1.0-		BH 910 98
	1	7.7	7								
		0.0	V						2.0		
			į,						2.7=		2.7-3.8 No Recover
	7	17	2000						3.0_	$\bigvee$	1. 7. 0 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.
		200	Re		<b>10</b> 2				3.8		
	1	0	P	0/02	PS ĪSO			<u></u>	-4.0 -4.3 -4.5		3.8-6.5 Sandy Clay; light yellowish
	30-	ol '	0	203	VOA			66	4.8		plasticity with fine to
	1	7	, ,	99	A4	1/2-	001-	.XYX			coarse subangulas 40 Subroyande
	7	2	200						-\(\daggregartarrow\)		Jothic Sand Trace Staves
	&	4	3						-6.5		
	2	2		20			27		_7.0	8	6.5-9.0 Sand; Strong brown 7.71
	6-5	7 7	200	194	419	2-0					angular locally solly tounded to
	~	'9	10	04	R5			56	8.0		clayer, also with fine to median
	Runt	0		06			e de la companya de l		- 8.4 - 8.5 - 8.5		Locally grading to May y Sond
	√ #	1 ~		1		1			7.0	1	9.0-11.5 "Layey Sand/
	Pun		18					76/	- +	C	locally sending to:

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Lo Da Ge Dri	cation cation te: cologis illing E	- Nor - Nor - 2 st:, quip.	nber: rth: <u>7</u> - 7- 98 7- 6	BH 4906	963 12~ 12~ EREI 10BE	98 st. 2: 8-9 P	085 8 VAC	REHO		LOG  Surface Elevation: 5979 ff  Area: 703 PAD 5  Total Depth: 16.5 Ff  Company: TERRA Project No.: 6E6000 00  Sample Type:
AF	PRO	VAL		Mank	<u>_ ω</u>	ord				DATE 7-6-99
TOP/BOTTOM OF COPE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD	SAMPLE NUMBER	PRACTURE ANGRE	BEDDING	GPAIN SIZE DISTRIBUTION	USCS		SOIJ LITHOLOGIC LOG	
	Ren # 4	Rec. 21	1100				Sc,	11.0		Sandy Clay P/A, doup
	115-14.0	33,	007	R3 Zso YOA			CL	-12.7 -12.4 -12.7 -12.7		11.5 to 14.0 Sandy Clay; Reddist. Brown, 57 k 4/3 trace to some plasticity, with fine to coorse subangular said (ty), locally
	Run #5.	. Rocan				. 4	611 5C	13.0- 	9/9/	Subangelax Said (1991) (ocally) Some fine ungular lattic graves si day 12.7 to 13.8 Gravilly Sand; sea bout emistatuents.  13.8-40 Cloyer Sand see above for constit.
	Ran X6, 14,0-16,5	ROCOVERY 38'	010 011 012	RS 750 VOA			BR mona 7/U	15.0 15.0 16.0 16.2		140-16.5 Claystone, light Olive gray 57 locally weathered, Mother with other dense, locally some 5/5/6. Blocky, dense, locally some light gray N7 very firm sand day wet 014.0-14.2
								-17.0- - 18.0- - 19.0-		Assumed Brown contact @ 14.0  Last Sample lost from samples, whieved with Inal wall.  TD: 16.5'

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							во	REHO			PAGEOF3
Bot	rehole	Numb North	er:		964 Eas		85	910		Surface Elevation Area:903	on: <u>5976 FF</u>
Dat	te: <u>//</u> /	121/9	78 -	101	26/9	98			•	Total Depth:	23.0ff
	ologisi Iling E				BE		DVAL	WALL		Company: <u>///</u> Sample Type: _	ERRA Project No.: <u>6 E 6000 O</u> C CONTINUOUS
					ERV		0				
AP	PRO	VAL.	M	arle	<u> </u>	Sov	<u>\times_{}   </u>			DATE_	7-6-99
TO WE X	TTOM	CORE PVAL D MENT)	'LE JER	URE	Î.E.	GPAIN SIZE DISTRIBUTION	SSL	3	SOIL/ LITHOLOGIC LOG		
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOI OF INTERVAL	FET OF INITE	SAMPLE	FRACTURE	BEDDING	GPAIN	USCS	DEPTH	SOIL		SAMPLE DESCRIPTION
-	_	F. 2				-	$\vdash$			00-38	See Bonohole log of
										0.0-3.8	BH 90998
								-10-		<b>'</b>	911 10 7 78
	8.8	7						1.0			
	00-3.8	$\sim$						<b>-</b> -			
	9	~						-2.25			
	_	- ,						2.25		225-38	No Rocovery
	Ann #	7							$] \setminus /$	2.2) - 3.8	the Mace of
	7	100						-30-	X		·
	Pu	Pac							$ / \setminus$	ĺ	
						4.0		3.8	1/6/		
				001	RS	4.4	<	-4.4			Clayer Sand
	-			007	ISO	4.8	DC.	4.8		med line	Some coarse, sub engular
	2.8			013	1.00	5.2		<del>5</del> .20—		to subron	aded some median, fold- que 1/2, clayer, segue 5. H.
	,	~						3.2		spar and	questa, clayer, some site
	8	. 7	99	A32	10-	001-	<i>11</i> 1×	_		Traces Mp	to 3 cm bolom father
	3,	3					S.C	6.0-		Evaded "	noist
	^.	, ,					5				
	74	Ven						20			·
	4	000									
	Sy.	R								7.53-7.8	No Recovery
	2							-8.0-	HUIN		ned Sampler to 7.5 due to
	11.0									1 .	cen liner and stoo
	3			002	01			<b>-</b>		7.5-11.0	S-lay Grovelly Soud
	6.				· · ·		5M	9.0		Dud VLAY	line to fine tage med and
	13			008	<i>I50</i>				FAT	Coarse, Sy	from ded to Sa banger on, lace
	MM			014	VOA			10.0		Very Silly	ant bolon littic gener
L				L			1	10.0	$\Pi\Pi\Pi$	10 Thank	ani on see Exiline

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Bo Lo Da Ge	rehole cation te:/	Num - Nort - 0/2/ t:	ber. h: <u>74</u> /98	BH 9 1914	649 _Eas	8st: <u>Z</u>	85	REHO		LOG  Surface Elevation: 5976 Ff  Area: 903 PAD  Total Depth: 23.0 Pf  Company: 17ERA Project No.: 6E6000 ecc  Sample Type: CONTINUOUS
ı	&G L			SUP Man	1		ۍ.	<del></del>		DATE _ 7-6-99
TOP/BOTTOM OF COPE IN BOX	-	W = 2	w c	FRACTURE	BEDDING	GPAIN SIZE DISTRIBUTION	USCS	DEPTH IN FEET	SAMPLE DESCRIPTION	
	Ruffs						6M	10.0	000	7.5-11.0 Conty Gravel Size A/A; Inaces Calicle, day
	Run Hy 11.0-14.0	Provery 36	003 009 015	KS 730			50	-12.0 12.2 -13.0 -13.5		11.0-14.0 Clayey Sand Samo as @ 3.8-7.53 day
	Run #5 140-170	2	004 010 016	RS 730 VOA			SC 617 CL	14.5 15,0		14.0-14.5 Clayer Sand Sams 95 96000. 14.5-15.9 5-14+ browth Sand Same 95@ 7.5-15.0 dax 15.9-16.5 Sandy Clay 5.730 and texture same 95@ 3.8-7.53 day. 16.5-17.0 No Recover
	Run #6 17.0-20.0	Prinax: 2.6		2		Ra: 2.6	(8.6-19.9 5 hand 6 170-18.6	- 18.0 - 18.6 - 19.0 - 19.9	4 4	17.0-18,6 Clayer Sand Same 25 Q, 1 11.0-14,5. Obstruction Q 18.6 which required run & 7 from 18.6-19.9  18.6-19.9 Clayer Sand as a beve

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								REHO				PAGE 3 OF 3
		e Nurr		BH 49 14	764 1 = 2			910		Surface Elevati Area: <i>903</i>	on: <u>5976 Ft</u>	
Da	ite: 🔟	<u>0-21</u>	- 78	<b>→</b> /	0-20	395 5-95	3			Total Depth:		
				EREK		1311	11	WALL		Company: 7/	IERRA Proje	ct No.: <u>6E 6000 o</u> c
								WALL	<del></del>	Sample Type:	COUTINUOUS	
		VAL		SUP Ma	- 1	`	\	<u>Q</u>		DATE_	7-6-99	
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF COPE ININTERVAL (FIELD	8 AMPLE NUMBER	FRACTURE	BEDDING	GPAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN FEET	SOIU LITHOLOGIC LOG		SAMPLE DESCR	IPTION
								20.0	9/4/		Clayoy Sand	Samo as
	30	1						<b>-</b>	[9/9/]	above		
	73						SC	21,0			•	
	19.9-	2	006	0.5				21.4				
	İ	1 10		R5				<b> </b>				
	000	>		750			ļ	22,0	10//	22,0-23.0	Silty Claysto	ne Tor of Bodios
	#	70	018	VOA			BRS			c/althouse	then I- It	= 22.0 FF
	Run # 8	Rec					7/0/9	7 -		generally of	Silty Claysto Heard, slightly orhy, donse, my tic patterns, do	id. frig He, Some
								23,0		Myo dandu	tic patterns, da	<i>y'</i>
										TO=	23.0'	
		-										
				1								
			J									
		1							1			
		]										
												·
							-		1			·
-												
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- (1) Badly broken core, accurate footage measurements not possible.
- (2) Core breaks cannot be matched, accurate footage measurements not possible.

Borehole Number: BH965 98 Location - North: 249147 East: 2085867 Date: 5/7-99 Geologist: JUTHERE Sample Type: Continuous  RMRS LOGGING SUPERVISOR APPROVAL Mank Wall Bush Supervisor Sample Type: Continuous  RMRS LOGGING SUPERVISOR APPROVAL Mank Wall Bush Supervisor									FCHNO		
Drilling Equip. <u>Geoproble Dual Wall</u> RMRS LOGGING SUPERVISOR  APPROVAL Mark Ward  DATE 7-7-99  SAMPLE DESCRIPTION  SAMPLE DE	Boo Loc Dat	rehole cation te:S	Numt North	oer: n: <u>7</u> <del>9</del> 7 - <del>9</del> 9	BH 1914	965 ZEas	98			,	Surface Elevation: <u>5976 FF</u> Area: <u>103 PAD</u> Total Depth: <u>23 S</u>
APPROVAL Mark Word  DATE 7-7-99  SAMPLE DESCRIPTION  SAMPLE DESCRI	Drii	ling E	quip	GEO	PRO	BE	DUA	26 4	ISLL		Sample Type: CONTINUOUS
80.0-3.8' see log for  BH90898  20  38  30  30  30  30  30  30  30  40  30  30	RN AP	ARS L	.OGG VAL	ING S	as .	RVISC	OR W	vel			DATE
20 - 30 - 30 - 30 - 30 - 30 - 30 - 30 -	OF CORE	TOPBOTIOM OF OF INTERVAL	FEET OF CORE INHITERVAL (FIELD) MEASUMEMENT)	SAMPLE	FRACTORE ARKEE	BE DORKT AMERE	GIMINSIÆ DISTRIBUTION	USUS	N 11 11 11 11 11 11 11 11 11 11 11 11 11	SOIL/ (HEEROGR.	SAMPLE DESCRIPTION
20 - 30 - 30 - 30 - 30 - 30 - 30 - 30 -											0.0-3.8' See log for
38  38  38  38  38  38  38  25  40  38  25  78  80  25  78  80  80  80  80  80  80  80  80  80									10		BH90898
20- 20- 38- 38- 40- 38- 40- 38- 40- 38- 40- 38- 40- 38- 40- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 78- 25- 25- 25- 25- 25- 25- 25- 25	:	2. 3.	3						7,0-		
30- 30- 30- 30- 30- 30- 30- 30- 30- 30-		0.	3.6						70		
3.8  3.8  4.0  3.6-6.8' Clayry Sand wood here  2.5 TR 5/2,25 TR 4/2, pred vi  50  50  50  50  60  60  60  60  60  60		_							2.0		
3.8  3.8  4.0  3.6-6.8' Clayry Sand wood here  2.5 TR 5/2,25 TR 4/2, pred vi  50  50  50  50  60  60  60  60  60  60		#	72						20		
25 TR 5/2 25 TR 4/2 pred Valor to Salvand of to goong, Sand No. 1002 4,6 VAA SC - 2.5 TR 5/2 2.5 TR 4/2 pred Valor to Salvand of sand for sand, Sand of to 3.5 cm and angular lattic ground of the gro		ich	1000					-	<b>-</b> 9,0		
2.5 TR 3/2,2.5 TR 4/2 prod VI 2.5 TR 3/2,2.5 TR 4/2 prod VI 50 to Subnounded from Joseph destrict, the Some sill, Some med to cooking, Some to Subnounded from Joseph destrict, the Some sill, Some of to 3.5 cm 4.0 and angular lattic ground destrict of the second destric		8	-	Det	is 0	. 84				787	
Some sill, Some grand to cooning, some mind to cooning, some has first of the subnormal of the planting of the some first of the some sill, Some of the graves of the sound of the graves of the sound of the graves of the sound of the graves of the sound		6.8		003	4, 2	750			-7,0		3.6-6.8 (layry Sand wood led)
10 Subnounded for plasticity, the Some fill, Some of to 3.5 cm.  50 - 6.0 - 2 and angular lattic ground de some of the ground de som		-8	1	002	4,6	VPA					
99A6817-001-xxx 68 18-9.8' Clay of Sand 6.8-8.4 6node		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	3					<i>J</i> 5	-50-		to subnounded to plasticity trace
3 99A6817-001-xxx - 68 18-98' Clay of Sand 6.8-8.4 Goods		Ŧ 2	· .				-	SC			Some Sitt, Sorry of to 3.5 cm from
7.0-16.8-9.8' May of Sand 6.8-8.4 Grade		1	4100						-6.0-		and angular 1-11/1 grand day
6.8-9.8' May of Sand 6.8-8.4 Grade		R	Pa	99A	1811	7-001	- <i>x×</i> >		6.8		
		,							-7.0-		6.8-9.8' May of Sand 6.8-8.4 Grading

	ocation Date: Geologis Orilling E	<u>5-19</u> tt:	7-99 Lu	THER	E.R.				<del>-</del>	Area: 103 VAD  Total Depth: 23 \$  Company: TIERRA = rolect No.6E 600000  Sample Type: Continuous	2
. E	RMRS I	LOGG VAL	ING S	an i	RVISO	OR W	vel			DATE 7-7-99	
TOP:BOITOM OF CORE	TOPBOTTOM OF	FEET OF CORE IN HITE RAVAL (FIELD)	SAMPLE	FIVACTURE	BEDDING ANGE	GIMINSIZE DISTRIBUTION	USUS SYMBOL	# 117 117 10	SOUZ (HEENOGE: USE	SAMPLE DESCRIPTION	
	Pun X38-68 Run #2 38-68 Run #1 00.38	" Rooms 3.9'	99A 002	40 42	RS ISO VOA	- x*>	SC	-1.0 -2.0 -3.0 -3.0 -4.0 -5.0 -5.0 -7.0 -9.0		3.6-6.8' Claying Sand wood Not BH90898  2.5 TR 3/2,25 TR 4/2, pred virg to fine Some mid to cooning, safer to subnounded from plasticity, traco: Some soll, Some of to 3.5 gran fact and angular lattic groves days  6.8-9.8' Clay of Sand 6.8-8.4 broadings to Sandy Clay (2 8.4-9.8 Shoons Brown 7.5 TR 5/6 Components  P/A day to damp.	10 10 0
		1	L	1	L			i	11/		

Procedure No. RMRS/OPS-PRO.101

Revision 0

Materials amounts are estimated by % volume instead of % weight. (1) Badly broken core, accurate footage measurements not possible.

Date effective: 12/31/98

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Bor Loc Dat Geo	enole	Numb North	er. <u>/</u> : <u>74</u> -99	3H 9 914 -> THE	7 Eas 8-FR	50	85 9	ECHNO EG7	S A T	SITE BOREHOLE LOG PAGE 2 OF 2 3  urface Elevation: 5976 ff  rea: 903 FAD  otal Depth: 23.8  ompany: TIERRA Project No.:6E600000  ample Type: CONTINUOUS
RM	IRS L	OGGI		UPEF		)R			- 3.00	
AP	PRO	VAL .		011	MK		Vor		<del></del>	
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF COPE IN INTERVAL FIELD JEASUREMENT	SAMPLE	FRACTURE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTH IN FEET	SOIL/ LITHOLOGIC LOG	
	-83 (4 x)	my: 31"	001	181 11.2 R	7-00	3-X	5C	10.0   1.0		9.8-12.8, Clayer Sand: 15 At hour. to dark brown 7.5 yr 6/3 to 7.5 pg 3/3
	Sunt.	Rocos	003 002 092	1162			//	20	3 0	12.0-12.8 (layly Sand; with gome gravel Goddish follow fin to coars
	12.0-15	4.0	TAL	6-15	99		56	/3.0		Sand, fine to coase, subscended to surang Jense, maist-wet 12.8-150 Sandy Clay with trace fine
	Runts	Rocorus					CL	-14.0- - 15.0-		gravel fire to foot to factor you gravel for calacte no of stages of plasticity, stiff to calacte no of stages of the property 2.5 18 moist 12.8-13.5 last elive gray 2.5 18 to 13.5-15.0 mothed, dom, red 2.5 th 5/6 to the dive gray 2.5 TR 6/2
	150:18.1)	,0,	002 003 001	15.2 15.6 15.8 16.0			CL	16.0-		15.0-17.0 Sand (loy (L) voth Some fine graves for to come som Sabramaded, to Sabangular Stiff and mattled light dive may 2.5 mb/
	The state of the s	y Cours	99A	6817	-004	- >>	SC	17.0-		17.0-18.0 (layor and fine to course graves
	Run X	1					Ġw	-B, C-	(1)///	with floy dense maist. Gravel: abactgitz milble-broken, angalar 18.2-18.6 No Recovery 18.6-21.1 Gravelly Sand reddish yeller
	Run#8	RECOVERY					60	-17.0-		2.5 / R 6/6 fine de coarse su fans esta de su brown ded lattic, broken to Su bange ap la filic grave, sitter, locale

NOTES: General: USCS is modified for this log as follows:

Materials amounts are estimated by % volume instead of % weight.

Procedure No. 14 Azes Be

Revision 0

(1) Badly broken core, accurate footage measurements not possible.

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Boo Loc Dat Ge	rehole ation te: ologis	Num: - Nort: - / t:/	ber: // h: <u>74</u> ク〜タ	BH9 9147 9-3 UTH	659 Eas 5-21	8 st: <u>20</u> -99 =R	085	ECHNO 867 	; -	Y SITE BOREHOLE LOG PAGE 3 OF 3  Surface Elevation: 5976 FF  Area: 103 PAD  Total Depth: 23.8  Company: TIERRA Project No.: 6E 6000 00  Sample Type: CONTINUOUS
	IRS I PRO		ING S	21/1	RVISC		Vov	d		DATE
10P/BOT10M OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD MEASUREMENT)	SAMPLE	FRACTURE ANGLE	BEDDING	GPAIN SIZE DISTRIBUTION	USCS	OEPTH IN FEET	SAMPLE DESCRIPTION	
	Rums 8 18.6-21.1	RECOVERY:					60	20.0		dundont low plastic clay, saturated to 18.8 - Jamp 18.8-19.9
	Rum # 9	DUABLE TO DETERMINE		223 Vo4			6 <i>C</i> 5 <i>C</i>	22,0		21.1-22.5 21.1-22.4 Gravelly Sand A/A wot. locally grading to Clayer Samp 22.4-22.5 Claystans, BR Contact 0224
	Run 3 10 *20.8-23.8	Roovery	003 001	150 150 23 23	9 1 17 <b>00</b>	5 ×	BRO	23.0		225-23.8 (laysone 2.5/R 3/3) darh olive brown OTR 7/1, light gar some 10/R 6/8 brownish , slow-oxiding of weathered, placally dense + waxy, pourly ind mad fra able, w/ yery fine (gray) sand, site
	* Ao	Eve	apsoo	05	1 1	led 2-23	S			Porally grading to Ently Noyston
		٠								

Materials amounts are estimated by % volume instead of % weight.

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

	loreno .ocatio late: _ leolog	ie Nun	nber: th: <u>79</u> 2 - 59	13H 9 1912 →5-13 UTH	669 8 Ea 3-99 +	8 st: Z 6/8/ ER	199-	846		System Borehole Log PAGE OF 3 Surface Elevation: 5977 FF Area: 903 PAP Total Depth: 23,1 FF Company: TIERRA Project No. GE6600 October Sample Type: Continuous
		LOGO OVAL					u	lord	7	DATE
TOP-BOTTOM OF COPE	10P/80110M Of	FEET OF CORE IN HITE RVAL (FIELD	SAMPLE	FIVCTURE	BLODINA ANNE	GIMINSIA DISTRUBUTION	115CS SYMBOL	M PH IN	SORJ UTEKNOSIC	SAMPLE DESCRIPTION
	Run # 3. 6.8-9.8 Run # 2 38-68 Run #1 00-38	32' Recourt: 39' Recourt: 29	99A 002	4.2 4.6 664 7.8 8.0 .2	RS 150 VOA RS 150 VOA 9 00	,	SC.	-1,0- -2.0- -3.0- -3.0- -3.0- -6.0- -6.0- -8.0- -9.0-		2.9-3.8; No Brovery  3.8-6.8' Clayor Sand, Strong brown to light brown 7.5 TR 5/6 to 7.5 TR 6 pod very fine, some median to coaks angular to subrounded, lithic sand low plastic clay, sitty, with some probable of angular to broken lithic shall form angular to broken lithic shall form of the shall for

Materials amounts are estimated by % volume instead of % weight.

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Date effective: 12/31/98

Bore Loca Date Geol	ehole : ation - e: <u>5~/</u> logist:	Numb North 12-9	er. <u>f</u> : <u>74</u> : 9→ 5	749 1125 13-7 74E	6698 3 Eas 39 41 RER	? t: <u>Z</u> 0 D 6-	858	346 >6-9-99	S A T	SITE BOREHOLE LOG PAGE 2_OF 3  Surface Elevation: 5977 F4  Area: 93 PAI  Sotal Depth: 23   F1  Company: TIERRA Project No.:6E600000  Sample Type: 0NTIVVOUS					
RM	RMRS LOGGING SUPERVISOR APPROVAL Mark Word DATE 7-7-99														
1	- T	FEET OF CORE IN INTERVAL (FIELD (EASUREMENT)		FRACTURE		GRAIN SIZE DISTRIBUTION	USCS SYMBOL	DEPTH IN FEET	SOIL) LITHOLOGIC LOG						
	188-128	'y 24'	99A	664	9 00	<i>k</i>	before S	10.0 		9.8-12.8 9.8-10.4 Growthy Sand; yeary pale brown WTR 8/4, primarity very fine to fine, some medium to coarse, Sylvansalar to sylvan lithic sand, fine to coarse, Subangulo lithic sand, fine to coarse, Subangulo					
	Run XI	Rocove	801 803 802	12.9	RS ISO VOA			12.2		Total Sandy Clay grading to Clay w/ 10.4-De Sandy Clay grading to Clay w/ Some Sandy gravel, very pole brown to we 10/R 7/3 to 10R 4/2 mist, 12012.2 Saturated &					
	nts. 12.8 - 15.8'	overy; 2,9'	·				CL / 1/1/4			12.8-15.8 clay with perched water to 10.7' 12.8-14.2 (lay, with some sand, A/A moist. 14.2-15.7 Sandy clay A/A moist. laally grading to clayer cond. 15.7-15.8; No recovery					
	3 Runt 6 128-173	a Rocoper .	601	17,5			SC	15.\$ (6.0-	9//8	Gorehole a handoned 5/13/99  15.8-17.3'  Clay: reddish yellow to very gals brown 7,5 yr 7/6 to 10 yr sight plasticity; to some prod. fine to coarse sand, traces of some product to subangular, up-to 4cm li 17.3-18.3, Clayer Sand: strong brown to					
	Runk7 173-183	MEZOYE.	002	7.7	930	90 / x	ζί *	- <i> </i> 8,0-		Very pyle brown 75 YR 5/8 to 10 1/2 1/3 fine to coarse. Subungular, lithic sand, lo to man pluster for davel 4/4 with 18,3-19.8 Clayer Sand: A/A with					
	18.3 - 18	RECOVERY	00/				SC	19.0-	3 9	18.3-18.9					

Revision 0

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Date effective: 12/31/98

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE BOREHOLE LOG  Borehole Number: BH96698  Surface Elevation: 5977 Ft  Location - North: 749128 East: 2085846  Date: 5-12-99 > 5-1399  Geologist: 7: LUTHERER  Company: 71ERRA Project No. 6660													
Boo	rehole cation	Numl Nortl	oer: n: <i>74</i>	1912	7667 8 Eas	7 <u>8</u> st: <b>2</b>	085	846		Surface Elevation: 59//FF  Area: 103 PAD			
Dat	te: <u>-5</u> -	12-9	9-> 5	-13-8	9				-	Total Depth: 23,/			
Dri	ologis Iling E	t:/ quip	SE	PROPRE	BE BE	Z	na /	Wall	( )	Company: TIENRA Project No. GEL0000L			
i	ARS L			UPE	VISO	OR as le	/ 	Wood	1	DATE			
2	¥	# 7 E	_	T	T	мã	T	2					
TOPBOTTON OF CORE INBOX	TOP/BOTTOM OF INTERVAL	FEET OF CO INIMITERY INIMITERY INIMITERY AEASUMEMI	SAMPLE NUMBÉR	FINCTIME	BL DDIFRS APRSEE	GIWINSIZE JOISTRIBUTION	SYMBO!	1111	SOR/ LITHAN OUN LOSE	SAMPLE DESCRIPTION			
	200	Elia,	003		TAL	75	30	20.0	6//1/	19.8-20.6 Clayer Gund A/A			
	19.20 A	13 E	002	99A'	9300	2	لربد	<u></u>		4			
	1000 St. 6	LUDAO			·		SC	21.0		20.6-21.6 Cloyer Sond A/A nowith.			
	- · · v		TAL 6	129/99			1	220	6/6/	21.6-22.45 (Seyey Sand A/A maist			
	- m	14	7	22.4			SC	22,45		brown 10/R 7/3, dense loggly waxy, mod fright, mod on dense loggly waxy, to let stone w sill dans			
	サル	2002	2	228	-		BRS		W///	brown 10 yR 7/3, dense, logally waxy,			
	8 V.	6	003	23.0			7/6/9	7 23.6		mod fright, mod inglisted, for only			
			99 A	793	000	XX	ł	23,1 -23,5 -		Topof Bedrock = 221.45			
				•	·			2717		112: 23.1			
			·										
									-				
								<del>-</del> -		·			
								<b>-</b> -					
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							1			<u> </u>			

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Eo Lo Da Ge	rehole	Num - Non - Y:	ber: h: <u>74</u> 2 8 / 9	BH9 1910 9-> UTH	679 B Ea 57	8 st: <u>2</u> 12 - 9 ER	29	TECHNO 5866 		Y SITE BOREHOLE LOG PAGE OF J Surface Elevation: 5977 f f Area: 903 PAD Total Depth: 20.8 f f Company: 17 FRRA Project No. 6 E600000 Sample Type: CONTINUOUS
1	MRS L				RVISC		Voc	J		DATE 7-6-99
TOP/BOTTOM OF COME INBOX	TOPRIOTION OF INTERVAL	FEET OF COPE IN INTERNAL FEELD FEELD	SAMPI E NIMBERI	FHACHHE. ANGLE	BEODRAT APKIE	GIMINSIZE DISTRIBATION	USCS	N HI d 10	SOIL) LITHOLOGIC. LOST	SAMPLE DESCRIPTION
2	Runk 3 6.8- 5.8 Bunk 2, 3.8-6.8 Runk 1 0.0-3.8	102:34 RECOVERY. 33'	7ALS 001 003 002 002 002		\$ 500 0A	701-	SC XXX Cl	3.0 3.8 4.0 3.8 7.0 7.8 7.0		0,0-3.3 See bore hole  log for EH90898 or  BH91398  3.3-3.8; No Recover  3.8-6.8, Clayer Sand; Y. Vouist het  to pale yillow, 5 YR 5/6 to 2.5 y 3/4  some lift and IpR No men to pa of interval  fine to coarse, angular to suprement  littic sand, non to low plastic clay,  some to abundant, fine to coarse  Supremended to broken, littic sove  Jamp.  6.8-9.8 Sandy lay: light say  Joy powish brown 107R 7/1 to 10 YR  to yellowish brown 107R 7/1 to 10 YR  midium to goops & sub angular to suly  nounded littic + gupity Sand with  tigger up to 4 cm broken, to suly  tigger up to 4 cm broken, to suly  liftic gravel, non to low plastic  clay dry to damp.
						<u>_</u>	<del>-</del>	<u> </u>	///	Procedure No. RMRS/OPS-PRO.101

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Borehole Number: 1817678 East 2085864 Date: 4-88-77 > 5-12-99 Geologist: 2-28-95   5-12-99 Geologist: 2	R														
Geologist: Thread Project No. 166 6000 at Sample Type: Contributors  RMRS LOGGING SUPERVISOR  APPROVAL Mark Wall of Supervisor Super	Bo	rehole	Num	ber:	1349	677	78	205	Q I. (a			ion: <u>5977 F</u>			
Geologist: Thread Project No. 166 6000 at Sample Type: Contributors  RMRS LOGGING SUPERVISOR  APPROVAL Mark Wall of Supervisor Super	Da	ite:	1-28	199	<i>→</i>	5-12	-99	05	<u>50</u> 0						
RMRS LOGGING SUPERVISOR APPROVAL  MANK WOLLDWING  SOUTH STORY  AND SOUTH S	Ge	ologis	t: <u> </u>	64	THE	RER				(	Company: 7	TERRA Project No. 6E 6000 00			
APPROVAL  Mark Word DATE 7-6-99  SAMPLE DESCRIPTION  RECORD RS 12-2  RS 18 1-2  RS 200 RS 12-2  RS 18 18 18 18 18 18 18 18 18 18 18 18 18	Dr	illing E	quip.:	DE	PRI	BE	110%	16 1	WALL		Sample Type:	CONTIVIOUS			
SAMPLE DESCRIPTION  2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RI	MRS L	.OGG	ING:	_	•	`		0						
10.0 Sandy Clay with Gome gravel  A/A. damp-day  11.8	AF	PRO	VAL		Mo	NK	ک	coc	<u> </u>		DATE	7-6-99			
10.0 Sandy Clay with Gome gravel  A/A. damp-day  11.8	MO # 7	₩ 7	SAL SAL	w c	# /	8 "	IZ TON		2	3ic					
10.0 Sandy Clay with Gome gravel  A/A. damp-day  11.8	7807 7008 7008 8008	OF OF TERV	SEE SEE	AMPL	S C	EDDIN	RIBU	YMBC	FEET	2017		SAMPLE DESCRIPTION			
10.0 Sandy Clay with Gome gravil  A/A. damp-dry  A/	0 0	ō Z	FEET	s Z	WAL-1	2	AB DIST	200	č	5	98-118				
11.8		67/-	Š					1	10.0		Sandy (	Lax with Some Gavil			
11.8 11.8 12.2 12.3 12.2 12.3 12.3 12.3 12.3 12.3		16	N						-						
11.8 11.8 Cay, wat some grouped of the sound		1	١٤					10,	11		A/A . 0	amp-Oxx			
185 188 Clay water some savel  180 185 188 Clay water some savel  180 180 180 180 180 180 180 180 180 180		#	14					102	11.0-	1//					
185 188 Clay water some savel  180 185 188 Clay water some savel  180 180 180 180 180 180 180 180 180 180		3	N. O.			]			L -						
Some Stand Clay, with some ground control of the ground control of the some ground control of the		-		<del> </del>	<b>├</b>	1, 2		<u> </u>	11.8						
13.8-15.8  Sandy Clay, wolk Some Shave!  Out 150 Ony - James  Out 15,8-15.8  Sandy Clay, wolk Some Shave!  Out 150 Ony - James  Out 16.0 ony 16.0 ony 25.77 pc  To broughty Clay, Joseph Gray 25.77 pc  To bro		8	1	001	RS 1	2.7			122	1//	(1.8 2, 1.28)	Clariust som grovel			
13.8-15.8  Sandy Clay, wolk Some Shave!  Out 150 Ony - James  Out 15,8-15.8  Sandy Clay, wolk Some Shave!  Out 150 Ony - James  Out 16.0 ony 16.0 ony 25.77 pc  To broughty Clay, Joseph Gray 25.77 pc  To bro		1-2	3	003	I50 )	2.5		No 7	1499		1 /1	to the to Change			
13.8-15.8  Sandy Clay, worth Some Shavel  Out 150 Out 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The 6.32.49  The following to be found to form to compare the form to compare the first to some from to compare the first to some from to compare the first to some from to compare the first to some from to compare the first to some from to compare the first to some from to compare the first to some from to compare the first some from the first specific to some from the first some from the first specific to some from		8//	Ĭ,			2-9		7	,,_	1/1	Vocaly	- didains 10 colors			
Sandy Clay, with Some Shavel of 15.8 - 15.8 Sandy Clay, with Some Shavel of 15.8 - 15.8 Sandy Clay, with Some Shavel of 15.8 - 18.8 17.5 Clay, locally gooding to brought (lay, light Gray 2.57 7) but to map fasticity, trajecto some soil, trace to some fine to coarge form of coarge form of soil, and a with a fine to some fine to coarge form of soil, and a with a fine to some fine to subangular observations of the soil of the savel day damp of the soil of the savel day damp of the soil of the savel day damp of the soil of the savel day of the soil of the savel day of the soil of the savel day of the soil of the savel day of the soil of the savel day of the savel day of the soil of the savel day of			131			'		CL	13.0_	0	day ~	dany A/A			
Sandy Clay, with Some Shavel of 15.8 - 15.8 Sandy Clay, with Some Shavel of 15.8 - 15.8 Sandy Clay, with Some Shavel of 15.8 - 18.8 17.5 Clay, locally gooding to brought (lay, light Gray 2.57 7) but to map fasticity, trajecto some soil, trace to some fine to coarge form of coarge form of soil, and a with a fine to some fine to coarge form of soil, and a with a fine to some fine to subangular observations of the soil of the savel day damp of the soil of the savel day damp of the soil of the savel day damp of the soil of the savel day of the soil of the savel day of the soil of the savel day of the soil of the savel day of the soil of the savel day of the savel day of the soil of the savel day of		1	E.	30	1		02	1	L _						
Sandy Clay, wath Some Stavel.  CL 150 day-damp  Tol 6:22.49  Tol 6:2.57  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.57  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:22.49  Tol 6:2.41  Tol 6:2		R	8	77/	603	0-0	07	tera	13.8						
Sandy Clay, with Some Stavel.  CL 150 day-damp  Tol 6:22-49  Tol 6:22-		15.5	\	1					140-		13.8-15.8				
20 16.0 16.0 15.8 - 18.8 17.5 Clay, losely grading to broadly (lay, light brown 2.57 7/2 10.0 16.6 16.6 16.6 16.6 16.6 16.6 16.6		00	1								Cil	Clar wolf Some Clavel			
20 16.0 16.0 16.0 15.8 - 18.8 17.5 Clay, losely goding to boath (lar, light boar 2.57 7/2 10.0 16.6 16.6 16.6 16.6 16.6 16.6 16.6		1	7					رمرا			Jama y				
20 16.0 16.0 15.8 - 18.8 17.5 Clay, losely grading to broadly (lay, light brown 2.57 7/2 10.0 16.6 16.6 16.6 16.6 16.6 16.6 16.6		3	` \(\hat{y}\)					CL	15,0		OAY-	Samp			
8002 16.4 as  15.8 - +8.8 17.5 Clay, loicly goding  1001 16.6 as  1003 16.82 to  1004 to map fishicity, Ingia to some  1005 16.82 to  1006 to map first coange some  1006 sith, Ingia to some firm to coange some  1007 angular to some firm to coange some  1008 angular to some firm to coange some  1009 to map angular to some firm to coange some  1009 to map angular to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to coange some  1009 to some firm to some  1009 to some firm to some  1009 to some firm to some  1009 to some firm to some  1009 to some  1		1	0												
8002 16.4 05  15.8 - +8.8 17.5 Clay, losely goding  1001 16.6 100  1003 16.82 100  1003 16.82 100  1004 10 map fasticity, trajecto some  1005 16.82 100  1006 10 map fasticity, trajecto some  1006 10 map fasticity, trajecto some  1007 10 map fasticity, trajecto some  1008 10 map fasticity, trajecto some  1009 10 map fasticity  1009 10 map fastic		1 N	2						_		,	Tal 4-22-49			
100 16.6 As SCL 100 100 100 100 100 100 100 100 100 10						44			16.0						
1003 16.8280  1003 16.8280  1004 to map pasticity, Inglato some from to coarse food among when with up to coarse food among when with up to coarse food among when the subang when also because of the subang when a so because of the subang when a so because of the subang when a so because of the subang when a so because of the subang when a solid so because of the subang when a solid					16.4	C		AL 22-99			1 /				
10 Silt, trace to some fine to coarse some of the with up to amount at subangular with up to subangular with up to them amount to subangular also because of the subangular of			1~	001	16.6			116	-		.1 /				
17.5-18.3 Claysy Sand Otivo yellow  SC 18.8-19.8 Clayer Sand A/D with  Some gravel, damp		1 6		000	16.82			P	120-		5-Pf +				
10 18.8-19.8 Clayer Sand A/D with Secure Same Sand A/D with Secure Same Sand A/D with Secure Same Sand A/D with Secure Same Sand A/D with Secure Sand Same Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand A/D with Secure Sand Sand Sand Sand Sand Sand Sand Sand		15.6	$\sim$								ansular				
SC SOME Gravel, damp		1				1			-17.4 -	120	4im ans				
SC 17.5-18.8 Clayer Sand; Olive yollow  To light gray 2.5 y 5/6 to 2.5 1N7  18.8-19.8 Clayer Sand A/D with  Sc Some gravel, damp		4	ER	99A	665	0-00	4-x	××	12/2	3/5	Villie &				
10 18.8-19.8 Clayer Sand A/D with.  Sc Some grave damp		1/2	0	. (-1			. ,	!	الال ال	1	17.5-18-8	Claver Sand of in rolling			
18.8-19.8 Clayer Sand A/D with		C. T.	Qu'					ت ر	-		to light	grax 2.5 y 5/6 to 254N7			
18.8-19.8 (Jayer Sand A) with Some Gravel damp		3	$\overline{}$						AA		A/A dr	Υ			
198 198 198 198 198 198 198 198 198 198		1, 2d	0 %						1/1/						
001 200 83		35.03	acol.					30		1	50 mi & 19	1) damp			
			A.	001		R3			F1.8						

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Bore Loca Date Geo	ehole ation e: <u> </u>	Num: Norti	ber: h: <u>74</u> 8-99	BH	967 Eas 3-1 RER	28		ECHNO BUO	:	Y SITE BORE Surface Elevation Area: 903 Total Depth: 2 Company: 2	on: <u>597</u> <i>PAD</i> 20.8 <i>FF</i>	77 <i>F</i>	GE <u>3</u> 01	
RM	RS L		ING S	UPE			Sample Type: _ DATE _	7-6-	99					
TOPBOTTOM OF CORE INBOX	TOP-BOTTOM OF INTERVAL	FEET OF CORE INHITERVAL FIELD MEASUREMENT	SAMPLE NUMBER .	FTACTURE ARGLE	BEUDINS ANGLE	GPAIN SIZE DISTRIBUTION	USCS STMBOL	01 PTH 18	SOIL/ LILIFOLOGIC LCK1		SAMPLE	DESCRIPTION	ИС	. ;
2	198-20.8	AECOVERY;	003 003 002 003	20.4	156 + SUP VOA T 1)	v R	SC	20.0		19.6-20.8 gnavel, d	ŕ		with	
NOTE	S. G		TSO N VOA TSO RS	RUSI II II RINS	000000000000000000000000000000000000000	クラファク	003 002 003 004 005 001	ollows:		Th=20		No. RMRS/		

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Revision 0

(1) Badly broken core, accurate footage measurements not possible.

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Date effective: 12/31/98

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE BOREHOLE LOG  Borehole Number: BH 96898  Surface Elevation: 5978 ff  Location - North: 749095 East: 2085713  Date: 4-12-99 + 4-13-99  Total Depth: 18.8 ff  Geologist: 7. LUTHERER  Drilling Equip.: GEOPROBE DUAL WALL  Sample Type: CONTINUOUS										
RMRS LOGGING SUPERVISOR APPROVAL Mark Wind DATE 7-6-99										
TOP-BOTTOM OF COPE HIBOX	10P/BO110U Of HITERVAL	FEET OF COPE INIMERIAL FIELD	SAMPLE NIMBÉR	FINCTURE ALKREE	BLDDING ANGLE	GIMIN SIZE DISTRIBUTION	USCS SYMBOL	DIPBAIN 1111	SOR/ UDIOROGIC UDIOROGIC	SAMPLE DESCRIPTION
	Run # 3, 6.8-9.8 Run # 2, 3.8-6.8 Run #1, 0.0-38	Recovery 3.5' Recovery: 3.8'	99) 99)	630	77-0 77-0 77-0	4/21/3	SC SC 39	4.7 5.0 6.0 8.2 8.2 8.2 8.2 9.8		2.4 to 3.8; No herover,  3.8-6,8 Sondy (fay / Clayer Sand; pink to redistry plow; 548 7/4 to 578 7/6. fine to rounse subangular Sand moderatory plastic clay, somm up to 4cm angular to subangular Lathic gravel, damp.  6.8-9.8, Clayer Sand, as a boxe.  day, locally grading to Sandy Clay.
NOTES: General: USCS is modified for this log as follows:  Procedure No. RMRS/OPS-PRO.101										

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

Bo Loc Da Ge	rehole	Num - Nort /~/2- t:	ber: h: <u>74</u> 99 -	BH 7 909 → 7	1689 5 Ea 1113 12ER	\$ 20 \$ 20 \$ 9		77.3		Sy SITE BOREHOLE LOG PAGE 1 OF 2 Surface Ejevation: 5978 F+ Area: 103 PAD Total Depth: 18.8 F+ Company: TERRA Project No.:6E6000 ac Sample Type: CONTINUOUS
1	MRS L		ING S		RVISO Mas		w	ad	, 	DATE _ 7-6-99
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL FIELD MEASUREMENT	SAMPLE	FPACTURE ANGLE	BEDDING	GFAIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LITHOLOGIC	SAMPLE DESCRIPTION
	4. 28-12.8'	. 36'		63.	07-	æ3-	KXY	10.0  -/1.0-		9.8-12-8 Clayey Sand Sams 45 above
66/6	8 Run X	Rocavers	001	ł	003	14 L 4/21/	SC 49	121 121 - - - - - - - - - - - - - - - -		12-8-15.8 (layer Sand Same as
6//4	Runt 5 12.8-915.	Recovery 2.0	j				SC.			about.
	Run #6 15.8-18.8	RELOVENT 4.0	99,	RS ISO	TAL 4/4	/49 004-	SC.	-16.0- -17.0- 169 173:		15.8 to 17.3 Clayer Sound Some  95 0 bove  17.3-18.8 (layertone, strong brown  to light gray 75 4R 5/8 to 25 the first side of man top of interval, light high organized men top of interval, light was a dense becoming 55 to layertone 15° (lind, plane Gellopston)
								-188 -19.0		TD= 18.8 Slightly weatherd (D) Si Top of Bedrock = 17.3 Ft

Materials amounts are estimated by % volume instead of % weight.

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(2) Core breaks cannot be matched, accurate foctage measurements not possible.

Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Bo Lo Da Ge	rehole cation te: ologis	Numi - Norti - 4-1-2 t:	ber:	ВН9 90= ЭТН	699 8Eas	8 st: <u>20</u> - 26 FR	985 -99	7//		Y SITE BOREHOLE LOG PAGE CF Surface Elevation: 5978
1		.OGG VAL			RVISC		Vor	d		DATE 7-6-99
10P/BOTTOM OF COFIE H4 BOX	TOP/BOTTOM OF HITERVAL	FEET OF CORE ININGERVAL (FIELD ALASUMEMENT)	SAMPLE NIMABER	FINCTION APAILE	DE ODIEAT AFRELE	GIVINSIZE DISTRIBUTION	USCS SYMBOL	String CITT	SORJ 1 H POLOGIC. 1081	SAMPLE DESCRIPTION  0.0-2.45
	Run #3; 6.8-7.8 Bun #2, 38-6.8 Run #1, 0.0-38	My = 2.7 Recover = 37	99A 99A 001 003	4.4 4.8 682 8.4 3.8	RS iso VOA 4-08	)/X/\$	SC	-1,0- -2.0- -3.0- -3.0- -5.0- -3.0- -3.0- -3.0- -3.0-		See Borehole 109 for  BH91198  2.65 to 3.8  No Recovery  3.8-6.8 Sandy Clay; very Pate how  to yellowist and  very fine to fire, locally undian  to coanse, angular to subangular  softe with some of 9 3.5 angular  to subangular littic gravel.  damp locally graving to Clayer Sand  TOLL 5-2.99  9.8-9.8 Sandy Clay A/A locally  grading to Clayer Sand, day  Procedure No RMRS/OPS-PRO.101

Procedure No. RMRS/OPS-PRO.10

Revision 0

Materials amounts are estimated by % volume instead of % weight.

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Date effective: 12/31/98

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Materials amounts are estimated by % volume instead of % weight.
(1) Badly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

Bo Lo Di Go	oreholocation ate:eologi	e Nun ı - Nor <u>4- 2</u> st:	nber: th: <u>74</u> 7-29-	BH9 903 7 UTH	PLA 8/99/8 8 Eas 4-2: ERE COBE	est: 29 8 - 9 R	985°	REHO		LOG  Surface Elevation: 5978 Ff  Area: 903 PAD  Total Depth: 18.8 FF  Company: TIERRA Project No.: 6E00000  Sample Type: CONTINUOUS
ł	G&G PPRC		GING	_	ERVI Parl		w.	vd		DATE 7-6-99
TOP/BOTTOM OF CORE	TOP/BOTTOM OF	FEET OF CORE IN INTERVAL (FIELD	SAMPLE NUMBER	FRACTURE	BEDDING	GPAIN SIZE DISTRIBUTION	USCS	DEPTH IN	SOIL/ LITHOLOGIC LOG	SAMPLE DESCRIPTION
	Run # 4.90-178	0.5	99 /	122	24-ac RS ISO VOA	93 <i>-</i> XX	x 5c	11.0		9.8-12.8 Sandy Clay, A/A locally Clay with some Sand day
	Run 45, 128-15.8	ROCOVENY 32.					50	-13.0 -14.0 -15.0		12.8-15.8 Sandy Clay, A/A locally glading to Clay with some Sound A/A. day
	1644 Pan 26:13-178	Brail Rover 3.2		682 17.4 17.5 2.6 2.6 2.6 45°	9-004	-	65 60 BR.	-16.0 -17.0 -17.8. -17.4 -18.0 -		15.8-17.4 Sandy flor; A/A locally grading to flay unth, some send A/A day & damp 17.4-17.8 Gravely Fond, very pale brown pred fige to vy fine, some med to coarse angular to boken this grave with so angular to boken this grave with so 17.8-18.8 Cloystong; Oxiding d (weathed) & to 18.2. fight fray to hownish yellow, 25% & not-proper property stiff trace to some south very liable, with twinned, 45° 13°
NOT	ES: Ge	eneral:	USCS	is mod	ified for	this ic	og as fo			The 18.8 Bedrotk = 17.8ft

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Be Lo Di Ge	OCK prehole pcation ate: 3 eologis illing E	Num - Nort - ∠9- t:	ber: 14 h: 74 99—	BH91 8980 -> 4- UTH	7098 9 Ea: 77-9 ER!	{ st: <u>2</u> 9 e_R	085			Y SITE BOREHOLE LOG PAGE / CF 2 Surface Elevation: 5979 f + Area: 903 PAP Total Depth: 18,8 Company: 17 FRRA Project No. 6 E6000 00 Sample Type: CONTINUOUS
1	MRS L				RVISC			Voro	l	DATE 7-7-99
TOP/BOTTOM OF COPE	TOP/BOTTOM OF HATERVAL	FEET OF CORE ININTERVAL (FIELD ALASIAPÉMENT	SAMPLE NUMBER	FILMC TUPIE ALIGI E	BEDDINA	GIVIN SIZE DISTRBUTION	USCS SYMBOL	DI PTA IN	SORJ LILLFOLDGIG. LOXI	SAMPLE DESCRIPTION
NOT	Run # 3 6.8-98 Run # 2:3.8-6.8 Run # 1 . 0.0-38	Recovery 2.9" (RODVING 2.35 #	994	630 32 RS 2 RS 4 130	6308 8-20	2-47	** Sc	-6.0 -6.15 		0.0-3.8 See Bowhole Log of BH 91598  2.7-3.8: No Recovery  3.8-6.8: Sandy Clay, light, hown KRG  Very fine to medium subams was some  Incolly 10218, trace to some part to  4cm angular and body for the gradus  Recovery  6.8-9.8 Send (loy, locally gradus  to Clayer Sand Recovery  10 Clayer Sand Recovery  And 55h yelow Red: 5'78 5/8  A/A dry.  Procedure No. RMRS/OPS-PRO.101
NOTE	ES: Ger Ma						-	ollows:	of % w	n dialog 0 1

Materials amounts are estimated by % volume instead of % weight.

(1) Sadly broken core, accurate footage measurements not possible.

(2) Core breaks cannot be matched, accurate footage measurements not possible.

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Boo Loc Dat Ge	OCKY rehole ation te: 3	Numt North -29- t: Z	per/ n: <u>74</u> 99-	BH 8980 → "	970 e Eas 7-7 RER	98	0850		\$ # T	SITE BOREHOLE LOG PAGE 2 OF 2 Surface Elevation: 5979 ft Area: 903 PAD Total Depth: 18.8 Company: TIERRA Project No.:6E6000 00 Sample Type: 0NT IVVOUS
ł	ARS L 'PRO'		ING S	UPER	iviso Na		a	lond	· 	DATE 7-7-99
TOP/BOTTOM OF CORE IN BOX	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD JEASUPEMENT)	SAMPLE	FRACTURE	BEDDING	GRAIN SIZE DISTRIBUTION	USCS	DEPTH IN FEET	SOIL/ LITHOLOGIC	SAMPLE DESCRIPTION
17	Run & 6: 15.8-18,8 Run & 5: 12.8-15.8 Run # 4: 98-12.8"	RECOURT: 3,7 RECOURT: 3,5" RECOURT: 3,9" ME	7AL 2001 001 001	12.6 VA 12.6 VA 12.6 VA 17.6 VA 17.6	8-06 50 8A	3- >>>	CC	10.0 -11.0 10.0 -11.0 -12.8 -13.0 -15.0 -15.0 -15.0 -15.0 -15.0 -15.0 -15.0 -15.0 -15.0		AB-11.1 [ Say plaster ty, trace to  Some some A/A, trace Sith, Such  Segret A/A: dense, massive, dry of  Segret A/A: dense, massive, dry of  Segret A/A: dense, massive, dry of  Segret Segret Segret Segret Segret  Aug. Cocally gooding to Clayer Segret  12.8-15.8 Sandy Coy A/A  locally gooding to Clayer Segret  Jamp A/A  Clayer Send damp AA  16.8 to 18.8 Broker & Clayer Sandstone  1. Hosay 5/R 1/1, some profishing for 25 +8, 62  Viry poorly mounded, staffer 25 +8, 62  Viry poorly mounded, staffer was for segret such  Subscomplet to regarded, quarigoso, low to  man stastic clay, damp  TC=18.8 ft
NOT	F9. G	eneral:	USC	S is mo	dified fo	or this	log as :	follows:		Procedure No. RMRS/OPS-PRO.101

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible.

NOTES: General: USCS is modified for this log as follows:

COLLABORATE STORMAND AND STORMAND COLLABORATION

Bo Loc Da Ge	rehole cation te: <u>/</u>	Num - Nom - /4 t:	iber: _ th: 24 -98-	BH 1891 7 THL	97/ 1/ Ea: 1-9- EREK	98 st; Z 99	085	REHO	:	Surface Elevation: 5980 F4  Area: 903 PAD  Total Depth: 26.5 F4.  Company: TIERRA Project No.: 6E6000 00  Sample Type: CONTINUOUS
ı	&G I		SING	M	ERVI	SOR	/~	1		DATE 7-7-99
TOP/BOTTOM OF COPE IN BOX	9 -	FEET OF CORE IN INTERVAL	8 AMPLE NI MBER	FRACTURE	BEDDING	GRAIN SIZE DISTRIBLITION	USCS	DEPTH IN FEET	SOIL/ LITHOLOGIC LOG	SAMPLE DESCRIPTION
	6.5 * Pun # 1,00-3,8'	Mocovery 23	004 005	.R3 T50				-1.0- -2.0- -3.0- -3.8 4.0 -42 -44		0.0-3.8 See Bore holo log for BH 92098  2.3-3.8 No Recovery  3.8-6.5 Clayer Sand; Yollowish red torrellow 5YR 5/6 to 2.57,7/4, fine
	30 Bun \$ 2,38-6	BROOVEY: 2	601	NOA A 4 RS	102.	802	5C ***	-6.0 -7.0		Sand from sular to so browned of little sand from to low plastic clay damp
	Punt 4 Runt 3 6,5-9	Re. 32 Rovery: 34	994		7.6 7.6 2.00	72 ×	<i>ن</i> د	-8,0 - 9,0		HOFFSET STARTED ON 12-15-98.
NOTE	M	aterials	amou	nts are		ted by '	% volu	ollows: me instead easurement		eight. OFIGUAL BOREHOLE ENTOVOYEE

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(2) Core breaks cannot be matched, accurate footage measurements not possible.

							ВС	REHO	DLE	
	Soreho				1971		000	= 7.70		Surface Elevation: 5980 FF
	ocalioi ate: _	12-12	nn; <u>7.</u> 7-98	707	<u> </u>	151. <u>2</u> 7-99	08:	5411		Area: <u>903 PAD</u> Total Depth: 26,5 f+
G	eologi	st:	7.1	UTH	ERE					Company: TIERRA Project No.: 6E/00000
	rilling	Equip	: 66	EOPA	POBE		<u>VA C</u>	WALL		Sample Type:
1				SUF	PERV	ISOA	1			
A	PPRO	DVAL			ask		No	vd (	<del></del>	DATE
O'TOM O'RE	OX TOM	280 280 280 280 280 280 280 280 280 280	EMENT PLE	1GRE	2 y	1817E	CS	3 5	SOIL/ LITHOLOGIC	
TOP/BOTTO OF CORE	TOP/BOTTC TOP/BOTTC	N OF E	BAN	FRACTURE ANGLE	A EE	GPAIN SIZE DISTRIBUTION	USCS	DEPTH FEET	80 101110	SAMPLE DESCRIPTION
-	*	1	7	1 1	AVALT	TR.		10,0	16///	9.0-11.5 Payor Sand, damp
	2	1 ^						-		
	14/	^					150	11/1	4//	
	20	2	2					7.0		
	1	7,	17-	7-99	+		111	<del> -</del> -	<b>1</b>	11,5-14.0
	7	"	006	RS	1007		6/4	20	6 6	115-120 Sandy Grove . Sand A/A wear Sal
	1		09/	750	1008			-122		Grave A/A. day broved: Quantyoso
	6 //	00	098	VER	009			12.8		12.0-14.0 Clayer Sand: Brown 7,5 YR 6/3
	1	M	•					13.0		dangs
Ì	#	. ,					50			, j
	A.	Sold Sold	99.	1410.	2 00	2 X	×χ			
	XL		7		7-99			14.0		14.0-165 Clayer Sand; A/A
	1/2/	,	069	`				├ -		14.0 16) Chapty said 1911
	14.0	N.	010					150		Jouands bottom of interval.
	6	, ,,	200	R3 376	010		51	13.3		
	TE	んな	911	410	011			75,4		15.6-16-5 Clay; prontisk gray to reddish
	1	7.40	de	YOA	012		<u> </u>	_// /2_}		40/10W 754R6/2 /2 757R 6/6 Dense
	5	da				ľ	CL	16.0		Staddly Nasta Trace Fond, touce marel.
-	*							- +		16.5-17.8 Clay with sand, A/A
	19	7						-17.0-		16.5-17.8 Clay with sand, A/A
	2.5	W.	`				CL			damy
	7		İ				5	7/1/99		
	4	7				T		-180-		128-190 Clayer Sand: A/A
	4	70,					56.			dans
	Ch.	Rich					) -		6	
	M 1-					-+		19.0		19.0-215 Clayer Sand A/A
	4.5	2			-		50		8	damp damp
	190	₹0 \$\v				_			2	an any

Materials amounts are estimated by % volume instead of % weight.

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- (2) Core breaks cannot be matched, accurate footage measurements not possible.

Boo Loc Dat Ge	POCKY rehole cation te:/ cologis: Iling E	Num! - Nort! 2 - <u>/4</u> t:	ber: h: <u>74</u> - 99,	13H 189 12ER	97/9 11 Eas 1-7- ER	38				SITE BOREHOLE LOG PAGE 3 OF 3  Surface Elevation: 5980 ff  Area: 203 PAD  Sotal Depth: 265 ff  Company: 1 FRRA Project No. 6 6 600000  Sample Type: Cantimuoms
RN	MRS L	.OGG	ING S	UPE	RVISC	OR:	- h	- Sovo		DATE 7-7-99
TOP BOTTOM OF COPE IN BOX	TOP-BOTTOM OF INTERVAL	FEET OF COPE INITERVAL FEELD FEASUREMENT	SAMPLE NUMBER	FIMCTORIE ARSEE	BE DIDTERS APRILE	GIWINSIZ. DISTRIBUTION	175C.S STMBOL	SI P. F. F. F. F. F. F. F. F. F. F. F. F. F.	SOR/ LITHOLOGIC LONE	SAMPLE DESCRIPTION
401 30	Run # 10 Run # 9 Run #8 100	RECOVERY GO RECOVERY REDVERY 2,2 REDVERY 2,5 MEAS	17 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	KS ISO VOA	013	HD ISIG	20.2 20.5 3C 3C 24.2 24.4 24.8	21,0 21,0 22,0		Clayer Sand A/A maist  24.0-26.5 Sandstone: white to list  gray also very pule frown to dans  yellow frown. 2.5 y N8/ 2.5 y N8/  10 y R 7/3 to 10 y R 4/1, locally very Soil  very fine to firm, subsounded, primails  973, locally very clayer, locally graving  10 Sitty llar star uf Sand, frighte, poorly  inducated, oxidized, locally deast.  dampe  Bedireck et 24.0 ft  TD = 26.5 ft
				·		-				

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

В	ROCH orehole ocation	Num	ber: _	BH	972	18		REHC		LOG PAGE LOF Z  Surface Elevation: 5974 Ft  Area: 103 PAN LIP Area
G	ate: leologis rilling E	5 - 2 st:	26-9 - Lu	79 - 1746	7 G RER	-3~	99	- WALC		Total Depth:/8,5FF Company:
	G&G PPRC						Noc	d		DATE _7-6-99
TOP:BOTTOM UP COFE	TOP/BOTTOM OF OF	FEET OF CORE ININTERVAL (FIELD	SAMPLE NUMBER	FIVACTUME ARRIE	AND CONTROL	GIMIN SIZE DISTRIBITION	USCS	DEPTH IN	\$017 111101.0GIC 10G	SAMPLE DESCRIPTION
(O)	36.8-88 Run # 2 3.8-6.8% Run # 1. 0.0-38	Reguest 2.7 IN Ro	-	4.5	WOA O	02 03 01 21 ×	SC	- 1		0.0-2.65 Gravelly Sand; very dark  gray 57R 3/1 to 5, remaining of interval, is reddish brown to dark  reddish brown, 57R 4/3 to 57R  2.5/2 Fine to coarse, sufamosfur to Subnounded, little, fine to a  4 cm subnounded to broken  little gravel, some silt tolay, days.  3.8-6.5 Gravelly, Sand; uddish  lower to dark reddish brown,  A/A  65-8.8 Cloyer Sand, light red  107R 6/8 to reddish gray fore 6/1,  with a light redges brown 25
	Bunt 3	Racen	RS ISO VOA	8.4	001 602 003		50	8- 	2	olo, fine to course, subjuspely to subjounde mp, to 4.4 cm answay to fither swell, low plasticity, some Gilt, damp
	Runk 4 8.8-11.0	Ricoupy:		<i>y</i>				-9- 		8.8-11.0 (loyer Sound P/A

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	Bor Loc Dat Geo	ehole ation e:	Numb North	oer. n: <u>748</u> 6-99	BH9 384 74E)	727 4Eas	t: <u>20</u>		730	S A T	SITE BOREHOLE LOG  urface Elevation: 5974 Ft  rea: 903 PAD Cip Area  otal Depth: 18.5 Ft  company: TIERRA Project No.:65600000  ample Type: CONTINIOUS
		IRS L		ING S	UPER	RVISC	Doo	2			DATE 7-6-99
	TOP/BOTTOM OF CORE IN BOX	TOP/80TTOM OF INTERVAL	FEET OF CORE ININTERVAL (FIELD AEASUREMENT)	STAPLE NUMBER	FRACTURE ANGLE	ANGRE ANGRE	Grain SIZE DISTRIBLITION	USCS	DEPTHIN	\$01U 1111101 0GIC 10G	SAMPLE DESCRIPTION
***************************************		1.35 Pun \$ 4	VO RICOVAY:			Nº.		SC	10.0	ø// ø//	USEN SOLIN POINT TO BREAK THRONGS OBSTRUCTION
		114-136)	2.7.	RS ISO VOA	12-2 12-4 12-8	001 002 003		50	 120		DSEN GOLD POWT TO BREAK TUROUS OBSTRUCTION  2 11.0 - INTERNAL WAS NOT SAMPLED  11.4-13.6 Clayer Samd A/A
0.9/-	- 1	5 RW#6	Rocovu	99A		500	λ\	<i>y</i>	-13.6 -	8	13.6-15.5 (Payor Sand A/A, not
15. 15. 15. 15. 15. 15. 15. 15. 15. 15.		9WX7136-15	Provery 13					SC	14.0 15.0	0/6	@ 13.8
4/4		N 8 A	1, 2, 1	RS ISO	16.2 16.4	00i 00]		50	16.0		15.5-160; Clayer Sand A/A, Jamp to 16.0-17.0; Clayer Sand A/A, Jamp to wet
		10 Kunx 8,5 (60-1	1	VOA VOA	17.0	9682 003 002	5 004	SC SC	-/7.0-		17.0-17.8 Clayer Sound A/A; wet
		Runt	Ruc. le	T50 R5	17.9 18.1 18.3	003 001	<u> </u>	BAN	8.0		17.8-18.5 Silty (laystone slightly weathers mostly light gray 2.5 TRN7/, some browning to your 10 1R 6/6, very poorly indusated locally dans 0, massive, stiff-damp
	·			790	7682	5 00	7 X		-19.0-		Top of Bedruck= 17.8Ft  TD = 18.5 ft
				1156	<u></u>	4:504	inc this	log as	follows:	<u></u>	Procedure No. RMRS/OPS-PRO.101

Materials amounts are estimated by % volume instead of % weight.

(1) Badly broken core, accurate footage measurements not possible. (2) Core breaks cannot be matched, accurate footage measurements not possible. Revision 0

Date effective: 12/31/98

Borehole Number	BH97398 48827 East: 201 UTHERER	36096 A	SITE BOREHOLE LOG FAGE _ CF_I Surface Elevation: 5956 FH Area: 903 PAPLIP Area  Total Depth: 9.0  Company: TIERRA = Folect No. GE6000 OC  Cample Type: CONTINUOUS
RMRS LOGGING	SUPERVISOR MAKE W	boo	DATE 7-2-99
UP BOITOM UP COLE UP COLE UP COLE UP COLE UP COLE UP FEEL OF COPE FEEL OF COPE FEEL OF SAMPLE SAMPLE	BOTTLE WALLE ON DEFENDING HOLD STREET	1975 1111 (01711 m 1111 \$604/ 1111	SAMPLE DESCRIPTION
3 0 002 5 1 003	RS 001 ( RS 001 RS 001 ISO 002	2.0	0.0-2.0 (layor Sitt, very danh snay) 2.5 7 N 3/, dense, moderate plasticing traces fine to coarse, angela to sout- angular, littic sound, traces fine to coarse, become and grasular littic gravel with organic matter, wet - moist, 2.0-3.4 (layer Sand, light redoish brown 57R 6/3, components as above damp.
992 615	5-001 001 (002) 002 001 (002) 003 001 (002) 004 00! (002)	-5.0 -5.0 -7.0 -7.0	Proceedure No. RMRS/OPS-PRO.101

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Bo Lo Da Go	oreho ocation ate: <u>/</u> eologi	ie Nur n - No 5- /4 ist:	nher	13/1 1877	97 10 Es	4 98 ist: <u>Z</u> ER	086	TECHNO 182 — U. WAL		Y SITE BOREHOLE LOG PAGE OF Surface Elevation: 5947 Ft.  Area: 903 PAD Lip Acea Total Depth: 4,0 Company: TIERRA Project No. GE6000 Sample Type: CONTINUOUS
		LOGO	GING	SUPE	RVIS	OR				CATE
Of COPE	10P/BO110M OF	FEET OF CORE IN HATERVAL	AL ASIMEREMENTS AND AND AND AND AND AND AND AND AND AND	AVALIE VIENE	POTILE	GIVINSIA DISTUBITION	USCS	1111 1111	SOM) 1111#34 OLAR 1184	SAMPLE DESCRIPTION
Bas 105 1, 0.0-1.8'	Run # 1,00.40	ADD ROCKEY: 18'	001	RS TXV RS TXO RS TXO RS TXO 002 003	002 001 002 001 002 002 001	2 x (002)	SC	-30 -40 -5.0 -2.0		0.0-1.3 (layer sitt; dark reddish from 57R 4/3 degree, mod. plasticity, traces for to coarse, any in to subangular littles traces from to coarse, broken and against little gravel, with organic mother, we mais.  1.3-1.8 /layer Sand wodish broken.  57R 5/3, companieds &s above, dans.
								3.0		

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Boreh Locati Date: Geolo	KY FI lole Nu lon - No 6-/- gist: g Equip	mber: grth: <u>24</u> 7 - 99 7 - L	1384 1884 UTH	975 45 Ea	98 st: <b>20</b> ER	186			Y SITE BOR Surface Eleval Area: <u>703</u> Total Depth: _ Company: <u>1</u> Sample Type:	ion: <u>595</u> PAPL, 4,0 TERRA	Ares		of_L
1	S LOG			RVIS		) <del>00 c</del>	<u>L</u>		DATE	7-2	-99		
TOP/BOTTOM OF CORE IN BOX TOP/BOTTOM	INTERVAL FEET OF CORE	MEASUREMENT	FINCTURE	BEDDING ANGLE	GIWIN SIZE DISTRIBLITION	USCS SYMBOI	DEPTH IN	SOIL/ LITHOLOGIC LOGS		SAMPL	E DESCRIP	TION	
Bay 1051, a0-27,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00   00 2   00 3   00 4   00 5   00 6   37	R S 150 R S 150 R S 150 R S 150 R S 150 R S 150 R S 150 R S 150 R S 50 R	00) 002 001 002 001 002 001 002 001 001	002) (002) (002) (002)	ES	-1,0- -2.0- -3.0- -4.0 -5.0- -7.0- -8.0- -9.0-		0.0+2-7 10R 2-5/ tiacos (5) angula coarse	e letter	ense go Sand,	ngolar Tageos Jula	to sul time su

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Procedure No. RMRS/OPS-PRO.101

Revision 0

Date effective: 12/31/98

Boo Loc Dat Ge	OCKY rehole cation te:	Numi - Norti - 18	ber: h: <i>74</i> - 99	BH 9 1913 <del></del>	767 5 Eas 6-2 6k	98 st: <u>Z4</u> 3-99	85		· · · · · · · · · · · · · · · · · · ·	SITE BOREHOLE LOG PAGE 1 OF 3  Surface Elevation: 5976 FF  Area: 903 PAD  Total Depth: 743 PADIAC 2949  Company: 1ERRA Project No Elevator  Sample Type: Courinvous
	ARS L			SUPE	RVISO Ma	OR	W	lad		DATE 7-6-99
TOP BOTTOM OF CORE INBOX	TOPBOITOM OF INTERVAL	FEET OF CONE INHITENVAL (FIELD) MEASIMEMENT)	SAMPLE NUMBER	FRACTURE ARGLE	BLODIES APRÍSE	GIMIN SIA DISTRIBUTION	11SC.S SYMBOL	DEFTRIN	SOR/ UTHOLOGIC UNI	SAMPLE DESCRIPTION
	Run #2: 3.8-6.8 Run #1, 20-3.8	Recovery: 3.9' Recovery: 2.5'	006	VOA	001 003 003 002 002	DUP.	ŞC	3.8 - 3.0 - 3.0 - 3.0 - 5.0 - 5.0		3.8-6.8 Clayor Sand yelowish BH 90998  Brown, 1078 514, very fine to coarse, angular to subungular lithic sand, non plastic clay, silty, locally abundant up to 35 cm, brown to subangular lithic sand, abundant up to 35 cm, brown to subangular lithic snavel, day-boatly clamp.
	Run #3 6.8-58		βοπι Νο. 00; 003 002	RS 8. VOA ISO 8.	6 8 0022		<i>SC SC SC</i>	-7,0 -8,0 - -9,0 - 		40.9.2 Sand, Gavel, color and composers, 9.2-9.8 Clayer Sand A/A Jany.  Procedure No. RMRS/OPS-PRO. 101

Materials amounts are estimated by % volume instead of % weight.

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(2) Core breaks cannot be matched, accurate footage measurements not possible.

Revision 0

Date effective: 12/31/98

Boo Lox Da Ge	rehole cation te: ologis	Num - Nort	ber: h: 74 /8 - 9	BH9 9135	Ear RER	8 st: 20	2858	ECHNO	:	Y SITE BOREHOLE LOG  Surface Elevation: 5976 ff  Area: 903 PAD  Total Depth: 228  Company: 71ERRA Project No.:6E600000  Sample Type: 0NTIWOUS
1	ARS L		ING S	SUPER Man	,		1	/		DATE 7-6-99
TOP/BOTTOM OF CORE	TOP/BOTTOM OF INTERVAL	FEET OF CORE IN INTERVAL (FIELD	SAMPLE NUMBER	ANGLE ANGLE	BEDDING	GPAIN SIZE DISTRIBLITION	USCS	DEPTH IN	SOIL/ LITHOLOGIC	SAMPLE DESCRIPTION
	14.8 42 12.8 4	Reover 5.	991 13 002 003	11.0 RS 11.2 VO 11.8 I: 11.8 I: 12. RS 14. 1 15.0 14. 1	A 10		54	10.0 11.0 11.0 12.0 13.0 14.0		9.8-11.9 foundy (lay, A/A W/ focally abundant gravel, at times locally grading to Sandy onavel A/A damp damp  11.9-12.8 (layer Sand, Briddish Browns, found for subnounded, lothic sand damp to maist.  12.8-14.8 (layer Sand, pole yellow to olive yellow 2.547/4 to 2.58 6/8 fine to coarse sand, Suban gula, tonous lather and calific grains, trace from and lather gravel, low plasticity, locally
	-18.8 Run & 6.8'	x 3.25 Decorar 2.65	991 003 002	1827 15.9 16.1 16.3 16.7	005	**		15.0 -16.0 -17.0		Silty damps 14.8-16-8 Clayer Sand, A/A, locally with abundant gravel, damp with  16.8-18.8 Clayer Sand with some to abundant gravel. A/A
	Run & Shin #	Recovery 2.4	991 991 901 003	18.0 18.2 18.8 18.8 19.8 19.9 19.8	7 00-		SC	1810 188 -17.0	0000	brown in YR 5/6 and durk yellowish brown damp  18.8-20.8 Clayor Sand A/A  Procedure No. RMRS/OPS-PRO.101

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Revision 0

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Date effective: 12/31/98

Boo Loc Dat Ge	rehole cation te: ologis	Numt	per: 1: <u>74</u> 2 - 99	BH9 913:	76 East	9 8 st: <u>20</u> 9 3 - 9	985) 9	880	\$ A	Y SITE BOREHOLE LOG PAGE 3 OF 3  Surface Elevation: 5976 Ff:  Area: 903 PAD  Total Depth: 228  Company: TIERRA Project No. 6 F 6000 00  Sample Type: CONTINUOUS
RN AP	ARS L	.OGG VAL	ING S	UPER	evisc en E	OR W	loc	l .		DATE 7-6-99
TOP:BOTTOM OF CORE IN BUX	TOP-BOTTOM OF INTERVAL	FEET OF COPE INIMERAL (FIELD MLASUREMENT)	SAMPLE NUMBER	FEWCTVIRE - ANGLE	BEDDIFES ANGE	GRAIN SIZE DISTRIBUTION	USCS SYMBOL	01 61H IN	SOIL/ LIVIOLOGIC LOXI	SAMPLE DESCRIPTION
	Report S	Ricovery 2.4					SC	20.0		
	Run × 9	Recovery:					SC	12.0		20.8-22.8 (loger Sand A/A) with locally abundant gravel 20.8-21.1 Saturated, otherwise damp
	-	Ri PõA	nsa 827	100	7 00	21 R	SA DA	23.0 		TP= 22.8
			100		00	4 V	SO		Autoritania de la companya del la companya de la co	
					,					
								follows:		Procedure No. RMRS/OPS-PRO.101

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Characterization Report for the	Document Number:	RF/RMRS-99-427.UN
903 Drum Storage Area,	Revision:	0
903 Lip Area, and Americium Zone	Date:	September 28, 1999
	Page:	B-1

### Appendix B

Precision (DER and RPD) Calculations

# Surface Soil Charcterization Precision Resuts HPGe Survey - Americium-241

DER		0.2124		0.0798	Price community for the Magnetic and many for	0.1286	a delinica en l'acce commendentes	The programmer of the characteristic for the comment	N. Wall a discretion PW to discrete A A Africance S (1995).	0.0397	The state of the s	0.0772	Control of the second control of the second	0.1042	and the second s	0.0268	THE THEOLOGY WAS LAMBORATED A VICTOR AND A TO BE VALLED.	0.0965	and substitution for any and successful and any of professional and	0.0240	Office and County of the Count	0.0151	The second secon	0.0326	100 - Ann and married Ody Springer on Advancer was a second	0.0098	The same of the sa	0.2240	entrain 10 material authorities and tombound the control	0.0076	and a constraint of the contract of the contra	0.0850	A THE PROPERTY OF THE PROPERTY	0.0856
TPE	2.549	2.2123	5.0238	5.3329	6.306	6.9159	0	0	13.65	13.272	12.9	8.0445	16.186	14.842	7.3941	7.5902	15.873	14.724	7.8517	7.7575	6.7068	6.7023	8.7316	8.8974	10.678	18.774	10.143	8.3195	5.7712	5.753	5.9036	5.4386	6.1004	5.8097
MDA	1.1669	1.0471	1.3254	1.3118	1.5454	1.4108	0.87883	0.85795	1.6698	1.8841	1.9062	1.9814	2.4216	2.1482	1.5532	1.6708	2.5172	2.1576	1.8399	1.9362	1.5574	1.737	2.2537	2.1187	1.5395	1.6862	1.8151	1.3885	1.3913	1.3877	1.8115	1.5745	1.1197	1.4074
Counting Error	1.4611	1.3394	2.5898	2.7235	3.1812	3.43	0	0	6.5632	6.4112	9.2351	4.0278	7.9047	7.2465	3.651	3.762	7.5668	7.0445	3.9436	3.9288	3.3664	3.4046	4.4282	4.4725	5.1655	13.326	4.9867	4.0446	2.9194	2.8826	3.0676	2.8074	2.9936	2.9191
Qualifer		eg en estados compos do estados de estados d	THE PERSON NAMED AND PARTY OF THE PE			190 - 190 -	<b>5</b>	<b>)</b>			_			W 1 - 14440-17 V N 4004-17 V V				Yannahan and year owner and				The state of the s												100 cm 10
Result   Unit	3.6265 pCi/g	2.9097 pCi/g	8.1133 pCi/g	8.6981 pCi/g	10.416 pCi/g	11.62 pCi/g	0.87883 pCi/g	0.85795 pCi/g	23.623 pCi/g	22.868 pCi/g	12.216 pCi/g	13.389 pCi/g	27.605 pCi/g	25.317 pCi/g	12.477 pCi/g	12.761 pCi/g	27.687 pCi/g	25.597 pCi/g	13.027 pCi/g	12.762 pCi/g	11.135 pCi/g	10.992 pCi/g	14.344 pCi/g	14.75 pCi/g	18.374 pCi/g	18.162 pCi/g	17.188 pCi/g	14.25 pCi/g	9.5058 pCi/g	9.5679 pCi/g	9.4532 pCi/g	8.7707 pCi/g	10.356 pCi/g	9.6353 pCi/g
sotope	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241
Result Identifer	REAL	RP	REAL	伀	REAL	RP	REAL	쮼		RP		RP	REAL	RP	REAL	RP	REAL	RP		RP	REAL	8	REAL			RP	REAL	RP	REAL	格	REAL	RP	REAL	쮼
Easting	2086712.625 REAI	The state of the s	2086940.341 REAL	V at a second control of the second control	2086923.395		2086547.392 REAL		2086501.735		2086788.193	S. A. A. S. S. S. S. S. S. S. S. S. S. S. S. S.	2086525.162		2086456.248		2086475.732		2086617.93	Control of the Contro	2086637.588		2086327.974		2086348.428		2087177.737		2087156.342	American State Comment of the Commen	2087306.954		2087288.334 REAL	
Northing	749504.228	The state of the s	749488.57		749457.057		749274.78		748741.807		748758.403		748762.927		748686.658		748712.728		748543.498		748569.785		748530.596		748553.614		749282.129		749308.922		749360.365		749384.141	
Measurement Location	₹	9,000	34		20		70		102		92		103		144		143		188		187		224		223	A STATE OF THE STA	293		292		328		327	
Measurment     Set	1		2		က	-	4		Ŋ		9		7		ω		<u></u> ත		10	to the second state of the	7		12	F	<u>~</u>		41	100000000000000000000000000000000000000	5		16		17	

# Surface Soil Charcterization Precision Resuts HPGe Survey - Americium-241

TPE DER	4.1153	4.1107 0.0428	4.9784	5.4418 0.1160	9.9739	9.7264 0.0405	4.466	4.1875 0.0827	Elling av 1. 1912 — 20000 III. I Labbidgerden Anberger (Bernetterner) es o.c.o.o.o.	13.1 a.g. Valada (1917) Program (1918) Little-regarder even eventure regarder (1918) Little-regarder eventure eventure regarder (1918) Little-regarder eventure eventure regarder (1918) Little-regarder eventure	2.8954	2.8385 0.0483	93.346 mills bench handle bench hand benchmann and graphy and the stress has a construction of the stress hand benchmann and graphy and the stress hand benchmann and graphy and	10.713 0.1841	7.9431	8.6259 0.1096	8.185	5.6322 0.4466	7,7467	8 008		PROPERTY OF THE CONTROL OF THE CONTR	ene seminolemano (GLES) (G).	A STATE OF THE STA	TOTAL CONTROL OF THE STATE OF T			
MDA	1.7649	1.5527	1.1926	1.2176	1.4883	1.7304	1.5166	1.4983	1.1475	1.1779	1.0916	1.1654	2.3354	2.1778	1.8642	1.8275	1.6359	1.2918	1.5516	1 7761	->	1	1			diameter 1		
Counting er Error	2.3238	2.2445	2.4629	2.6696	4.8726	4.7944	2.3826	2.2561	0	0	1.5688	1.5708	4.7461	5.3281	4.0085	4.3058	3.9786	2.7567	3.8208	3.9737		3.0181	3.0181	3.0181 2.6872 5.1869	3.0181 2.6872 5.1869 5.1799	3.0181 2.6872 5.1869 5.1799 4.756	3.0181 2.6872 5.1869 5.1799 4.756 4.8554	3.0181 2.6872 5.1869 5.1799 4.756 4.8554 5.436
Result Unit Qualifer	5.9716 pCi/g	6.2208 pCi/g	8.385 pCi/g	9.2405 pCi/g	17.004 pci/g	16.44 pCi/g	6.9447 pCi/g	6.4381 pCi/g	1.1475 pCi/g U	1.1779 pCi/g U	4.4217 pCi/g	4.2258 pCi/g	15.333 pCi/g	17.951 pCi/g	13.115 pCi/g	14.4 pCi/g	14.022 pCi/g	9.585 pCi/g	13.086 pCi/g	13.441 pCi/g		8.2579 pCi/g	8.2579 pCi/g 7.4445 pCi/g	8.2579 pCi/g 7.4445 pCi/g 18.093 pCi/g	8.2579 pCi/g 7.4445 pCi/g 18.093 pCi/g 18.444 pCi/g	8.2579 pCl/g 7.4445 pCl/g 18.093 pCl/g 18.44 pCl/g 14.247 pCl/g	8.2579 pCl/g 7.4445 pCl/g 18.093 pCl/g 18.444 pCl/g 14.247 pCl/g 15.912 pCl/g	8.2579 pCl/g 7.4445 pCl/g 18.093 pCl/g 18.444 pCl/g 14.247 pCl/g 15.912 pCl/g 18.874 pCl/g
r Isotope	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	V 24.4	1 47-1114	Am-241	Am-241 Am-241 Am-241	Am-241 Am-241 Am-241	Am-241 Am-241 Am-241 Am-241	Am-241 Am-241 Am-241 Am-241	Am-241 Am-241 Am-241 Am-241 Am-241 Am-241
Result   Res	3.89 2087225.351 REAL	The second secon	2087259.129	RP	254 2087288.321 REAL	RP	725 2087268.341 REAL	AP.	144 2086857.564 REAL	RP	2.52 2086871.874 REAL	RP	781 2086645.557 REAL	<b>4</b>	751 2086627.577 REAL	AP.	455 2087170.102 REAL		819 2087136.494 REAL	Co. D. C. Waller and C. C. C. C. C. C. C. C. C. C. C. C. C.	728 2086730.163 REAL	Committee of the commit		2086716.347	2086716.347	8 8	2086716.347	2086716.347 2086803.595 2086813.193
Measurement Location Northing	347 749466.89	di di banana di dana di dana di dana di dana di dana di dana di dana di dana di dana di dana di dana di dana di	348 749473.379		392 749237.254		391 749265.725		424 749122.144		423 749152,52		466 749030.781		465 749061.751		491 749106.455		493 749103.819	- 1	534 748827.728			533 748861.115				
Measurment   Mea	18	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	19		20		21	100000000000000000000000000000000000000	22		23		24		22	Anna Mara (d. 18.) one of Marada Anna and Anna and Control of the	26		27	employee group of the section of the	28		The second secon	29	29	299	300	30 (1997)

# Surface Soil Charcterization Precision Resuts HPGe Survey - Americium-241

DER	A COMMISSION OF THE PROPERTY O	0.0728		0.0590		0.0147		0.1099	The state of the s	0.2336		0.0188		0.1059	And the second of the second o	0.1824		0.0335		0.0862		0.0330		0.2077		0.0332		0.1896		0.0055
TPE	19.486	18.457	12.101	11.613	10.584	10.49	2.3966	1.9957	3.2106	2.467	4.8422	4.9176	4.6661	4.951	3.3922	2.97	5.0392	4.8791	5.134	4.8365	13.248	13.426	3.9318	3.118	3.6322	3.7581	5.6174	6.6487	4.2731	4 1987
MDA	1.583	2.0883	2.1069	2.4666	1.6981	1.8335	1.6254	1.3121	1.51	1.0788	1.1885	1.2336	1.7624	1.624	1.1309	1.1273	1.6674	1.6321	1.1477	1.2636	1.9225	1.6238	1.526	1.029	1.4006	1.4691	1.6295	2.0171	1.4023	1 2010
Counting Error	9.2692	8.8266	5.8026	5.611	5.2004	5.173	1.6399	1.3419	1.8583	1.3985	2.4323	2.4687	2.526	2.5948	1.7862	1.6108	2.6069	2.5173	2.5766	2.4615	6.3291	6.3199	2.1689	1.6679	1.9885	2.0624	2.89	3.4262	2.2551	2 4006
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Unit	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g		pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	5.4789 pCi/g	5.6524 pCi/g	bCi/g	10.742 pCi/g	6.7266 pCi/g	
Result	34.057	32.102	20.996	20.006	17.944	17.725	2.5224	2.1795	4.5077	3.5617	8.0332	8.1629	7.1336	7.8541	5.3532	4.531	8.1076 pCi/g	7.8726	8.5245	7.9166 pCi/g	23.062 pCi/g	23.685	5.8762	4.8337	5.4789	5.6524	9.0916 pCi/g	10.742	6.7266	
Isotope	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	Am-241	acceleration death and a thinking
Result Identifer	REAL	RP	REAL	RP P	REAL	RP	REAL	RP	REAL	RP	REAL	RP	REAL	짠	REAL	RP	REAL	RP	REAL	R	REAL	8	REAL	뫈	REAL	格	REAL	윰	REAL	The second flowers of the second second
Easting	2086641.506 REA	the side (C) is the demonstrate by the continue of the physician	2086833.856 REAL	The state of the s	2086763.165 REAI	in Visit ad Visit and Class Company or constraints and other his	2085991.96 REAI	The state of the s	2086013.852	MAN A VIEW CONTRACTOR OF THE PROPERTY OF THE P	2085849.536 REAI	And the state of t	2085827.994		2086926.887		2086894.845	to consider our representation of the contract	2087188.642	AND THE PARTY OF T	2087208.331	on the state of the second of a transfer of the state of	2086066.366	The second of th	2086097.672	portra for Weingergreen and American and Ame	2087427.728	The control of the co	2087445.174 REAL	The state of the s
Northing	749006.216	The first of the second of the	748997.504	and the same of th	748992.091		748633.56	With the same of t	748662.599	September of Contraction and Contraction of Contrac	748554.388		748528.91	and the comment of a comment of	748550.632		748558.501		749066.896	The second section of the section of the sect	749053.005	The Processing of Annial Manham Control of the Process of the	748467.494	A CONTRACT OF THE CONTRACT OF	748458.181	The first of the f	748829.304		748800.474	Court of City and and City and a second
Measurement Location	587	The service of the se	624	en en en en en en en en en en en en en e	622	The state of the s	999	The state of the s	665	Comment of the commen	705	encountry at the continuency of the order of	902	Wife and Control day, 17.5 challes and immediated to the control of the control o	770	The state of the s	692	The major of the control of the cont	785	The second secon	786	The state of the s	837	A STATE OF CALLEY AND THE COLUMN TO THE COLUMN TO THE CALLEY AND T	836	A contract of the first teacher with the contract of the contr	874	And the Company of the company of th	873	the second contract of the second contract of
Measurment Set	32		33	the second secon	34	and the second s	35	the second secon	36	and the second s	37	and the control of th	38	to the control of the	30	A manAAA T Code Suidebillip py and Cognision of the Process	40	A Comment of the comm	41	The second of th	42	PERSONAL CONTRACTOR CO	43	of particionals. To example the Contains of emballion	44	The second secon	45	a Commence or attack of the delicate of the commence of the co	46	the second from the same detailed in the office and the con-

# Surface Soil Charcterization Precision Resuts HPGe Survey - Americium-241

Location         Northing         Easting         Identifier         Isotope         Result         Unit         Qualifier           47         902         749150.108         2087462.745         REAL         Am-241         1.256 pCl/g         U           48         903         749159.127         2087493.409         REAL         Am-241         1.256 pCl/g         U           49         946         748935.561         2087258.354         REAL         Am-241         4.6188 pCl/g         J           50         965         748836.522         2086172.771         REAL         Am-241         24.748 pCl/g         J           51         986         748836.522         2086172.771         REAL         Am-241         25.012 pCl/g         J           52         1003         748566.447         2085682.743         REAL         Am-241         20.353 pCl/g         J           53         1002         748594.463         2085666.295         REAL         Am-241         1.0946 pCl/g         J           54         1036         748851.904         2087437.883         REAL         Am-241         1.0946 pCl/g         J           55         1069         749181.174         2087419.516         REAL<	Measurment	Measurment Measurement		# 10 m	Result				7,656	Counting			
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946 748935.561 2087258.354 REAL Am-241 3.791 pCi/g 965 748838.416 2086052.179 REAL Am-241 24.748 pCi/g 986 748836.522 2086172.771 REAL Am-241 25.012 pCi/g 1003 748566.447 2085682.743 REAL Am-241 20.353 pCi/g 1002 748594.463 208566.295 REAL Am-241 1.398 pCi/g 11036 74851.904 2087437.883 REAL Am-241 7.2614 pCi/g 11056 749317.343 2087419.516 REAL Am-241 7.6217 pCi/g 11069 749181.174 2087619.571 REAL Am-241 0.9178 pCi/g 1107 749240.763 2086516.094 REAL Am-241 0.9178 pCi/g 1106 749240.763 2086516.094 REAL Am-241 0.9178 pCi/g 1106 749271.949 2086516.094 REAL Am-241 0.9178 pCi/g 1106 749271.949 2086516.094 REAL Am-241 0.9169 pCi/g 1106 749271.949 2086516.094 REAL Am-241 0.9169 pCi/g 1106 749271.949 2086516.094 REAL Am-241 0.9163 pCi/g 1106 749271.949 2086516.17 REAL Am-241 0.8923 pCi/g 1107 749271.949 2086516.17 REAL Am-241 0.8923 pCi/g 1108 PAM-241 0.8923 pCi/g 1109 PAM-241 PAM-241 0.8923 pCi/g 1109 PAM-241 PAM-241 0.89628 pCi/g						Am-241	0.67627 F	Ci/g J	0.	0.70307	0.7365	0.90595	0.2325
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1003 748566.447 2085682.743 REAL Am-241 1.1398 pCi/g BPP Am-241 1.1398 pCi/g J Am-241 1.0946 pCi/g J Am-241 1.0946 pCi/g J Am-241 1.0946 pCi/g J Am-241 1.0946 pCi/g J Am-241 1.0946 pCi/g J Am-241 1.1322 pCi/g J Am-241 1.1322 pCi/g J Am-241 1.1322 pCi/g J Am-241 1.1322 pCi/g J Am-241 1.1322 pCi/g J Am-241 1.1322 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.1405 pCi/g J Am-241 1.0416 pCi/g J Am-241 1.	51			2086172.771		Am-241	20.353 p	Ci/g		5.627	1.6216	11.733	2 TH BO 2 A ROTT COLOUR ON TO THE PROPERTY CONTROL WINDOWS AND LIBERTY COLOUR
1003 748566.447 2085682.743 REAL Am-241 1.1398 pCi/g J 1002 748594.463 2085666.295 REAL Am-241 1.0946 pCi/g J 1036 748851.904 2087437.883 REAL Am-241 7.2614 pCi/g U 1055 749317.343 2087419.516 REAL Am-241 7.4422 pCi/g RP Am-241 7.4405 pCi/g D 1069 749181.174 2087619.571 REAL Am-241 0.9178 pCi/g U 1107 749240.763 2086516.094 REAL Am-241 0.9173 pCi/g U 1106 749271.949 2086516.417 REAL Am-241 0.92887 pCi/g U						Am-241	20.87   ₽	Ci/g		5.7331	1.6008	11.994	0.0308
1002 748594.463 2085666.295 REAL Am-241 1.0946 pCi/g U 1036 748851.904 2087437.883 REAL Am-241 7.2614 pCi/g U 1055 749317.343 2087419.516 REAL Am-241 7.4422 pCi/g RP Am-241 7.4422 pCi/g RP Am-241 7.4422 pCi/g RP Am-241 7.4422 pCi/g U 1069 749181.174 2087619.571 REAL Am-241 0.9178 pCi/g U 1107 749240.763 2086516.094 REAL Am-241 0.9178 pCi/g U 1106 749271.949 2086516.417 REAL Am-241 0.92887 pCi/g U	52		748566.447	2085682.743		Am-241	1.1398 p	)Ci/g		0.9978	1.0314	1.3397	14 mins - 15 th Same access considerable confidences and access con-
1002 748594.463 208566.295 REAL Am-241 1.0946 pCi/g U 1036 748851.904 2087437.883 REAL Am-241 7.2614 pCi/g U 1055 749317.343 2087419.516 REAL Am-241 7.4422 pCi/g U 1069 749181.174 2087619.571 REAL Am-241 0.9178 pCi/g U 1107 749240.763 2086516.094 REAL Am-241 0.9923 pCi/g U 1106 749271.949 2086516.417 REAL Am-241 0.9923 pCi/g U			The second secon	The second secon		Am-241	0.9303 <sub>F</sub>	Ci/g	William Commence of the Commen	1.065	1.1296	1.3441	0.1104
1036 748851.904 2087437.883 REAL Am-241 7.2614 pCi/g U 1055 749317.343 2087419.516 REAL Am-241 7.4422 pCi/g RP Am-241 7.4422 pCi/g RP Am-241 7.4422 pCi/g RP Am-241 7.4405 pCi/g U 1069 749181.174 2087619.571 REAL Am-241 0.9178 pCi/g U 1107 749240.763 2086516.094 REAL Am-241 0.9923 pCi/g U 1106 749271.949 2086516.417 REAL Am-241 0.82887 pCi/g U	53			2085666.295		Am-241	1.0946 p	Ci/g U	A complete and the comp	0	1.0946	0	AND THE PROPERTY OF THE PROPER
1036 748851.904 2087437.883 REAL Am-241 7.2614 pCi/g RP Am-241 7.4422 pCi/g Am-241 7.4422 pCi/g RP Am-241 7.4405 pCi/g RP Am-241 7.4405 pCi/g RP Am-241 7.6217 pCi/g U Am-241 7.6217 pCi/g U Am-241 0.9178 pCi/g U RP Am-241 0.9178 pCi/g U Am-241 0.9178 pCi/g U Am-241 0.9178 pCi/g U Am-241 0.923 pCi/g U Am-241 0.923 pCi/g U Am-241 0.923 pCi/g U Am-241 0.923 pCi/g U Am-241 0.923 pCi/g U Am-241 0.92887 pCi/g U						Am-241	1.1322 p	Ci/g U		0	1.1322	0	TATE OF BRITAIN TOLDS SERVICES AND SERVICES
1055 749317.343 2087419.516 REAL Am-241 7.4422 pCi/g RP Am-241 7.1405 pCi/g RP Am-241 7.6217 pCi/g RP Am-241 7.6217 pCi/g U RP Am-241 0.9178 pCi/g U RP Am-241 0.9178 pCi/g U RP Am-241 0.9178 pCi/g U RP Am-241 0.9153 pCi/g U RP Am-241 0.9923 pCi/g U RP Am-241 0.9923 pCi/g U RP Am-241 0.9923 pCi/g U RP Am-241 0.9923 pCi/g U Am-241 0.82887 pCi/g U	54			2087437.883		Am-241	7.2614 p	Ci/g		2.4047	1.4711	4.5831	
1055 749317.343 2087419.516 REAL Am-241 7.1405 pCi/g RP Am-241 7.6217 pCi/g Colored Am-241 7.6217 pCi/g U Am-241 0.9178 pCi/g U Am-241 0.9178 pCi/g U Am-241 0.9153 pCi/g U Am-241 0.9240.763 2086516.094 REAL Am-241 0.9923 pCi/g U Am-241 1.0416 pCi/g U Am-241 0.82887 pCi/g U	- Line and the second s	Widows and the same of the sam				Am-241	7.4422 F	Ci/g		2.3804	1.3392	4.6131	0.0278
1069 749181.174 2087619.571 REAL Am-241 7.6217 pCi/g U 1107 749240.763 2086516.094 REAL Am-241 0.9923 pCi/g U 1106 749271.949 2086516.417 REAL Am-241 0.82887 pCi/g U	55	According to the Conference of the control of the c		2087419.516		Am-241	7.1405 p	Ci/g	.7	2.3449	1.4828	4.4871	And the committee of the first first and the section of terrorization property and
1069 749181.174 2087619.571 REAL Am-241 0.9178 pci/g U RP Am-241 0.9178 pci/g U Am-241 0.9178 pci/g U Am-241 0.9178 pci/g U Am-241 0.9178 pci/g U Am-241 0.9178 pci/g U Am-241 0.9923 pci/g U Am-241 0.923 pci/g U Am-241 0.82887 pci/g U	-					Am-241	7.6217	Ci/g		2.3994	1.446	4.6859	0.0742
1107 749240.763 2086516.094 REAL Am-241 0.91153 pci/g U RP Am-241 0.9923 pci/g U RP Am-241 1.0416 pci/g U Am-241 0.82887 pci/g U	56	William Co. The Control of the Contr		2087619.571		Am-241	0.9178	Ci/g U	Total Marie Control on the spirit	0	0.9178	0	Accommendation of the filter of the filter control of the filter of the
1107 749240.763 2086516.094 REAL Am-241 0.9923 pCi/g U RP Am-241 1.0416 pCi/g U 1106 749271.949 2086516.417 REAL Am-241 0.82887 pCi/g U	COMMISSION CONTRACTOR STATEMENT OF STATEMENT	The company of the state of the	THE AND A COMMENT OF THE PROPERTY OF THE PROPE	A STATE AND AND AND AND AND AND AND AND AND AND		Am-241	0.91153p	Ci/g U		0	0.91153	0	obtaine d'Argon de comment de la commentación de la commentación de commentaci
1106 749271.949 2086516.417 REAL Am-241 0.82887 pCi/g U	57	and the second s		2086516.094	1	Am-241	0.9923 p	Ci/g U	and the second s	0	0.9923	0	minimum of a contraction of a decided to the contraction of the contra
1106 749271.949 2086516.417 REAL   Am-241   0.82887 pCi/g   U						Am-241	1.0416 p	Ci/g U		0	1.0416	0	ekallis kirri sippiga san ya kiii chidasha ana da mis ay umasa
	58	ann an ann an Aidea (A' The Bill T' - 1960 o prosence		2086516.417		Am-241	0.82887 F	Ci/g U			0.82887	0	The second secon
RP   Am-241   0.52757   DCi/g   J						Am-241	0.52757 F	Ci/g   J		1.1216	1.2218	1.2798	0.2354

### Sufrace Soil Characterization Precison Results Gamma Spectroscopy - Americium-241

HPGe Measurement Location	Real Sample No.	Radius (m)	QA Sample No.	Real Sample Am241(pCi/g)	25 1, 1120 - 1139 1139 1139 123	QA Sample Am241(pCi/g)	QA Sample 2s Counting Error	DER
30	99A5936-002.001	0	99A5936-003.001	2.37	.332	1.71	.276	1.529
	99A5936-004.001	1	99A5936-005.001	4.66	.366	4.46	.374	0.382
	99A5936-006.001	3	99A5936-007.001	3.57	.426	3.2	.313	0.700

HPGe Measurement Location	Real Sample No.	Radius (m)	QA Sample No.	Real Sample Am241(pCi/g)	Real Sample 2s Counting Error	QA Sample Am241(pCi/g)	QA Sample 2s Counting Error	DER
460	98A3372-002.002	0	98A3372-002.007	62.4	6.82	86.6	14.2	1.536
	98A3372-002.004	1	98A3372-002.008	183.	19.9	91.3	9.7	4.142
	98A3372-002.006	3	98A3372-002.009	95.	14.3	106.	12.9	0.571

HPGe Measurement Location	Real Sample No.	Radius (m)	Committee of the commit	Real Sample Am241(pCi/g)	Real Sample 2s Counting Error		QA Sample 2s Counting Error	DER
669	99A4878-003.001	0	99A4878-004.001	40.8	2.41	75.9	3.35	8.505
	99A4878-005.001	1	99A4878-006.001	55.1	7.35	66.7	3.15	1.451
	99A4878-007.001	3	99A4878-007.001	60.4	3.93	51.	3.93	1.691

# Surface Soil Characterization Program Precision Results Alpha Spectroscopy

HPGe MEASUREMENT LOCATION	SAMPLE TYPE	SAMPLE NUMBER	ANALYTE	RESULT	UNIT_	a	RC_SIGMA ERROR	DER
SALA TERROPERIO TELEBRICA NO TRANSPORTA	Camp 2000 507 (960)	99A5936-005.001	for Sales and the Control of the Control of the Control of Control	4.4612	PCI/G	9	0.3741	0.39
	Real	99A5936-004.001		4.6643	PCI/G		0.3659	0.00
	1	99A5936-007.001		3.1966	PCI/G		0.3134	0.71
	Real	99A5936-006.001		3.574	PCI/G		0.4259	J., .
		99A5936-003.001		1.7105	PCI/G		0.2759	1.52
	Real	99A5936-002.001		2.3659	PCI/G		0.332	
	<i>i</i>	99A3372-002.008	j.	172.9098	PCI/G	ł	5.4249	2.69
	Real	99A3372-002.004		151.9866	PCI/G		5.5795	2.00
		99A3372-002.009		145.2979	PCI/G		4.8513	0.99
	Real	99A3372-002.006		137.9899	PCI/G		5.5697	0.00
		99A3372-002.007		175.1638	PCI/G		5.6641	12.16
	Real	99A3372-002.002		90.1227	PCI/G		4.0973	12.10
		99A4878-006.001		66.7147	PCI/G	Ι,	3.1482	2.74
	Real	99A4878-005.001	I .	55.0517	PCI/G		2.8592	2.74
		99A4878-008.001	1	51.0332	PCI/G		2.5161	2.35
	Real	99A4878-007.001	1	60.4235	PCI/G		3.1018	2.55
		99A4878-004.001	l .	75.9211	PCI/G		3.3548	8.49
	Real	99A4878-003.001		40.8194	PCI/G		2.413	0.49
		99A5936-005.001	I	23.1372	PCI/G		0.8293	1.19
	Real	99A5936-004.001	ľ	21.7524	PCI/G		0.8293 0.8192	1.19
		99A5936-007.001	F .	1	•		1.2054	5.12
	Real		D .	15.5486	PCI/G		!	5.12
		99A5936-006.001	E .	23.8498	PCI/G		1.0835	4 24
	· ·	99A5936-003.001	<b>1</b>	8.4155	PCI/G		0.7811	4.31
		99A5936-002.001		12.8235	PCI/G		0.6603	20.00
		99A3372-002.008	li .	684.6637	PCI/G		12.2161	36.09
		99A3372-002.004	1	1481.6998			18.4008	0.04
		99A3372-002.009	1	l	PCI/G		15.1618	8.94
	Real	99A3372-002.006	1	675.0613	PCI/G		10.7885	40.00
		99A3372-002.007		782.3574	PCI/G		13.1426	13.22
		99A3372-002.002	l .	554.3172	PCI/G		11.1808	
		99A4878-006.001	Pu-239/240	435.6164	PCI/G		8.6241	10.35
		99A4878-005.001	Pu-239/240	318.3239	PCI/G		7.3486	
, i		99A4878-008.001	l .	1	PCI/G		7.2987	7.13
		99A4878-007.001		1	PCI/G		8.3559	
		99A4878-004.001	i e		PCI/G		9.415	22.44
		99A4878-003.001	1	1	PCI/G		6.7098	
		99A5936-005.001		1	PCI/G		0.1928	0.00
t t		99A5936-004.001					0.184	
		99A5936-007.001					0.1677	0.26
		99A5936-006.001			PCI/G		0.1997	4
		99A5936-003.001			PCI/G		0.6882	2.13
		99A5936-002.001			PCI/G	J	0.2129	
		99A3372-002.008		1.0197	PCI/G		.1613	0.70
	t	99A3372-002.004	·	.8624	PCI/G	J	.1556	
		99A3372-002.009		1.184	PCI/G		.2339	0.16
		99A3372-002.006		1.1367	PCI/G		.1879	
1	-	99A3372-002.007	1	.8937	PCI/G	1 1	.1574	0.95
		99A3372-002.002		1.1157	PCI/G	1 1	.1721	
669	Duplicate	99A4878-006.001	U-233,-234	0.842	PCI/G	J	0.3213	0.52

# Surface Soil Characterization Program Precision Results Alpha Spectroscopy

	I CONTRACTOR STATE OF THE STATE	A	Ipha Spectro	scopy	Petronova saturate and	1	I work the wind the same of th	NOVE Acres continues assessed acres days a production of
HPGe	0411015	50. 30.00	estate of schill		100		An are passed in	
MEASUREMENT	100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to	SAMPLE	446,446,925		UNIT_		RC_SIGMA	grander Landenberger
LOCATION	TYPE	NUMBER	ANALYTE	RESULT	CODE	u	NACH THE RESERVE OF THE PROPERTY OF THE PROPER	DER
<u> </u>	Real	99A4878-005.001	U-233,-234	0.6224	1	J	0.2696	
			1	0.8276	l .	J	0.3128	0.25
	Real	99A4878-007.001		0.9393	l .	J	0.326	
•		99A4878-004.001		0.6928		J	0.4082	0.12
	Real	99A4878-003.001	U-233,-234	0.7556		J	0.3191	
		99A5936-005.001	U-235	0.08	i .	J	0.0614	0.52
	Real	99A5936-004.001	U-235	0.0413	,	U	0.0433	
	-	99A5936-007.001	U-235	0.0434			0.0454	0.66
9	Real	99A5936-006.001	U-235	0.1111	1		0.0926	
		99A5936-003.001	U-235	0.1025		U	0.1417	0.07
	Real	99A5936-002.001	U-235	0.0907		J	0.0725	
		99A3372-002.008		.0883		J	.0489	0.23
	Real	99A3372-002.004	U-235	.0729		J	.045	
		99A3372-002.009	U-235	.0837	PCI/G	J	.0618	0.36
460	Real	99A3372-002.006	U-235	.0566	PCI/G	J	.0418	
460	Duplicate	99A3372-002.007	U-235	.0986	PCI/G	J	.0525	0.05
460	Real	99A3372-002.002	U-235	.0948	PCI/G	J	.0505	
		99A4878-006.001	U-235	0.0524	PCI/G	U	0.0835	0.06
669	Real	99A4878-005.001	U-235	0.0457	PCI/G	υ	0.0854	
669	Duplicate	99A4878-008.001	U-235	0.065	PCI/G	U	0.0993	0.84
669	Real	99A4878-007.001	U-235	-0.0205	PCI/G	U	0.0231	
669	Duplicate	99A4878-004.001	U-235	-0.0382	PCI/G	U	0.0431	0.87
669	Real	99A4878-003.001	U-235	0.0463	PCI/G	υ	0.0865	
30	Duplicate	99A5936-005.001	U-238	0.9948	PCI/G	J	0.2135	0.53
30	Real	99A5936-004.001	U-238	1.1579	PCI/G		0.2215	
30	Duplicate	99A5936-007.001	U-238	1.0056	PCI/G	-	0.212	0.05
30	Real	99A5936-006.001	U-238	1.024	PCI/G		0.2661	
30	Duplicate	99A5936-003.001	U-238	2.8263	PCI/G		0.751	2.57
30	Real	99A5936-002.001	U-238	0.823	PCI/G	J	0.211	
460	Duplicate	99A3372-002.008	U-238	2.5451	PCI/G		.2547	1.71
460	Real	99A3372-002.004	U-238	1.9538	PCI/G		.2339	
460	Duplicate	99A3372-002.009	U-238	2.442	PCI/G		.3347	0.50
460	Real	99A3372-002.006		2.661	PCI/G		.2875	
460	Duplicate	99A3372-002.007	U-238	2.2426	PCI/G		.2482	0.61
		99A3372-002.002		2.4613	PCI/G		.2549	
669		99A4878-006.001		1.4272	PCI/G		0.4037	0.78
	•	99A4878-005.001	í i	1.0122	PCI/G		0.3429	
Y .		99A4878-008.001		1.3592	PCI/G		0.3867	0.60
				1.0519	PCI/G		0.3389	,
	1	99A4878-004.001		1.1399	PCI/G		0.4882	0.02
		99A4878-003.001		1.1541	PCI/G		0.3669	3.92

# Subsurface Soil Characterization Program Precision Results - Americium-241

Borehole	Sample Type	RIN/Event/Bottle	Analyte	Result	Unit	lo	Det Limit	Sigma Error	DER
90198		98A1496-001.014	AM-241	12 15 10 10 10 10 10 10 10 10 10 10 10 10 10	PCI/G	g (Sec.	0.024	0.51	6.803
1	Real	98A1496-001.006	AM-241	i e	PCI/G		1.09	12.2	0.000
90698	Replicate	98A1055-003.036	AM-241		PCI/G		0.224	69.1	5.415
	Real	98A1055-003.033	AM-241	r	PCI/G	1	5.13	228	
90798	Replicate	98A1055-002.020	AM-241		PCI/G	lυ	0.086	0.044	0.163
	Real	98A1055-002.019	AM-241		PCI/G	J	0.027	0.043	31.133
91298	Replicate	98A1055-001.011	AM-241		PCI/G	ľ	0.038	0.085	0.817
	Real	98A1055-001.010	AM-241		PCI/G	IJ	0.040	0.072	
91598	Replicate	98A1296-001.010	AM-241	•	PCI/G		94.6	1604	4.548
	Real	98A1296-001.002	AM-241	1	PCI/G		51.5	3776	
91698	Replicate	98A2017-001.012	AM-241		PCI/G		25.6	546	0.132
	Real	98A2017-001.002	AM-241	3930	PCI/G		53.2	526	
92498	Replicate	98A1502-001.010	AM-241	16.7	PCI/G		0.904	3.38	5.443
	Real	98A1502-001.002	AM-241	59.5	PCI/G		0.118	7.1	
92698	Replicate	98A2022-001.010	AM-241	0.311	PCI/G		0.099	0.133	0.182
	Real	98A2022-001.004	AM-241	0.345	PCI/G		0.059	0.131	
93098	Replicate	99A4353-005.001	AM-241	0.181	PCI/G	J	0.115	0.120	0.819
	Real	99A4353-004.002	AM-241	0.361	PCI/G	1	0.146	0.184	
93698	Replicate	98A1289-001.010	AM-241	76.8	PCI/G		19.8	23.8	2.805
	Real	98A1289-001.004	AM-241	9.95	PCI/G		0.084	1.31	
94298	Replicate	99A4849-005.002	AM-241	0.26	PCI/G	J	0.123	0.147	1.456
	Real	99A4849-004.002	AM-241	0.026	PCI/G	υ	0.107	0.065	
94598	Replicate	98A5489-001.009	AM-241	0.026	PCI/G	U	0.074	0.048	0.090
	Real	98A5489-001.008	AM-241	0.032	PCI/G	U	0.066	0.046	
95298	Replicate	98A5494-001.009	AM-241	0.225	PCI/G	J	0.057	0.105	0.084
	Real	98A5494-001.008	AM-241	0.238	PCI/G	J	0.083	0.114	
95798	Replicate	99A5832-005.002	AM-241	0.031	PCI/G	U	0.123	0.075	0.777
	Real	99A5832-004.002	AM-241	0.13	PCI/G	J	0.113	0.103	
95998	Replicate	99A7799-009.003	AM-241	0.035	PCI/G	U	0.048	0.050	0.317
	Real	99A7799-006.003	AM-241	0.016	PCI/G	U	0.045	0.033	·
96298	Replicate	99A3210-004.009	AM-241		PCI/G	U	0.200	0.110	3.144
	Real	99A3210-004.008	AM-241		PCI/G		0.143	0.556	
96798	Replicate	99A6650-006.003	AM-241	0	PCI/G	U	0.054	0.000	0.841
	Real	99A6650-005.003	AM-241		PCI/G		0.048	0.063	
97598	Replicate	99A7937-005.001	AM-241	ı	PCI/G		0.041	0.152	0.558
	Real	99A7937-004.002	AM-241		PCI/G		0.041	0.117	
97698	Replicate	99A8275-006.003	AM-241		PCI/G		0.052	0.000	0.268
	Real	99A8275-001.003	AM-241	0.011	PCI/G	U	0.090	0.041	

# Subsurface Soil Characterization Program Precision Results - Plutonium-239/240

	Sample Type	RIN/Event/Bottle	Analyte	Result	Unit	Q	Det_Limit	Sigma_Error	DER
D	Replicate	98A1496-001.014	PU-239	20.6	PCI/G		0.016	2.41	6.951
90198		98A1496-001.006	PU-239	711	PCI/G	1	6.49	99.3	l
90698	Replicate	98A1055-003.036	PU-239	7320	PCI/G		3.04	858	2.211
90698		98A1055-003.033	PU-239	10670	PCI/G		1.91	1249	
	Replicate	98A1055-002.020	PU-239	0.039	PCI/G	U	0.040	0.032	0.747
90798	Real	98A1055-002.019	PU-239	0.01	PCI/G	U	0.051	0.022	
	Replicate	98A1055-001.011	PU-239	1.5	PCI/G	ĺ	0.034	0.263	0.028
91298		98A1055-001.010	PU-239	1.49	PCI/G		0.032	0.247	ŀ
	Replicate	98A1296-001.010	PU-239	70030	PCI/G		37	8213	4.194
91598		98A1296-001.002	PU-239	152260	PCI/G		17.8	17801	
	Replicate	98A2017-001.012	PU-239	373	PCI/G		42.5	95.9	0.112
91698		98A2017-001.002	PU-239	389	PCI/G		50.4	106	
92498	Replicate	98A1502-001.010	PU-239	94.8	PCI/G		0.582	12.3	6.547
92498	Real	98A1502-001.002	PU-239	474	PCI/G		0.583	56.6	l
92698	Replicate	98A2022-001.010	PU-239	0.464	PCI/G		0.061	0.156	2.378
92698		98A2022-001.004	PU-239	1.22	PCI/G		0.061	0.277	· .
	Replicate	99A4353-005.001	PU-239/240	0.812	PCI/G		0.083	0.291	2.121
93098		99A4353-004.002	PU-239/240	2.33	PCI/G	В	0.037	0.654	
93698	Replicate	98A1289-001.010	PU-239	495	PCI/G		15.3	80.7	5.506
93698		98A1289-001.004	PU-239	49.5	PCI/G		0.049	5.91	
	Replicate	99A4849-005.002	PU-239/240	7.35	PCI/G		0.034	1.82	3.760
94298		99A4849-004.002	PU-239/240	0.471	PCI/G	'	0.033	0.186	
	Replicate	98A5489-001.009	PU-239/240	0.08	PCI/G	J	0.020	0.052	0.013
94598		98A5489-001.008	PU-239/240	0.081	PCI/G	J	0.050	0.060	
	Replicate	98A5494-001.009	PU-239/240	0.982	PCI/G		0.037	0.291	0.690
95298		98A5494-001.008	PU-239/240	1.31	PCI/G		0.022	0.376	
	Replicate	99A5832-005.002	PU-239/240		PCI/G		1	0.205	0.817
95798		99A5832-004.002	PU-239/240	0.816	PCI/G		0.082	0.282	
The second secon	Replicate	99A7799-009.003	PU-239/240		PCI/G	U	0.041	0.000	0.826
95998	CONTRACTOR CONTRACTOR	99A7799-006.003	PU-239/240	-0.019	PCI/G	U	0.102	0.023	
	Replicate	99A3210-004.009	PU-239/240		PCI/G	U	0.037	0.040	3.245
96298			PU-239/240		PCI/G		0.070	0.492	
THE RESIDENCE OF THE PROPERTY	Replicate		PU-239/240	-0.007			0.079	0.014	0.500
96798	***	99A6650-005.003	PU-239/240	0	PCI/G	U	0.052	0.000	
personal comprehensive and a feature and a comprehensive and a second se	Replicate		PU-239/240	2.88	PCI/G		0.048	0.833	2.187
97598			PU-239/240	0.913	PCI/G		0.085	0.339	
	Replicate		PU-239/240	0.037	PCI/G	U	0.049	0.052	0.261
97698	Real	99A8275-001.003	PU-239/240	0.06	PCI/G	J	0.054	0.071	

### Subsurface Soil Characterization Program Precision Results - Uranium-233/234

Borehole	Sample Type	RIN/Event/Bottle	Analyte	Result	Unit	Q	Det_Limit	Sigma_Error	DER
93098	Replicate	99A4353-005.001	U-233/234	0.575	PCI/G	J	0.035	0.212	0.573
93098		99A4353-004.002	U-233/234	0.773	PCI/G	J	0.040	0.273	
94298	Replicate	99A4849-005.002	U-233/234	0.549	PCI/G	J	0.088	0.209	0.428
94298	Real	99A4849-004.002	U-233/234	0.686	PCI/G	J	0.074	0.242	
94598	Replicate	98A5489-001.009	U-233/234	0.735	PCI/G	J	0.017	0.211	0.214
94598	Real	98A5489-001.008	U-233/234	0.802	PCI/G	J	0.019	0.232	,
95298	Replicate	98A5494-001.009	U-233/234	0.652	PCI/G	J	0.033	0.196	0.346
95298	Real	98A5494-001.008	U-233/234	0.562	PCI/G	J	0.017	0.171	
	Replicate	99A5832-005.002	U-233/234	0.783	PCI/G	J	0.095	0.272	0.363
95798		99A5832-004.002	U-233/234	0.654	PCI/G	J	0.068	0.228	
95998	Replicate	99A7799-009.003	U-233/234	0.769	PCI/G	J	0.046	0.285	0.880
95998	Real	99A7799-006.003	U-233/234	0.455	PCI/G	J	0.054	0.215	
	Replicate	99A3210-004.009	U-233/234	0.4	PCI/G	J	0.076	0.172	0.869
96298	Real	99A3210-004.008	U-233/234	0.656	PCI/G	J	0.038	0.239	
	Replicate	99A6650-006.003	U-233/234	0.591	PCI/G	J	0.039	0.226	0.041
96798	Real	99A6650-005.003	U-233/234	0.578	PCI/G	J	0.040	0.225	
97598	Replicate	99A7937-005.001	U-233/234	0.95	PCI/G	J	0.075	0.323	0.061
97598	Real	99A7937-004.002	U-233/234	0.978	PCI/G	J	0.042	0.327	
97698	Replicate	99A8275-006.003	U-233/234	0.407	PCI/G	J	0.050	0.196	0.382
97698	Real	99A8275-001.003	U-233/234	0.519	PCI/G	J	0.079	0.218	
90198	Replicate	98A1496-001.014	U-234	0.756	PCI/G	J	0.024	0.128	1.255
90198		98A1496-001.006	U-234	1.58	PCI/G		0.479	0.644	
	Replicate	98A1055-003.036	U-234	1.83	PCI/G	U	2.72	1.75	1.067
90698		98A1055-003.033	U-234	5.14	PCI/G		2.68	2.56	
	Replicate	98A1055-002.020	U-234	3		J	0.024	0.118	0.231
90798	Real	98A1055-002.019	U-234	0.859	PCI/G	J	0.015	0.121	
91298	Replicate	98A1055-001.011	U-234	0.368	PCI/G	J	0.014	0.062	1.038
91298	Real	98A1055-001.010	U-234	0.284	PCI/G	J	0.012	0.052	
91598	Replicate	98A1296-001.010	U-234	31.5	PCI/G		23.6	20.7	0.415
91598	Real	98A1296-001.002	U-234	19.8	PCI/G	U	30.6	19.1	
	Replicate	98A2017-001.012	U-234		PCI/G		27.6	16.7	0.568
91698	Real	98A2017-001.002	U-234	1.83	PCI/G	U	30.1	14.0	
Committee of the commit	Replicate	98A1502-001.010	U-234	I	PCI/G		0.748	0.746	0.928
92498	Real	98A1502-001.002	U-234	0.758	PCI/G	J	0.043	0.181	
92698	Replicate	98A2022-001.010	U-234	0.477	PCI/G	J	0.057	0.145	0.180
92698	Real	98A2022-001.004	U-234	0.442	PCI/G	J	0.059	0.130	
	Replicate	98A1289-001.010	U-234	0.883	PCI/G	J	0.037	0.156	1.867
93698	Real	98A1289-001.004	U-234	0.511	PCI/G	J	0.057	0.124	

# Subsurface Soil Characterization Program Precision Results - Uranium-235

Borehole	Sample Type	RIN/Event/Bottle	Analyte	Result	Unit	Q	Det_Limit	Sigma_Error	DER
	Replicate	98A1496-001.014	U-235	0.038	PCI/G	J	0.022	0.022	1.016
90198	Real	98A1496-001.006	U-235	0.384	PCI/G	U	0.514	0.34	
90698	Replicate	98A1055-003.036	U-235	0.412	PCI/G	U	1.94	1.03	0.106
90698	Real	98A1055-003.033	U-235	0.577	PCI/G	U	2.42	1.16	
90798	Replicate	98A1055-002.020	U-235	0.045	PCI/G	J	0.014	0.018	0.427
90798	Real	98A1055-002.019	U-235	0.035	PCI/G	J	0.009	0.015	
91298	Replicate	98A1055-001.011	U-235	0.018	PCI/G	J	0.013	0.011	0.774
91298	Real	98A1055-001.010	U-235	0.007	PCI/G	U	0.016	0.009	
91598	Replicate	98A1296-001.010	U-235	-1.748	PCI/G	U	19.2	10.2	0.602
91598	Real	98A1296-001.002	U-235	7.2	PCI/G		19.8	10.8	
	Replicate	98A2017-001.012	U-235		PCI/G		21.2	12.8	0.224
91698	Real	98A2017-001.002	U-235	-0.913	PCI/G	U	23.2	14.0	
92498	Replicate	98A1502-001.010	U-235	0.438	PCI/G	U	0.603	0.413	0.830
92498		98A1502-001.002	U-235	0.092	PCI/G	J	0.043	0.057	
92698	Replicate	98A2022-001.010	U-235	0.008	PCI/G	U	0.049	0.029	0.341
92698	Real	98A2022-001.004	U-235	0.022	PCI/G	U	0.049	0.029	
93098	Replicate	99A4353-005.001	U-235	0.072	PCI/G	U	0.076	0.075	0.960
93098	Real	99A4353-004.002	U-235	0	PCI/G	U	0.050	0.000	
93698	Replicate	98A1289-001.010	U-235	0.05	PCI/G	J	0.027	0.029	0.439
93698	Real	98A1289-001.004	U-235	0.032	PCI/G	U	0.039	0.029	
94298	Replicate	99A4849-005.002	U-235	0.056	PCI/G	U	0.076	0.066	0.249
94298	Real	99A4849-004.002	U-235	0.034	PCI/G	U	0.091	0.059	
94598	Replicate	98A5489-001.009	U-235	l:	PCI/G	J	0.021	0.032	0.231
94598	·	98A5489-001.008	U-235	0.043	PCI/G	J	0.024	0.041	
95298	Replicate	98A5494-001.009	U-235	0.038	PCI/G	U	0.040	0.040	0.307
95298		98A5494-001.008	U-235	0.023	PCI/G	J	0.021	0.028	
95798	Replicate	99A5832-005.002	U-235	0.01	PCI/G	U	0.081	0.037	0.120
95798	Real	99A5832-004.002	U-235	1	PCI/G	U	0.084	0.045	
95998	Replicate	99A7799-009.003	U-235	0.084	PCI/G	J	0.057	0.088	0.683
95998		99A7799-006.003	U-235	0.21	PCI/G	J	0.117	0.162	
96298	Replicate	99A3210-004.009	U-235	-0.007	PCI/G	U	0.079	0.014	1.200
96298	Real	99A3210-004.008	U-235		1	J	0.083	0.099	
	Replicate	99A6650-006.003	U-235		PCI/G	U	0.085	0.014	0.919
96798		99A6650-005.003	U-235	1	PCI/G	J	0.050	0.066	
97598	Replicate	99A7937-005.001	U-235		PCI/G	U	0.109	0.093	0.033
97598	Real	99A7937-004.002	U-235	0.077	PCI/G	J	0.052	0.080	
	Replicate	99A8275-006.003	U-235		PCI/G	J	0.062	0.108	0.053
97698	Real	99A8275-001.003	U-235	0.122	PCI/G	J	0.055	0.106	

# Subsurface Soil Characterization Project Precision Results - Uranium-238

Borehole	Sample Type	RIN/Event/Bottle	Analyte	Result	Unit	Q	Det Limit	Sigma Error	DER
90198	Replicate	98A1496-001.014	U-238	0.828	PCI/G	J	0.025	0.137	1.471
90198	Real	98A1496-001.006	U-238	1.9	PCI/G		0.546	0.716	
90698	Replicate	98A1055-003.036	U-238	2.89	PCI/G	U	3.69	2.37	1.289
90698	Real	98A1055-003.033	U-238	7.92	PCI/G		2.42	3.1	
90798	Replicate	98A1055-002.020	U-238	0.689	PCI/G	J	0.020	0.102	1.024
90798	Real	98A1055-002.019	U-238	0.851	PCI/G	J	0.016	0.121	
91298	Replicate	98A1055-001.011	U-238	0.395	PCI/G	J	0.015	0.065	0.879
91298	Real	98A1055-001.010	U-238	0.319	PCI/G	J	0.020	0.057	
91598	Replicate	98A1296-001.010	U-238	90.9	PCI/G		26.9	35	1.571
91598	Real	98A1296-001.002	U-238	28.2	PCI/G		19.8	19.2	
91698	Replicate	98A2017-001.012	U-238	4.18	PCI/G	lυ	31.9	12.8	0.172
91698	Real	98A2017-001.002	U-238	0.913	PCI/G	U	32.7	14.0	
92498	Replicate	98A1502-001.010	U-238	1.31	PCI/G		0.501	0.68	0.293
92498	Real	98A1502-001.002	U-238	1.1	PCI/G		0.056	0.229	
92698	Replicate	98A2022-001.010	U-238	0.658	PCI/G	J	0.064	0.175	0.628
92698	Real	98A2022-001.004	U-238	0.516	PCI/G	J	0.059	0.143	
93098	Replicate	99A4353-005.001	U-238	0.592	PCI/G	J	0.061	0.217	0.163
93098	Real	99A4353-004.002	U-238	0.645	PCI/G	J	0.072	0.242	
93698	Replicate	98A1289-001.010	U-238	1.62	PCI/G		0.030	0.246	2.922
93698	Real	98A1289-001.004	U-238	0.764	PCI/G	J	0.044	0.159	
94298	Replicate	99A4849-005.002	U-238	0.739	PCI/G	J	0.061	0.253	0.093
94298	Real	99A4849-004.002	U-238	0.773	PCI/G	J	0.073	0.263	
94598	Replicate	98A5489-001.009	U-238	0.659	PCI/G	J	0.035	0.193	0.506
94598	Real	98A5489-001.008	U-238	0.813	PCI/G	J	0.019	0.235	
95298	Replicate	98A5494-001.009	U-238	0.733	PCI/G	J	0.018	0.214	0.495
95298	Real	98A5494-001.008	U-238	0.595	PCI/G	J	0.030	0.179	1
95798	Replicate	99A5832-005.002	U-238	0.66	PCI/G	J	0.066	0.240	0.373
95798	Real	99A5832-004.002	U-238	0.792	PCI/G	J	0.067	0.260	ı
95998	Replicate	99A7799-009.003	U-238	0.854	PCI/G	J	0.096	0.308	0.463
95998	Real	99A7799-006.003	U-238	1.08	PCI/G		0.094	0.379	
96298	Replicate	99A3210-004.009	U-238	0.353	PCI/G	J	0.084	0.161	1.902
96298	Real	99A3210-004.008	U-238	1.06	PCI/G	В	0.038	0.335	
96798	Replicate	99A6650-006.003	U-238	0.798	PCI/G	J	0.069	0.278	0.795
96798	Real	99A6650-005.003	U-238	0.52	PCI/G	J	0.083	0.212	
97598	Replicate	99A7937-005.001	U-238	0.828	PCI/G	J	0.042	0.292	0.147
97598	Real	99A7937-004.002	U-238		PCI/G	J	0.074	0.306	
	Replicate	99A8275-006.003	U-238	0.472	PCI/G	J	0.088	0.216	0.092
97698	Real		U-238	0.5	PCI/G	J	0.078	0.213	

# Subsurface Soil Characterization Program Precision Results - Relative Percent Difference - VOCs

Borehole	Sample Type	RIN/Event/Bottle	Analyte	Result	Unit	Q	%RPD
92598	Dup	98A1092-001.037	Carbon Tetrachloride	740	UG/KG	Ü	2.7
92598	Real	98A1092-001.036	Carbon Tetrachloride	720	UG/KG	U	
95998	Dup	99A7799-009.002	Carbon Tetrachloride	6.1	UG/KG	U	3.2
95998	Real	99A7799-006.002	Carbon Tetrachloride	6.3	UG/KG	U	
96298	Dup	99A3210-004.015	Carbon Tetrachloride	700	UG/KG	U	4.4
96298	Real	99A3210-004.014	Carbon Tetrachloride	670	UG/KG	U	
96798	Dup	99A6650-006.002	Carbon Tetrachloride	0.81	UG/KG	J	147
96798	Real	99A6650-005.002	Carbon Tetrachloride	5.3	UG/KG	J	
97698	Dup	99A8275-006.002	Carbon Tetrachloride	5.4	UG/KG	U	1.9
97698	Real	99A8275-001.002	Carbon Tetrachloride	5.3	UG/KG	U	
97698	Dup	99A8275-006.002	1,2-Cis-Dichloroethylene	5.4	UG/KG	U	1.9
97698	Real	99A8275-001.002	1,2-Cis-Dichloroethylene	5.3	UG/KG	U	
96798	Dup	99A6650-006.002	1,2-Cis-Dichloroethylene	6.8	UG/KG	Ū	74.7
96798	Real	99A6650-005.002	1,2-Cis-Dichloroethylene	14.9	UG/KG		
96298	Dup		1,2-Cis-Dichloroethylene	700	UG/KG	U	4.4
96298	Real	99A3210-004.014	1,2-Cis-Dichloroethylene	670	UG/KG	U	
95998	Dup	99A7799-009.002	1,2-Cis-Dichloroethylene	6.1	UG/KG	U	171.5
95998	Real	99A7799-006.002	1,2-Cis-Dichloroethylene	79.5	UG/KG	П	
92598	Dup	98A1092-001.037	1,2-Cis-Dichloroethylene	740	UG/KG	U	2.7
92598	Real	98A1092-001.036	1,2-Cis-Dichloroethylene	720	UG/KG	U	
97698	Dup	99A8275-006.002	Tetrachloroethene	5.4	UG/KG	U	1.9
97698	Real	99A8275-001.002	Tetrachloroethene	5.3	UG/KG	U	
96798	Dup	99A6650-006.002	Tetrachloroethene	7.8	UG/KG		161
96798	Real	99A6650-005.002	Tetrachloroethene	72.2	UG/KG	П	
96298	Dup	99A3210-004.015	Tetrachloroethene	700	UG/KG	U	4.4
96298	Real	99A3210-004.014	Tetrachloroethene	670	UG/KG	U	
95998	Dup	99A7799-009.002	Tetrachloroethene	6.1	UG/KG	Ū	193
95998	Real	99A7799-006.002	Tetrachloroethene	343	UG/KG	E	
92598	Dup	98A1092-001.037	Tetrachloroethene	740	UG/KG	U	2.7
92598	Real	98A1092-001.036	Tetrachloroethene	720	UG/KG	U	
97698	Dup	99A8275-006.002	Trichloroethene	5.4	UG/KG	U	1.9
97698	Real	99A8275-001.002	Trichloroethene	5.3	UG/KG	U	
96798	Dup	99A6650-006.002	Trichloroethene	0.85	UG/KG	J	179.9
96798	Real	99A6650-005.002	Trichloroethene	16.1	UG/KG	П	
96298	Dup	99A3210-004.015	Trichloroethene	700	UG/KG	U	4.4
96298	Real	99A3210-004.014	Trichloroethene	670	UG/KG	U	
95998	Dup	99A7799-009.002	Trichloroethene	6.1	UG/KG	U	71.6
95998	Real	99A7799-006.002	Trichloroethene	12.9	UG/KG	$\Box$	
92598	Dup	98A1092-001.037	Trichloroethene	740	UG/KG	U	2.7
92598	Real	98A1092-001.036	Trichloroethene	720	UG/KG	U	

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### Appendix C

903 Pad *In-Situ* Models and Uncertainties

### 903 PAD IN SITU MODELS AND UNCERTAINTIES

### In Situ Models

The Canberra in situ systems used to perform measurements at the RFETS 903 Pad project site employ the Canberra In Situ Object Counting System (ISOCS) software. This software package allows the user to calculate efficiencies for in situ quantification of defined objects using standard templates. One such template has been used to define the in situ measurement of contaminants in soils at the 903 Pad locations. This template requires the entry of various parameters which should accurately represent the actual conditions at the project site.

The template selected for this application is the circular plane source. This template requires the user to define a horizontal source size, a vertical source size, material composition and material density. In addition, the software uses detector specific physical parameters and user definable environmental parameters such as humidity, pressure and temperature. Each of these parameters has been defined in the model to represent actual conditions at 903 Pad, using existing knowledge of the site and project defined parameters. These parameter values, and the basis for selection, are described below.

Use of inappropriate values could lead to errors in *in situ* measurements. The model used for routine measurements contains the values most representative of actual conditions, however it is possible that actual measurement locations may vary from these assumed default conditions. Since it is not possible to verify all parameter values at each measurement location, default values will be used except where it is known that conditions vary significantly. An evaluation of the potential errors associated with deviation from default parameters has been performed and forms the basis of the total propagated measurement uncertainty (TMU) used when reporting *in situ* measurement results. These are also described below.

### Soil Density

The available soil density data from 903 Pad locations shows densities ranging from 1.0 to 1.3 g/cc. *In Situ* soil densities are typically on the order of 1.6 g/cc, but it is believed that, due to the lower moisture content of RFETS soils, this value may be too high. The ISOCS model uses a value of 1.3 g/cc as a mean value for 903 Pad soils.

### Uniformity

The uniformity, or non-uniformity, of contamination, both vertically and horizontally, will impact measurement results. Based on the mode of contamination deposition and on prior survey results (including *in situ* surveys), it is believed that the contamination is relatively uniform within the field of view in the ISOCS systems. This is a reasonable assumption since the in situ measurements integrate the readings over nearly 80 sq m areas. Thus, any individual "hot spots" are averaged over the entire area, or volume, and their impacts are minimized. The ISOCS model is based on uniform distributions.

### **Environmental Conditions**

Environmental temperature, humidity and pressure may impact some measurements. The ISOCS models assume standard environmental conditions; i.e. 20 C, 50 % relative humidity and 760 mm barometric pressure. Normal barometric pressure at RFETS is less, but the impact is negligible, as shown below.

### **Detector Parameters**

An ISOCS efficiency for each detector has been generated, using the specific detector characteristics, which tend to remain constant for long periods of time. The parameter of concern is the detector surface dead layer, which, if it increases could effect detection of low energy photons. This can be monitored by routine check source counts using a source with a low energy photon, such as Am-241. There have been no changes to these parameters over the course of the 903 Pad Project.

The ISOCS template used for the 903 Pad ISOCS efficiency is attached.

```
Default soil; Dry Dirt (490, 27Si, 4Fe, 1.6Mg, 4Ca, 2.7K, 7Al) Am-241 = 12.2 pCi/g
Dirt 2 (550, 31Si, 3Fe, 7Al) Am-241 = 11.6 pCi/g
Dirt 4 (450, 25Si, 12Fe, 2.5Mg, 4.1Ca, 2Mn, 8.3Al, 0.7Ti) Am-241 = 15.4 pCi/g
```

The overall impact of a likely range of compositions is about +/- 25%

### Soil Density

Soil densities were varied from the minimum of 1.0 to a maximum of 1,6 g/cc.

### Results

Default density 1.3 g/cc	Am-241 = 12.2 pCi/g
Density 1.6 g/cc	Am-241 = 12.0  pCi/g
Density 1.0 g/cc	Am-241 = 13.8 pCi/g

The overall impact of density changes is about +/- 10 %-

### **Environmental Conditions**

The default temperature and relative humidity are close to the ranges at RFETS but the default pressure is 20 % higher than normal barometric pressure at this altitude. However, changing the parameters to the RFETS values had no impact (same Am-241 results).

### **Detector Parameters**

Detector characteristics have been shown to be unchanged since factory calibration by verifying response by counting a standard reference material and obtaining the correct result. There is no error assigned to this.

### Data Quality Objectives for Measurement Data

Data Quality Objectives (DQOs) are qualitative and quantitative statements that describe the *in situ* characterization technical and quality objectives, define the appropriate type of data and specify acceptable levels of decision errors used to establish the quality of data. These data are used to assist RMRS in developing remedial action or management actions for the affected areas. For 903 Pad *in situ* measurements, the DQO is:

• To classify surface soils as exceeding Tier I soil action levels. This objective is met by measuring soil concentrations of Am-241, U-235 and U-238. Concentrations of Pu and other U isotopes are derived from these measurements. In order to provide sufficient margin for detection of Tier I levels, detection limits for the three nuclides measurable by *in situ* methods have been set at; 1 pCi/g Am-241, 0.5 pCi/g U-235 and 5.0 pCi/g U-238.

Data Quality Objectives used to validate all data generated by *in situ* measurements include the following: precision, accuracy, sensitivity, completeness, comparability and total uncertainty. For the 903 Pad Project, these are defined as follows:

- <u>Precision</u> A quantitative measure of the reproducibility or degree of agreement among replicate or duplicate measurements of a parameter. For the 903 Pad Project, precision shall be demonstrated by performing duplicate counts of specified soil locations on a frequency not to exceed once per 20 measurement locations. The reproducibility shall be calculate using accepted methods for evaluation of duplicate counting.
- Accuracy The degree of agreement between measured concentration values and the true or known values. For *in situ* measurements, true values are difficult to establish and may be estimated from alternate assay methods. For this project. *In situ* results will be compared to laboratory analyses of discrete soil samples. Comparable measurements at the action levels are expected to agree within +/- 50%. Evaluation of accuracy will be performed by RMRS and Canberra technical representatives.
- <u>Sensitivity</u> Sensitivity limits are defined as that level of radioactivity which, if
  present, will yield a measured value less than the critical limit with 5% probability.
  The critical limit is defined as that value which measurements of background will
  exceed with a 5% probability. Sensitivity limits for three detectable radionuclides are
  specified above.
- Completeness A quantitative measure expressed as a percentage of valid or acceptable data obtained from a measurement system. A goal of 90% has been set for this project.

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903 Drum Storage Area,	Revision:	0
903 Lip Area, and Americium Zone	Date:	September 28, 1999
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### Appendix D

**Summary Statistics** 

Characterization Report for the	Document Number:	RF/RMRS-99-427.UN
903 Drum Storage Area,	Revision:	0
903 Lip Area, and Americium Zone	Date:	September 21, 1999
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### Appendix D

**Summary Statistics** 

Appendix D. Summary Statistics HPGe Data

		HPGe P	HPGe Prtedicted Data	ıta			
				35% UCL	95% UCL	Best Fit	Best Fit
			HPGe	Predicted	Predicted	Predicted	Predicted
	235U	238U	241Am	<sup>241</sup> Am <sup>1</sup>	<sup>239/240</sup> Pu <sup>2</sup>	<sup>241</sup> Am <sup>3</sup>	239/240Pu <sup>4</sup>
Descriptive Statistic	(pCi/g)	(pCi/g)	(bCi/g)	(pCi/g)	(pCi/g)	(pCi/g)	(pCi/g)
C C C C C C C C C C C C C C C C C C C	760	7 7	12.40	67 aC	00.100	00	
Geometric Mean	1 C C	DI IV	00.71 14.104	20.40 	07:107	ZO. 17	105.03
	0.00	#IAOIAII	iiNION#	# P P P P P P P P P P P P P P P P P P P	#NOM:	#NOM!	ï⊠∩Z#
standard Error	1.3/E-03	0.02	0.38	0.45	3.00	0.48	3.07
Median	0.23	4.37	9.62	24.80	176.67	16.46	80.94
Mode	0.23	3.63	0.90	15.46	118.91	5.56	10.55
Standard Deviation	0.05	0.67	12.67	15.02	100.11	15.85	102,38
Sample Variance	2.07E-03	0.45	160.54	225.69	10021.87	251.25	10481.30
Kurtosis	4.18	10.50	13.05	18.39	22.63	13.05	13.05
Skewness	-0.12	1.10	2.84	3.36	3.74	2.84	2.84
Coefficient of Variation	0.19	0.15	1.01	0.53	0.50	0.78	0.97
Range	0.51	10,04	115.36	150.48	1060.92	144.31	932.10
Minimum	0.07	1.31	0.38	14.91	115.55	4.91	6.32
Maximum	0.58	11,35	115.74	165.39	1176.47	149.22	938.42
Sum	261.72	4946.04	13985.89	31555.57	223330.46	22414.09	116602.40
Count	1110	1110	1110	1110	1110	0111	1110
Confidence Level (95,0%)	2,68E-03	0.04	0.75	0.88	5.89	0.93	6.02
Number of Detections Above Tier I	0	0	0	0	0	0	0
Number of Detections Above Tier II	0	0	48	162	183	0	82

Predicted <sup>241</sup> Am Based on Regression Equation:  $|^{241}Am = 0.0022*^{241}Am^2 + 1.049*^{241}Am + 14.509$ 

<sup>2</sup> Predicted <sup>239/240</sup> Pu Based on Regression Equation:

 $\begin{bmatrix}
239/240 Pu = 0.0243^{*24} Am^2 + 6.3749^{*24} Am + 113.12
\end{bmatrix}$   $\begin{bmatrix}
241 & Am = 1.251 * ^{24} & Am + 4.43
\end{bmatrix}$ 

<sup>3</sup> Predicted <sup>241</sup>Am Based on Regression Equation: <sup>4</sup> Predicted <sup>239/240</sup> Pu Based on Regression Equation:

 ${}^{241} Am = 1.251 * {}^{241} Am + 4.43$   ${}^{239} / {}^{240} Pu = 8.08 * {}^{241} Am + 3.24$ 

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Appendix D. Summary Statistics
Borehole Radiological Data-903 Pad and Lip Area

	As	phalt		<del></del>	
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	0.81	0.05	0.75	0.16	0.07
Geometric Mean	0.80	0.04	0.74	#N/A	0.04
Standard Error	0.05	0.01	0.04	0.13	0.03
Median	0.78	0.04	0.75	0.03	0.04
Mode	#N/A	#N/A	#N/A	#N/A	#N/A
Standard Deviation	0.15	0.03	0.13	0.40	0.10
Sample Variance	0.02	0.00	0.02	0.16	0.01
Kurtosis	1.70	7.01	-1.60	8.85	8.28
Skewness	1.22	2.46	-0.08	2.97	2.84
Coefficient of Variation	0.19	0.72	0.17	2.42	1.46
Range	0.47	0.12	0.32	1.22	0.33
Minimum	0.66	0.01	0.60	0.00	0.02
Maximum	1.13	0.13	0.92	1.22	0.34
Sum	7.27	0.42	6.74	1.48	0.63
Count	9	9	9	9	9
Confidence Level (90.0%)	0.08	0.02	0.07	0.22	0.06

	Be	drock			
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	0.49	0.04	0.62	0.09	0.04
Geometric Mean	0.49	0.04 N/A	0.52	0.05	0.04 N/A
Standard Error	0.45	0.01	0.06	0.03	0.02
Median	0.08	0.01	0.00	0.03	0.02
Mode	#N/A	#N/A	#N/A	0.04	0.03
Standard Deviation	0.19	0.03	0.19	0.11	0.06
Sample Variance	0.04	0.00	0.04	0.01	0.00
Kurtosis	1.08	-0.02	0.13	1.89	3.71
Skewness	0.86	0.50	-0.96	1.69	1.51
Coefficient of Variation	0.39	0.81	0.31	1.26	1.54
Range	0.72	0.12	0.63	0.35	0.26
Minimum	0.19	-0.01	0.22	0.01	-0.05
Maximum	0.90	0.11	0.84	0.36	0.21
Sum	5.83	0.51	7.43	1.07	0.50
Count	12	12	12	12	12
Confidence Level (95.0%)	0.11	0.02	0.11	0.06	0.04
Number of Detections Above Tier I	0	0	0	0	0
Number of Detections Above Tier II	0	0	0	0	0

### Appendix D. Summary Statistics Borehole Radiological Data-903 Pad and Lip Area

		Fill	· · · · · · · · · · · · · · · · · · ·		
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	4.06	0.00	1 1 5	E2 75	10.01
Geometric Mean	1.06	0.09	1.15	53.75	12.01
Standard Error	1.02	0.06	1.00	5.78	1.18
	0.11	0.04	0.18	45.95	10.38
Median	0.98	0.06	1.13	4.48	0.85
Mode	0.84	0.07	1.24	#N/A	#N/A
Standard Deviation	0.38	0.13	0.61	159.19	35.97
Sample Variance	0.14	0.02	0.37	25340.90	1294.08
Kurtosis	4.79	11.19	5.53	11.88	11.90
Skewness	1.51	3.30	1.72	3.44	3.44
Coefficient of Variation	0.36	1.43	0.53	2.96	2.99
Range	1.61	0.49	2.60	557.99	125.98
Minimum	0.41	0.00	0.17	0.01	0.02
Maximum	2.02	0.49	2.77	558.00	126.00
Sum	12.25	1.00	13.33	642.14	143.51
Count	12	12	12	12	12
Confidence Level (90.0%)	0.18	0.06	0.29	75.59	17.08
Number of Detections Above Tier I	0	0	0	. 0	0
Number of Detections Above Tier II	0	0	0	1	1

	N	ative			
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	0.51	0.04	0.63	0.27	0.11
Geometric Mean	0.31	0.04 <b>N</b> /A	0.60	0.27 <b>N</b> /A	0.11 N/A
Standard Error					
	0.02	0.01	0.02	0.06	0.03
Median	0.48	0.03	0.59	0.05	0.04
Mode	0.58	0.02	0.66	0.01	0.00
Standard Deviation	0.16	0.05	0.21	0.53	0.25
Sample Variance	0.02	0.00	0.04	0.28	0.06
Kurtosis	13.79	2.25	4.58	9.25	31.76
Skewness	2.74	1.65	1.72	2.94	5.20
Coefficient of Variation	0.31	1.10	0.33	2.00	2.32
Range	1.12	0.22	1.16	2.86	1.81
Minimum	0.28	-0.01	0.30	-0.02	-0.01
Maximum	1.40	0.21	1.46	2.84	1.80
Sum	36.37	3.18	45.03	19.18	7.70
Count	72	72	72	72	72
Confidence Level (95.0%)	0.04	0.01	0.05	0.12	0.06
Number of Detections Above Tier I	0	0	0	0	O
Number of Detections Above Tier II	0	0	0	0	0

### Appendix D. Summary Statistics Borehole Radiological Data-903 Pad and Lip Area

	Na	itive 1			<del></del>
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	5.31	0.60	16.00	3595.75	775.68
Geometric Mean	1,43	0.60 N/A	16.83 1.99	146.69	30.48
Standard Error	2.91			2462.86	514.23
Median		0.30	12.58		34.80
	0.99	0.06	1.32	152.00	
Mode	1.14	0.04	1.54	#N/A	#N/A
Standard Deviation	22.90	2.38	99.08	19392.56	4049.07
Sample Variance	524.52	5.65	9817.55	376071264.13	16394945.59
Kurtosis	55.37	38.00	60.51	59.32	58.16
Skewness	7.30	5.87	7.74	7.63	7.53
Coefficient of Variation	4.31	3.94	5.89	5.39	5.22
Range	177.58	17.81	779.51	152259.18	31669.85
Minimum	0.42	-0.91	0.49	0.82	0.15
Maximum	178.00	16.90	780.00	152260.00	31670.00
Sum	329.51	37,38	1043.61	222936.51	48092.47
Count	62	62	62	62	62
Confidence Level (95.0%)	5.70	0.59	24.66	4827.10	1007.87
Number of Detections Above Tier I	0	0	1	9	12
Number of Detections Above Tier II	Ö	0	. 1	27	27

	Na	itive 2	· · · · · · · · · · · · · · · · · · ·		
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
	4.00	0.40	4.50	422.44	25.22
Mean	1.00	0.16	1.50	122.11	25.23
Geometric Mean	0.76	N/A	0.98	8.65	1.79
Standard Error	0.18	0.11	0.29	41.76	8.90
Median	0.73	0.04	0.88	7.62	1.50
Mode	1.63	0.02	0.40	#N/A	#N/A
Standard Deviation	1.42	0.83	2.32	328.85	70.12
Sample Variance	2.00	0.69	5.39	108142.37	4916.12
Kurtosis	49.56	61.25	24.30	15.58	16.02
Skewness	6.73	7.80	4.59	3.81	3.82
Coefficient of Variation	1.41	5.08	1.55	2.69	2.78
Range	11.36	6.58	15.40	1819.87	405.97
Minimum '	0.04	-0.01	0.30	0.14	0.03
Maximum	11.40	6.57	15.70	1820.00	406.00
Sum	62.21	10.12	92.74	7571.08	1564.40
Count	62	62	62	62	62
Confidence Level (95.0%)	0.35	0.21	0.58	81.86	17.45
Number of Detections Above Tier I	0	0	0	2	2
Number of Detections Above Tier II	0	0	0	7	8

### Appendix D. Summary Statistics Borehole Radiological Data-903 Pad and Lip Area

	Na	ative 3			
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	0.70	0.05	0.00	10.24	2.44
1	0.70	0.05	0.96	16.24	3.14
Geometric Mean	0.59	N/A	0.71	1.33	N/A
Standard Error	0.06	0.01	0.16	5.09	1.07
Median	0.61	0.03	0.64	0.94	0.23
Mode	0.38	0.02	0.57	0.06	0.25
Standard Deviation	0.44	0.06	1.23	40.12	8.46
Sample Variance	0.19	0.00	1.52	1609.25	71.49
Kurtosis	14.59	16.55	32.01	20.03	23.95
Skewness	3.03	3.70	5.22	4.19	4.60
Coefficient of Variation	0.63	1.23	1.28	2.47	2.69
Range	3.11	0.37	9.00	246.99	54.41
Minimum	0.01	-0.01	0.10	0.01	-0.01
Maximum	3.12	0.36	9.10	247.00	54.40
Sum	43.32	2.92	59.60	1007.14	194.71
Count	62	62	62	62	62
Confidence Level (95.0%)	0.11	0.01	0.31	9.99	2.10
Number of Detections Above Tier I	0	0	0	0	0
Number of Detections Above Tier II	0	0	0	0	1

	Na	tive 4			
Descriptive Statistic	U233/234 (pCi/g)	U235 (pCi/g)	U238 (pCi/g)	Pu239/240 (pCi/g)	Am241 (pCi/g)
Mean	0.58	0.03	0.64	4.97	0.90
Geometric Mean	0.54	0.03 N/A	0.59	N/A	0.50 N/A
Standard Error	0.03	0.00	0.04	1.40	0.23
Median	0.55	0.03	0.59	0.80	0.23
Mode	0.76	0.01	0.63	34.50	0.15
Standard Deviation	0.21	0.02	0.29	10.63	1,72
Sample Variance	0.04	0.00	0.08	112.97	2.95
Kurtosis	1.50	2.86	6.66	9.49	6.52
Skewness	1.03	0.19	1.96	3.04	2.67
Coefficient of Variation	0.36	0.74	0.45	2.14	1.92
Range	1.05	0.15	1.78	54.00	7.68
Minimum	0.27	-0.05	0.19	0.00	-0.05
Maximum	1.32	0.10	1.97	54.00	7.63
Sum	33.44	1.79	37.07	288.35	51.98
Count	58	58	58	. 58	58
Confidence Level (95.0%)	0.05	0.01	0.07	2.74	0.44
Number of Detections Above Tier I	0	0	0	0	0
Number of Detections Above Tier II	0	0	0	0	1

N/A Not Applicable

Appendix D. Summary Statistics VOC Borehole Data

		Native				
Descriptive Statistic	Carbon Tetrachloride (μg/Kg)	Tetrachloroethene (µg/Kg)	Trichloroethene (μg/Kg)	Chloroform² (µg/Kg)	Cis-1,2- Dichloroethene (µg/Kg)	Methylene Chloride <sup>a</sup> (μg/Kg)
Mean	351.59	438.75	344.72	351.36	838 40	205 10
Geometric Mean	47.84	51.01	47.91	40.84	742.11	36.97
Standard Error	50.73	94.02	50.33	50.76	148.57	60.20
Median	00.9	24.80	6.30	6.20	700.00	5.90
Mode	5.30	5.30	5.30	700.00	700.00	5.30
Standard Deviation	427.48	797.76	424.12	427.68	742.86	507.21
Sample Variance	182742.10	636420.43	179878.11	182907.29	551839.00	257264.17
Kurtosis	-0.37	35.93	-0.24	-0.37	24.87	-0.12
Skewness	0.82	5.21	0.87	0.82	4.98	1.06
Coefficient of Variation	1.22	1.82	1.23	1.22	0.89	1.32
Range	1494.90	6099.22	1497.00	1499.36	3790.00	1699.41
Minimum	5.10	0.78	3.00	0.64	610.00	0.59
Maximum	1500.00	6100.00	1500.00	1500.00	4400.00	1700.00
Sum	24962.60	31589.97	24475.40	24946.28	20960.00	27343.80
Count	71	72	71	711	25	71
Confidence Level (95.0%)	99.43	184.27	98.65	99.48	291.19	117.98
Number of Detections Above Current Tier I SSAL	0	0	0	0	0	0
Number of Samples at 10% of Current Tier I SSAL	0	. 9	5	0	<del>-</del>	25
Number of Detections Above Proposed Tier I SSAL	0	-	0	0	0	25
Number of Detections Above Proposed Tier II SSAL	31	33	31	0	25	37
Number of Non Detections	20	55	99	64	24	36
Number of Detections	1	17	2	7	-	35

Appendix D. Summary Statistics VOC Borehole Data

		Bedrock				
Descriptive Statistic	Carbon Tetrachloride (µg/Kg)	Tetrachloroethene (μg/Kg)	Trichloroethene (μg/Kg)	Chloroform <sup>a</sup> (µg/Kg)	Cis-1,2- Dichloroethene (μg/Kg)	Methylene Chloride <sup>a</sup> (μg/Kg)
Mean	428.37	458.71	428.85	427.25	698.57	493.06
Geometric Mean	71.75	87.43	73.06	45.48	697.70	59.10
Standard Error	117.96	122.44	117.83	118.24	13.88	151.12
Median	620.00	00.099	620.00	620.00	700.00	390.00
Mode	700.00	700.00	700.00	700.00	700.00	700.00
Standard Deviation	456.84	458.13	456.36	457.95	36.71	585.27
Sample Variance	208701.85	209885.96	208265.48	209715.19	1347.62	342541.03
Kurtosis	0.23	0.20	0.23	0.21	4.75	-0.20
Skewness	0.73	0.63	0.73	0.72	-2.05	0.96
Coefficient of Variation	1.07	1.00	1.06	1.07	0.05	1.19
Range	1497.70	1498.40	1499.11	1499.40	110.00	1699.17
Minimum	2.30	1.60	0.89	09.0	620.00	0.83
Maximum	1500.00	1500.00	1500.00	1500.00	730.00	1700.00
Sum	6425.50	6421.90	6432.79	6408.79	4890.00	7395.93
Count	15	14	15	15	7	15
Confidence Level (95.0%)	231.19	239.98	230.95	231.75	27.19	296.18
Number of Detections Above Current Tier I SSAL	0	0	0	0	0	0
Number of Samples at 10% of Current Tier I SSAL	<b>~</b>		~	0	0	ဖ
Number of Detections Above Proposed Tier I SSAL	0	0	0	0	0	φ
Number of Detections Above Proposed Tier II SSAL	æ	œ	80	80	7	တ
Number of Non Detections	5	12	13	10	7	7
Number of Detections	2	2	2	5	0	ω

Appendix D. Summary Statistics VOC Borehole Data

		IIA				
	Carbon				Cis-12-	Methylene
	Tetrachloride	Tetrachloroethene	Trichloroethene	Chloroform <sup>a</sup>	Dichloroethene	Chloride
Descriptive Statistic	(µg/Kg)	(µg/Kg)	(μg/Kg)	(μg/Kg)	(μg/Kg)	(µg/Kg)
Mean	364.98	442.00	359.40	364 50	807.84	20.00
Geometric Mean	51.34	55.69	51.57	41.62	727.16	403.93
Standard Error	46.47	80.96	46.19	46.51	118.05	40.12
Median	6.25	56.35	6.80	6.25	200.007	36.03 13.85
Mode	5.30	700.00	5.30	700.00	200.007	5.30
Standard Deviation	430.96	750.84	428.33	431.29	656.46	519.60
Sample Variance	185726.80	563753.37	183468.61	186010.08	430940.22	269980.52
Kurtosis	-0.33	37.87	-0.23	-0.34	31.79	-0.16
Skewness	0.79	5.21	0.83	0.79	5.63	1.03
Coefficient of Variation	1.18	1.70	1.19	1.18	0.81	129
Range	1497.70	6099.22	1499.11	1499.40	3790.00	1699.41
Minimum	2.30	0.78	0.89	0.60	610,00	0.59
Maximum	1500.00	6100.00	1500.00	1500.00	4400.00	1700.00
Sum	31388.10	38011.87	30908.19	31355.07	25850.00	34739.73
Count	86	86	98	86	32	86
Confidence Level (95.0%)	91.08	158.69	90.53	91.15	227.45	109.82
Number of Detections Above Proposed Tier I SSAL	0	-	0	0	0	10
Number of Detections Above Proposed Tier II SSAL	0	7	-	0	. —	2 %
Number of Non Detections	83	29	79	74	31	43
Number of Detections	က	19	7	12		43
Number of DLs Above Proposed Tier I <sup>b</sup> SSAL	0	0	0	0	0	. 2
Number of DLs Above Proposed Tier II <sup>b</sup> SSAL	39	37	38	39	31	24
a Donotos that analyte has been smitted as a COC dies to defend and the fact the	the detection of	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				

<sup>&</sup>lt;sup>a</sup> Denotes that analyte has been omitted as a COC due to detections in the laboratory blanks

<sup>&</sup>lt;sup>b</sup> Includes only non detections DL Detection Limit

Characterization Report for the	Document Number:	RF/RMRS-99-427.UN
903 Drum Storage Area,	Revision:	0
903 Lip Area, and Americium Zone	Date:	September 28, 1999
•	Page:	E-1

### Appendix E

Electronic Copy of Analytical Database
Electronic Copy of RFCA Tier I and Tier II RSAL Calculation Results

_ <del></del>	<del> </del>	<del></del>			<del>r</del>			<u> </u>	
	İ					95% UCL	95% UCL	Best Fit	Best Fit
					1	Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 001	2086660		0.21	3.63			118.61	5.50	10.18
STAKE 002	2086695	749530.9	0.21	3.58		17.03	128.53	7.43	22.59
STAKE 003	2086678	749501.1	0.20	3.51	0.81	15.36	118.31	5.45	9.80
STAKE 004	2086713		0.19	3.45	1		136.56	8.97	32.54
STAKE 005	2086732	749533.8	0.21	3.60		16.42	124.77	6.70	17.90
STAKE 006	2086749	749506.3	0.07	2.15		19.91	146.20	10.80	44.36
STAKE 007	2086762	749535.7	0.20	3.57	3.57	18.28	136.18	8.90	32.08
STAKE 008	2086781	749506.7	0.14	3.45		20.45	149.54	11.43	48.44
STAKE 009	2086800	749538.2	0.23	4.05		19.32	142.59	10.12	39.96
STAKE 010	2086819	749508.7	0.23	4.04		20.59	150.44	11.60	49.53
STAKE 011	2086833	749539.6	0.23	3.99		17.54	131.64	8.02	26.46
STAKE 012	2086852	749510.9	0.23	3.99		19.89	146.11	10.78	44.26
STAKE 013	2086871	749541.2	0.22	4.01	4.11	18.86	139.75	9.58	36.48
STAKE 014	2086887	749514.3	0.21	3.79	<del></del>	21.23	154.38	12.34	54.30
STAKE 015	2086903	749545.9	0.22	3.96		19.99	146.71	10.90	45.00
STAKE 016	2086920	749517.6	0.22	3.87	5.90	20.78	151.60	11.82	50.94
STAKE 017	2086937	749548.9	0.23	3.98	2.73	17.39	130.68	7.84	25.27
STAKE 018	2086957	749519	0.22	3.94		19.69	144.88	10.55	42.76
STAKE 019	2086975	749548.2	0.13	3.97	3.32	18.02	134.55	8.58	30.07
STAKE 020	2086991	749523.1	0.21	3.86		18.90	140.00	9.62	36.78
STAKE 021	2087007	749551.7	0.22	3.96		18.41	136.98	9.05	33.07
STAKE 022	2087025	749523.7	0.22	3.84		19.64	144.53	10.48	42.33
STAKE 023	2087041	749553.6	0.23	3.96		19.03	140.77	9.77	37.72
STAKE 024	2087061	749527.8	0.21	3.67	6.01	20.89	152.31	11.95	51.80
STAKE 025	2087074	749557.9	0.22	3.83		18.04	134.72	8.62	30.27
STAKE 026	2087094	749529.5	0.22	3.89	3.74	18.46	137.27	9.10	33.42
STAKE 027	2087112	749557.1	0.23	3.89	2.40	17.04	128.59	7.44	22.67
STAKE 028	2087129	749532.5	0.22	3.93	1.57	16.16	123.17	6.39	15.90
STAKE 029	2087146	749562.2	0.22	4.00	3.37	18.07	134.87	8.64	30.46
STAKE 030	2087180	749564.8	0.22	3.81	1.11	15.67	120.20	5.81	12.17
STAKE 031	2087046	749494.7	0.22	3.98	1.02	15.58	119.64	5.71	11.47
STAKE 032	2087011	749491.9	0.21	3.90	7.38	22.37	161.50	13.66	62.88
STAKE 033	2086977	749489.9	0.22	3.97	8.89	24.01	171.70	15.55	75.05
STAKE 034		749488.6	0.21	3.91		23.16	166.44		68.80
STAKE 035	2086908		0.23	3.97		23.05	165.72	14.45	67.94
STAKE 036	2086874	749483.4	0.21	3.85		24.36	173.92	15.96	77.69
STAKE 037	2086838	749480.7	0.22	4.06		21.66	157.09	12.84	57.58
STAKE 038	2086802	749478.1	0.21	3.84		22.22	160.54	13.49	61.73
STAKE 039	2086769	749476	0.22	3.97		20.24	148.26	11.19	46.88
STAKE 040	2086733		0.23	4.03		16.01	122.27	6.22	14.77
STAKE 041	2086699	749471.9	0.21	3.74		15.46	118.89	5.56	10.53
STAKE 043	2086685	749441.6	0.22	3.95		<del></del>	166.93	14.67	69.38
STAKE 044	2086719		0.21	3.75		22.81	164.26	14.18	66.19
STAKE 045	2086753			3.94		23.60	169.18	15.08	72.05
STAKE 046	2086789		0.23	4.04		27.70	194.96	19.77	102.33
STAKE 047	2086822	749449.3		3.90			167.33	14.74	69.86
STAKE 048	2086858	<b>-</b>		3.73			230.28	26.00	142.58
STAKE 049	2086892	749454.6		2.89			239.23	27.55	152.56
STAKE 050	2086923			3.96			182.16	17.46	87.40
STAKE 051	2086958			3.99			145.98	10.76	44.11
STAKE 052	2086875				<del></del>		119.27	5.63	11.00

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1		,			]	0.50( 115:	000/ 110/		
						95% UCL	95% UCL	Best Fit	Best Fit
OTAKE AND ADED						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 053	2086840		0.22	4.02	4.000	15.63	119.95	5.76	11.86
STAKE 054	2086803		0.23	4.08		18.65	138.44	9.33	34.85
STAKE 055	2086685	749285.1	0.22	3.88		15.55	119.43	5.66	11.21
STAKE 056	2086717	749291.1	0.23	4.02	1.81	16.41	124.72	6.69	17.84
STAKE 057	2086752	749296.6	0.24	4.07	1.06	15.62	119.90	5.76	11.80
STAKE 058	2086787	749306.1	0.22	4.11	2.18	16.81	127.14	7.16	20.86
STAKE 059	2086822	749313.2	0.23	3.94	3.14	17.83	133.40	8.36	28.64
STAKE 060	2086856	749321	0.22	3.89		20.35	148.94	11.32	47.71
STAKE 061	2086887	749330	0.23	3.87	8.30	23.36	167.69	14.81	70.28
STAKE 062	2086920	749342.4	0.23	3.84	6.09	20.98	152.88	12.06	52.49
STAKE 063	2086949	749356.8	0.21	3.72	3.95	18.69	138.70	9.38	35.18
STAKE 064	2086981	749367.5	0.22	3.81	7.92	22.96	165.13	14.34	67.24
STAKE 065	2087013	749380.5	0.22	3.81	6.52	21.45	155.74	12.59	55.95
STAKE 066	2087045	749396.4	0.20	3.57	6.24	21.14	153.84	12.24	53.66
STAKE 067	2086650	749284.9	0.21	3.74	0.89	15.44	118.80	5.54	10.41
STAKE 068	2086616	749278	0.22	3.95		16.16	123.19	6.39	15.92
STAKE 069	2086581	749276.9	0.25	4.30	0.95	15.51	119.18	5.62	10.90
STAKE 070	2086547	749274.8	0.22	3.89	0.88	15.43	118.74	5.53	10.34
STAKE 071	2086435	748842.5	0.28	4.52	1.03	15.59	119.68	5.71	11.52
STAKE 072	2086466	748834.5	0.25	4.17	0.66	15.21	117.36	5.26	8.60
STAKE 073	2086499	748825.2	0.27	4.55	1.06	15.62	119.90	5.75	11.79
STAKE 074	2086534	748821.3	0.28	4.62	1.59	16.19	123.34	6.42	16.11
STAKE 075	2086568	748816.2	0.25	4.32	1.10	15.67	120.16	5.81	12.13
STAKE 076	2086602	748813.4	0.27	4.52	3.02	17.70	132.60	8.21	27.65
STAKE 077	2086445	748809.3	0.23	4.05	8.31	23.38	167.81	14.83	70.42
STAKE 078	2086476	748799.3	0.23	3.94	21.19	37.72	259.10	30.94	174.44
STAKE 079	2086512	748793.8	0.25	4.43	22.58	39.32	269.46	32.68	185.69
STAKE 080	2086547	748787.8	0.27	4.76	18.53	34.70	239.56	27.61	152.93
STAKE 081	2086581	748786.5	0.31	5.80	28.12	45.75	311.60	39.61	230.46
STAKE 082	2086615	748782.2	0.34	6.07	25.08	42.20	288.26	35.80	205.86
STAKE 083	2086637	748807.5	0.33	5.88	7.05	22.02	159.30	13.26	60.24
STAKE 084	2086650	748778.6	0.33	5.99	15.75	31.57	219.53	24.13	130.48
STAKE 085	2086671	748803.8	0.29	4.85	6.27	21.17	154.01	12.27	53.86
STAKE 086	2086682					31.98	222.16	24.59	133.45
STAKE 087	2086706				<u> </u>	23.66	169.53	15.15	72.48
STAKE 088	2086718		0.28	5.28		32.17	223.37	24.80	134.81
STAKE 089	2086743		0.30			19.89	146.10	10.78	44.25
STAKE 090	2086755	748763.4	0.31	5.51	14.37	30.04	209.73	22.40	119.33
STAKE 091	2086776	748789	0.30	5.48	3.87	18.60	138.16	9.27	34.51
STAKE 092	2086788	748758.4	0.32	5.78	12.22	27.65	194.62	19.71	101.95
STAKE 093	2086812		0.31			15.99	122.14	6.19	14.61
STAKE 094	2086822	748753.5	0.28			29.66	207.32	21.98	116.58
STAKE 095	2086844		0.30			15.95	121.91	6.15	14.32
STAKE 096	2086858		0.31	5.75		25.08	178.43	16.78	83.01
STAKE 097	2086892		0.34			20.80	151.73	11.84	
STAKE 098	2086452	748776.1	0.26		477	52.53	356.73	46.77	276.72
STAKE 099	2086431	748749.9	0.32			51.16	347.52	45.33	
STAKE 100	2086467	748745.1	0.24			36.83	253.31	29.96	168.10
STAKE 1000	2085697	748599	0.23	4.31	0.61	15.15	117.02	5.19	8.17
STAKE 1001	2085713		0.21			16.56	125.62	6.86	
STAKE 1002	2085666	748594.5	0.22	4.12	1.09	15.66	120.13	5.80	12.08

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					)  -	95% UCL	95% UCL	Best Fit	Best Fit
	1			i		Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 1003	2085683		0.20	3.61	1.14	15.71	120.42	5.86	12.45
STAKE 1004	2085630	748595	0.22	4.03		15.57	119.60	5.70	11.42
STAKE 1005	2085646		0.21	3.72		15.43	118.70		10.29
STAKE 1006	2085597	748595	0.23	4.19		15.65	120.07	5.79	12.02
STAKE 1007	2085614	748566.8	0.22	3.82		15.43	118.76	5.53	10.36
STAKE 1008	2086111	748894.1	0.13	4.76		52.56	356.93	46.80	276.93
STAKE 1009	2086143	748893.3	0.21	4.03		26.09	184.78	17.94	90.48
STAKE 101	2086487	748769.4	0.28	5.12		35.13	242.34	28.08	156.02
STAKE 1010	2086125	748865.1	0.26	4.81	7.70	22.72	163.67	14.07	65.48
STAKE 1011	2086157	748865.8	0.22	3.98		23.17	166.47	14.59	68.83
STAKE 1012	2085795	748647.8	0.38	6.91	3.07	17.75	132.90	8.27	28.02
STAKE 1013	2085762	748642.8	0.14	3.64		16.24	123.69	6.49	16.56
STAKE 1014	2085723	748644.1	0.18	3.33	le	16.06	122.54	6.27	15.11
STAKE 1015	2085708	748673.8	0.17	3.22	3.22	17.91	133.91	8.46	29.27
STAKE 1016	2085739	748668	0.20	3.55		19.87	145.97	10.75	44.09
STAKE 1017	2085770	748672.1	0.20	3.56		15.46	118.91	5.56	10.55
STAKE 1018	2085792	748696.5	0.20	3.66		24.81	176.75		81.03
STAKE 1019	2085826	748700	0.22	3.94	24.20	41.18	281.62	34.70	198.78
STAKE 102	2086502	748741.8	0.27	4.71	23.62	40.52	277.27	33.98	194.11
STAKE 1020	2085859	748697.4	0.23	4.13		18.62	138.29	9.30	34.68
STAKE 1021	2085882	748720.2	0.24	4.31	12.18	27.61	194.36		101.65
STAKE 1022	2085893		0.23	4.07	3.18	17.87	133.67	8.41	28.97
STAKE 1023	2085812	748619.4	0.58	11.35	i	19.24	142.07	10.02	39.32
STAKE 1024	2085778	748615.9	0.28	6.17	1.86	16.47	125.05	6.76	18.26
STAKE 1025	2086291	748451.1	0.24	4.27	9.87	25.07	178.39	16.77	82.96
STAKE 1026	2087595	748909.5	0.18	3.72	1.19	15.76	120.73	5.92	12.84
STAKE 1027	2087576	748843.8	0.20	3.61	0.92	15.47	118.99	5.58	10.66
STAKE 1028	2087555	748862.8	0.24	4.24	1.05	15.61	119.83		11.71
STAKE 1029	2087502	748883.8	0.22	4.15	L	23.10	166.03	14.50	68.30
STAKE 103	2086525	748762.9	0.30	5.46		45.14	307.62	38.96	226.29
STAKE 1030	2087545	748833	0.19	3.60	L	15.53	119.31	5.64	11.06
STAKE 1031	2087509	748828.5	0.24	4.73	6.48	21.40	155.48	12.54	55.63
STAKE 1032	2087410	748801.9	0.22	3.95		22.83	164.37	14.20	66.32
STAKE 1033	2087400		0.25	4.56		23.31	167.37		69.91
STAKE 1034	2087381		0.22	3.88		19.28	142.34		39.65
STAKE 1035	2087370		0.25	4.55		20.48	149.73		48.66
STAKE 1036	2087438		0.22	4.00		22.24	160.69	13.51	61.91
STAKE 1037	2087145		0.22	4.06		15.98	122.10		14.57
STAKE 1038	2087123		0.27	4.81		22.00	159.20		60.12
STAKE 1039	2087139		0.23	4.10	<del></del>	16.83	127.28	7.19	21.04
STAKE 104	2086541		0.27	4.82		30.21	210.83		120.59
STAKE 1040	2087113		0.28	5.02		17.16	129.29		23.55
STAKE 1041	2087064			5.68			122.02	6.17	14.46
STAKE 1042	2087066		0.31	5.44		15.90	121.58	6.08	13.91
STAKE 1043	2087044		0.29	5.15			121.36		
STAKE 1044	2087012		0.27	4.96	4	15.78	120.88	5.95	
STAKE 1045	2087035	<del></del>	0.23				118.82		
STAKE 1046	2087009		0.27	4.71			120.10		
STAKE 1047	2086986		0.28				119.86		<del></del>
STAKE 1048	2086983						120.43		
STAKE 1049	2086958						119.59		<del></del>

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 105	2086562	748756.4	0.15	5.84		38.65	265.10	31.95	180.97
STAKE 1050	2086937	748759.9	0.25	4.59		15.71	120.45	5.86	12.49
STAKE 1051	2086967	748789.4	0.23	4.17	2.72	17.38	130.63	7.83	25.21
STAKE 1052	2086945	748784.8	0.27	4.91	8.73	23.84	170.63	15.35	73.79
STAKE 1053	2086986	748804.4	0.22	3.90	0.92	15.47	119.00	5.58	10.66
STAKE 1054	2087013	748807.7	0.24	4.54	1.56	16.15	123.11	6.38	15.83
STAKE 1055	2087420	749317.3	0.13	3.98	7.14	22.11	159.88	13.36	60.94
STAKE 1056	2087479	749229.9	0.14	3.63		26.34	186.34	18.22	92.31
STAKE 1057	2087513	749232.3	0.10	3.96		22.69	163.49	14.03	65.27
STAKE 1058	2087463	749198.1	0.27	4.69		15.75	120.69	5.91	12.79
STAKE 1059	2087498	749199.8	0.20	3.79		15.75	120.71	5.91	12.81
STAKE 106	2086577	748729.4	0.29	5.52	18.03	34.14	235.94	26.98	148.91
STAKE 1060	2087545	749234.6	0.09	3.94	8.91	24.03	171.82	15.57	75.20
STAKE 1061	2087534	749204.5	0.28	3.63		29.34	205.30	21.62	114.26
STAKE 1062	2087519	749171.7	0.21	3.89		16.49	125.19	6.78	18.42
STAKE 1063	2087567	749205.1	0.20	3.64	11.78	27.17	191.61	19.17	98.45
STAKE 1064	2087554	749177.4	0.20	3.80	11.54	26.91	189.94	18.87	96.51
STAKE 1065	2087585	749178.1	0.19	3.55		19.17	141.65	9.94	38.81
STAKE 1066	2087601	749207.2	0.26	4.54	1.16	15.73	120.54	5.88	12.60
STAKE 1067	2087635	749209.9	0.25	4.53	1.15	15.72	120.48	5.87	12.53
STAKE 1068	2087580	749236.5	0.14	4.05		18.40	136.93	9.04	33.00
STAKE 1069	2087620	749181.2	0.15	4.18	0.92	15.47	118.99	5.58	10.66
STAKE 107	2086597	748755.9	0.30	5.14	16.28	32.17	223.33	24.79	134.77
STAKE 1070	2087591	749270.4	0.24	4.39	1.13	15.70	120.35	5.84	12.37
STAKE 1071	2087612	749240.7	0.27	4.81	1.21	15.78	120.86	5.94	13.01
STAKE 1072	2087604	749154	0.23	3.92	0.90	15.46	118.91	5.56	10.55
STAKE 1073	2087559	749267	0.19	4.07	7.20	22.18	160.29	13.44	61.43
STAKE 1074	2087574	749152.5	0.09	3.48	1.38	15.96	121.97	6.16	14.40
STAKE 1075	2087525	749264.8	0.11	3.67	6.93	21.89	158.47	13.10	59.24
STAKE 1076	2087505	749291.6	0.20	3.59	9.26	24.41	174.24	16.01	78.06
STAKE 1077	2087540	749146.7	0.23	4.19	1.11	15.68	120.24	5.82	12.23
STAKE 1078	2087506	749141.1	0.24	4.40	1.18	15.75	120.66	5.90	12.75
STAKE 1079	2087592	749126.4	0.16	3.99	0.89	15.44	118.81	5.54	10.42
STAKE 108	2086609	748724.3	0.29	5.44		32.31	224.22	24.95	135.77
STAKE 1080	2086739		0.13			17.23	129.76	7.66	24.12
STAKE 1081	2086771	749416.7	0.23			15.47	118.99	5.58	10.65
STAKE 1082	2086755	749388.1	0.21	3.83	****	15.46	118.91	5.56	10.56
STAKE 1083	2086785		0.23			15.69	120.32	5.84	12.32
STAKE 1084	2086824					15.40	118.54	5.49	10.09
STAKE 1085	2086855		0.24	4.34		15.66	120.11	5.80	12.06
STAKE 1086	2086911		0.15			15.40	118.55	5.49	10.09
STAKE 1087	2086941	749429.4	0.23				120.12	5.80	12.08
STAKE 1088	2086978		0.21	3.65		15.40	118.53	5.49	10.07
STAKE 1089	2086994		0.23			16.34	124.29	6.61	17.30
STAKE 109	2086631		0.29			28.70	201.28	20.90	109.64
STAKE 1090	2087045		0.18		1	21.56	156.42	12.72	56.77
STAKE 1091	2087075		0.21	3.88		25.88	183.44	17.69	88.90
STAKE 1092	2087105		0.17	3.37		17.82	133.37	8.36	28.60
STAKE 1093	2087136	749446.2	0.19	3.51		19.10	141.26	9.86	38.32
STAKE 1094	2087166	749463.6	0.17	3.08		17.03	128.51	7.42	22.57
STAKE 1095	2087194	749482.1	0.19	3.50	1.01	15.57	119.58	5.69	11.40

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 1096	2087226	749500.9	0.18			17.25	129.83	7.68	24.21
STAKE 1097	2087255	749520.7	0.21	3.78	L	15.82	121.08	5.99	13.29
STAKE 1098	2087562	749114.9	0.18	3,46		15.33	118.10	5.40	9.53
STAKE 1099	2086602	749205.9	0.23	4.37		35.90	247.29	28.93	161.49
STAKE 110	2086642	748719.7	0.30			30.55	213.01	22.98	123.07
STAKE 1100	2086592	749179	0.22	3.83		27.57	194.13	19.62	101.37
STAKE 1101	2086570	749203.2	0.27	4.66		15.57	119.61	5.70	11.43
STAKE 1102	2086560	749176.4	0.24			15.54	119.39	5.66	11.16
STAKE 1103	2086577	749146.6	0.23		Luc-	27.12	191.28	19.11	98.07
STAKE 1104	2086552	749145.3	0.22	3.94		18.43	137.10	9.07	33.22
STAKE 1105	2086522	749021.2	0.19			58.02	393.68	52.46	313.45
STAKE 1106	2086516	749271.9	0.11	3.47	0.83	15.38	118.42	5.47	9.94
STAKE 1107	2086516	749240.8	0.22	3.91	0.99	15.55	119.47	5.67	11.26
STAKE 1108	2086516	749205.3	0.20	3.60	0.82	15.37	118.38	5.46	9.88
STAKE 1109	2086513	749174.3	0.23	4.25		35.22	242.92	28.18	156.65
STAKE 111	2086664	748744.5	0.30	5.07	12.47	27.93	196.37	20.03	103.97
STAKE 1110	2086511	749138.3	0.17	3.75		35.21	242.88	28.18	156.61
STAKE 1111	2086509	749107.3	0.24	4.40	23.80	40.72	278.61	34.20	195.54
STAKE 112	2086678	748714.9	0.27	5.13	14.98	30.72	214.10	23.18	124.31
STAKE 113	2086697	748740.3	0.26	4.72	14.19	29.84	208.48	22.18	117.90
STAKE 114	2086708	748710.7	0.27	5.01	11.66	27.04	190.76	19.02	97.46
STAKE 115	2086732	748735.7	0.25	4.52	13.58	29.16	204.17	21.42	112.97
STAKE 116	2086744	748704.7	0.29	5.34	13.23	28.77	201.69	20.98	110.11
STAKE 117	2086764	748729.3	0.27	4.67	10.69	25.98	184.07	17.81	89.65
STAKE 118	2086777	748697.7	0.28	5.07	11.37	26.72	188.72	18.65	95.08
STAKE 119	2086795	748724.3	0.25	4.48	10.82	26.12	184.97	17.97	90.70
STAKE 120	2086815	748696	0.29	5.24	9.94	25.15	178.86	16.86	83.53
STAKE 121	2086856	748655.2	0.28	5.13	12.94	28.45	199.65	20.61	107.76
STAKE 122	2086836	748630.6	0.26	4.57	10.69	25.97	184.02	17.80	89.59
STAKE 123	2086825	748663.2	0.29	3.96	9.81	25.01	177.98	16.70	82.48
STAKE 124	2086805	748637.8	0.26	4.63	10.83	26.12	184.99	17.97	90.72
STAKE 125	2086792	748669.6	0.22	5.43	11.35	26.70	188.58	18.63	94.92
STAKE 126	2086770	748641.1	0.27	4.60	10.18	25.42	180.56	17.17	85.52
STAKE 127	2086757	748672.9	0.28	4.92	11.40	26.76	188.97	18.69	95.37
STAKE 128	2086733	748648.3	0.25	5.29	13.50	29.08	203.64	21.32	112.35
STAKE 129	2086724	748670.7	0.27	4.74	12.21	27.64	194.57	19.70	101.88
STAKE 130	2086704	748651.7	0.31	5.58	13.75	29.34	205.33	21.63	114.30
STAKE 131	2086693	748680.9	0.27	5.01	10.02	25.24	179.44	16.97	84.21
STAKE 132	2086664	748663.1	0.24	4.37	6.41	21.32	154.98	12.45	55.03
STAKE 133	2086655	748689.4	0.29	5.40	15.60	31.40	218.45	23.94	129.26
STAKE 134	2086635	748659.4	0.29	5.41	18.31	34.46	238.01	27.34	151.21
STAKE 135	2086622	748692.3	0.28	5.28	17.58	33.63	232.70	26.42	145.29
STAKE 136	2086601	748663.8	0.23	4.21	8.61	23.71	169.82	15.20	72.82
STAKE 137	2086587	748694.8	0.27	5.12	16.92	32.89	227.95	25.60	139.96
STAKE 138	2086567	748671.2	0.23	4.05	9.34	24.50	174.80	16.12	78.73
STAKE 139	2086555	748700.2	0.29	5.39	19.08	35.32	243.59	28.30	157.40
STAKE 140	2086535	748675.3	0.25	4.37	15.55	31.35	218.13	23.88	128.89
STAKE 141	2086519	748704.7	0.31	5.78	19.84	36.19	249.16	29.25	163.54
STAKE 142	2086492	748681.3	0.25		16.31	32.20	223.56	24.83	135.02
STAKE 143	2086476	748712.7	0.21	6.02	27.69	45.24	308.25	39.07	226.95
STAKE 144	2086456	748686.7	0.28	4.76	12.48	27.94	196.44	20.04	104.05

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						95% UCL	95% UCL	Best Fit	Best Fit
			'		1	Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 145	2086444		0.33			46.43	316.13	40.34	235.18
STAKE 146	2086423		0.26			37.27	256.19	30.44	171.26
STAKE 147	2086410		0.31	5.72	1	47.46	322.95	41.43	242.25
STAKE 148	2086391	748696.5	0.24	4.36		39.51	270.70	32.89	187.04
STAKE 149	2086380	748639.9	0.28	5.19	18.13	34.25	236.66	27.11	149.70
STAKE 150	2086401	748664.6	0.24			41.48	283.54	35.02	200.82
STAKE 1500	2086365	748671.9	0.27	5.08	24.86	41.95	286.63	35.53	204.12
STAKE 151	2086413	748635.1	0.27	4.96		45.72	311.40	39.58	230.24
STAKE 152	2086433	748657.6	0.24	4.36		36.28	249.79	29.36	164.23
STAKE 153	2086446	748627.7	0.27	5.18		43.20	294.84	36.88	212.84
STAKE 154	2086465	748652.4	0.25	4.43		29.28	204.95	21.56	113.86
STAKE 155	2086478	748623.1	0.27	5.12		34.28	236.85	27.14	149.92
STAKE 156	2086500	748646.9	0.25	4.35	15.67	31.49	219.01	24.04	129.89
STAKE 157	2086518	748617.2	0.27	5.15	13.99	29.61	207.05	21.93	116.27
STAKE 158	2086542	748641.8	0.25	4,40		26.44	186.98	18.34	93.05
STAKE 159	2086553	748612.4	0.28	5.38	15.33	31.10	216.52	23.60	127.07
STAKE 160	2086578	748634.3	0.25	4.32	10.68	25.96	183.95	17.79	89.50
STAKE 161	2086595	748606.5	0.26	4.66	9.18	24.32	173.68	15.91	77.40
STAKE 162	2086613	748633.7	0.28	5.36	19.59	35.90	247.32	28.94	161.52
STAKE 163	2086628	748601.8	0.27	4.66	6.08	20.97	152.79	12.04	52.38
STAKE 164	2086645	748626.2	0.30	5.63	8.32	23.39	167.87	14.84	70.51
STAKE 165	2086659	748597.8	0.31	5.82	6.17	21.06	153.37	12.15	53.08
STAKE 166	2086680	748625.2	0.11	4.63	11.85	27.25	192.06	19.25	98.97
STAKE 167	2086690	748595.2	0.18	5.60	12.00	27.42	193.14	19.45	100.22
STAKE 168	2086713	748621.3	0.22	3.90	10.04	25.26	179.57	16.99	84.36
STAKE 169	2086725	748587.9	0.30	5.47	8.85	23.96	171.43	15.50	74.74
STAKE 170	2086746	748613.4	0.22	4.03	10.14	25.37	180.27	17.12	85.18
STAKE 171	2086351	748643.1	0.28	5.05	21.60	38.19	262.13	31.45	177.74
STAKE 172	2086356	748611.7	0.28	5.38	29.50	47.37	322.30	41.33	241.58
STAKE 173	2086391	748606.3	0.27	4.64	23.09	39.91	273.30	33.32	189.84
STAKE 174	2086368	748580.8	0.30	5.58	19.95	36.31	249.98	29.39	164.44
STAKE 175	2086421	748599.4	0.26	4.53	16.15	32.03	222.44	24.64	133.76
STAKE 176	2086401	748574.2	0.31	5.62	16.78	32.73	226.92	25.42	138.81
STAKE 177	2086456	748595.6	0.26	4.65	10.13	25.36	180.17	17.10	85.07
STAKE 178	2086437	748569.2	0.30			35.57	245.20	28.57	159.18
STAKE 179	2086494		0.25			26.63	188.16	18.55	94.43
STAKE 180	2086470	748566.5	0.18			31.28	217.63	23.80	128.33
STAKE 181	2086531	748585.8	0.27		<del></del>	29.18	204.33	21.45	113.14
STAKE 182	2086508	748560.7	0.30	1		30.66	213.71	23.11	123.87
STAKE 183	2086569		0.28			25.19		16.91	83.81
STAKE 184	2086546		0.31		13.81	29.41	205.76	21.70	114.79
STAKE 185	2086604		0.29			26.44	186.99	18.34	93.06
STAKE 186	2086582		0.32			29.94	209.11	22.29	118.62
STAKE 187	2086638	-	0.29			26.46	187.12	18.36	93.21
STAKE 188	2086618		0.29			28.55	200.29	20.73	
STAKE 189	2086668		0.21			25.15	178.88	16.86	
STAKE 190	2086649		0.29		1	29.05	203.50	21.30	112.20
STAKE 191	2086709		0.26			21.89	158.51	13.11	59.28
STAKE 192	2086688		0.32			30.10	210.11	22.47	
STAKE 193	2086741	748555.5	0.29		<del> </del>	25.84	183.21	17.65	1
STAKE 194	2086720	748524	0.29	5.26	8.17	23.23	166.82	14.65	69.25

						05% UC	059/ 1101	Doot Fit	Doot Fit
						95% UCL	95% UCL Predicted	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Predicted Am-241	Pu-239/240	Predicted Am-241	Predicted Pu-239/240
STAKE NOMBER	2086801	748492.8	0.31	5.63		25.08	178.41	16.78	83.00
STAKE 196	2086755		0.31	5.45		25.74	182.56	17.53	87.87
STAKE 190	2086782	748464.8	0.12	4.83		21.49	156.00	17.53	56.26
STAKE 197	2086786	748404.8	0.27	5.10	9.03	24.16	172.67	15.73	76.21
STAKE 199	2086767	748320.9	0.32	5.10	6.21	21.11	153.64	12.20	53.42
STAKE 199	2086749	748471.8	0.31	4.59	7.55	22.55	162.63	13.87	64.24
STAKE 200	2086735	748471.8	0.27	5.51	9.71	24.90	177.33	16.58	81.72
STAKE 201	2086733	748473.5	0.30	4.28	8.62	23.72	169.91	15.22	72.93
STAKE 202 STAKE 203	2086699	748503.2	0.24	4.26	8.66	23.76	170.18	15.22	73.25
STAKE 203	2086676	748478.5	0.25	4.90	7.00	21.96	158.95	13.19	59.81
STAKE 204	2086661	748509.6	0.29	5.11	8.05	23.10	166.04	14.51	68.32
STAKE 205	2086643	748309.0	0.29	4.29	7.14	22.11	159.88	13.36	60.94
STAKE 200	2086631	748515.1	0.24	5.20	11.16	26.49	187.30	18.39	93.43
STAKE 207	2086606	748313.1	0.26	4.67	7.15	22.13	159.97	13.38	61.05
STAKE 200	2086594	748523.8	0.26	4.99	10.93	26.24	185.70	18.10	91.55
STAKE 210	2086571	748498	0.24	4.31	9.37	24.53	174.97	16.15	78.93
STAKE 210	2086558	748524.6	0.24	5.73	13.84	29.45	206.00	21.74	115.07
STAKE 211	2086539	748324.0	0.31	4.57	10.01	25.23	179.40	16.96	84.15
STAKE 212 STAKE 213	2086524	748529.1	0.10	5.71	11.11	26.43	186.94	18.33	93.00
STAKE 213	2086500	748505.3	0.30	4.72	11.01	26.43	186.28	18.21	92.23
STAKE 214 STAKE 215	2086488	748536.7	0.27	5.64	10.46	25.72	182.47	17.52	87.76
STAKE 216	2086464	748530.7	0.31	4.42	10.40	26.21	185.55	18.08	91.38
STAKE 217	2086451	748540	0.20	5.50	15.85	31.69	220.28	24.26	131.32
STAKE 217	2086431	748517.5	0.24	4.27	9.44	24.60	175.44	16.24	79.48
STAKE 219	2086418	748546.4	0.29	5.43	16.84	32.79	227.33	25.49	139.27
STAKE 219	2086397	748522.2	0.24	4.33	12.90	28.41	199.41	20.57	107.48
STAKE 221	2086382	748549.2	0.25	4.38	13.40	28.96	202.89	21.19	111.50
STAKE 222	2086364	748528.3	0.28	5.24	18.72	34.92	240.97	27.85	154.50
STAKE 223	2086348	748553.6	0.26	4.54	18.37	34.53	238.46	27.42	151.70
STAKE 224	2086328	748530.6	0.29	5.46	14.34	30.01	209.56	22.37	119.14
STAKE 225	2086342	748498.9	0.27	4.62	8.98	24.11	172.35	15.67	75.83
STAKE 226	2086316	748476.1	0.32	5.97	15.54	31.35	218.08	23.88	128.84
STAKE 227	2086371	748492.9	0.32	4.10	10.52	25.78	182.85	17.59	88.21
STAKE 228	2086352		0.24	5.81	14.83	30.55	212.99	22.98	123.05
STAKE 229	2086407	748487.9	0.23	4.00		24.02	171.80	15.57	75.18
STAKE 230	2086389		0.29	5.53		28.09	197.39	20.21	105.15
STAKE 231	2086440		0.22	3.97	7.85	22.88	164.69	14.26	66.71
STAKE 232	2086421	748459.8	0.45	5.84		29.99	209.44	22.35	119.00
STAKE 233	2086476		0.23			24.17	172.71	15.73	76.25
STAKE 234	2086455		0.33			30.29	211.38	22.70	121.22
STAKE 235	2086511	748471.3	0.24		<del></del>	21.45	155.75	12.59	55.96
STAKE 236	2086490		0.32	5.88		25.96	183.94	17.78	89.49
STAKE 237	2086548		0.24			22.33	161.23	13.61	62.56
STAKE 238	2086526		0.28			21.85	158.24	13.06	58.97
STAKE 239	2086584		0.25				172.80	15.75	
STAKE 240	2086559		0.28			20.38	149.15	11.36	-
STAKE 241	2086326		0.28			24.73	176.22	16.38	
STAKE 242	2086306		0.23			21.78	157.81	12.98	
STAKE 243	2086362	748437.4	0.28		+	22.15	160.10	13.40	
STAKE 244	2086340		0.30			20.33	148.82	11.29	
STAKE 245	2086396		0.26				163.26	13.99	

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						050/ 1101	050/ 1101	D ( E)	D4 E''
						95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Footing	Northing	11.005	11.000	A 0.44	Predicted	Predicted	Predicted	Predicted
STAKE NOWBER	Easting 2086373	Northing 748405.9	U-235 0.29	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 247	2086321	748618.4	0.29	5.43	8.51	23.60	169.14	15.08	72.01
STAKE 247	2086289		0.22	4.88	1.11	15.68	120.26	5.82	12.25
STAKE 249	2086328		0.29	5.41	23.43	40.30	275.83	33.74	192.56
STAKE 250	2086299		0.26	4.54	19.29	35.56	245.11	28.56	159.08
STAKE 250 STAKE 251	2086299	748559.9	0.32	5.64 4.90	1.41 2.69	15.99	122.15	6.19	14.63
STAKE 251	2086279	748568.9	0.17		15.80	17.35 31.63	130.44 219.90	7.80	24.97
STAKE 252 STAKE 253	2086267	748599		5.55 4.68				24.19	130.90
STAKE 253	2086245	748576	0.26 0.32	5.80	18.81	35.01	241.60	27.96	155.19
STAKE 254 STAKE 255	2086286	748534.7	0.32		20.21	36.60	251.85	29.71	166.50
STAKE 256	2086256	748540.9	0.12	5.02 5.55	1.15	15.72 32.14	120.50 223.14	5.87	12.56
STAKE 250 STAKE 257	2086296		0.30	5.55 4.95	16.25		127.69	24.76	134.55
STAKE 257	2086290	748518.1			2.27	16.90 21.19		7.26	21.55
STAKE 260			0.31	5.68	6.29		154.17	12.30	54.05
STAKE 260	2086617	749237.8	0.23	4.30	2.20	16.83	127.25	7.18	21.00
STAKE 261	2086637 2086650	749211 749240.3	0.26	4.85	1.71	16.31	124.12	6.57	17.09
STAKE 262 STAKE 263		l	0.24	4.39	7.62	22.63	163.14	13.97	64.84
STAKE 263	2086671	749214	0.27	5.02	32.34	50.73	344.66	44.88	264.51
STAKE 264 STAKE 265	2086683 2086704	749245 749219.2	0.24 0.27	4.36	5.47	20.31	148.69	11.27	47.41 320.70
STAKE 266			0.27	5.06	39.29	59.12	401.09	53.58	76.89
STAKE 266	2086717	749249.5		4.34	9.11	24.25	173.24	15.83	
STAKE 267 STAKE 268	2086740 2086753	749226 749254.5	0.27	4.94	19.04	35.28	243.31	28.25	157.09 173.99
STAKE 269		749234.5	0.22	4.15 5.00	21.13	37.66 48.53	258.69	30.87 42.56	249.52
STAKE 209 STAKE 270	2086772 2086786	749258.8			30.48	40.37	330.00		193.10
STAKE 270 STAKE 271	2086806	749233.8	0.26	4.09 4.97	23.50	56,28	276.33	33.83 50.66	301.83
STAKE 271	2086823	749253.8	0.19		36.95 18.92	35.15	381.88 242.45	28.10	156.13
STAKE 272 STAKE 273	2086840	749204.5		4.11 5.02		49.71		43.81	257.57
STAKE 273			0.26 0.22	4.05	31.48 26.29	43.61	337.86	37.32	215.65
STAKE 274 STAKE 275	2086854 2086872	749268.9 749243.2	0.22	4.05	28.43	46.11	297.50 314.02	40.00	232.98
STAKE 275	2086888	749243.2	0.23	4.00	19.29	35.56	245.13	28.56	159.10
STAKE 276 STAKE 277						38.23			
STAKE 277	2086908 2086923	749248.8	0.25	4.82	21.63		262.39 222.33	31.49 24.62	178.03 133.64
STAKE 278		749277.8	0.23 0.25	4.17 4.79	16.14	32.01			126.24
STAKE 279 STAKE 280	2086942 2086955	749252.4 749282.8		4.79	15.22 15.39	30.99 31.17	215.80 216.95	23.47 23.68	127.55
STAKE 280	2086955		0.23 0.25			28.11	197.49	20.23	105.27
STAKE 281	2086989			4.39		26.63	188.16	18.55	94.42
STAKE 282	2087009		0.24 0.26	4.21		29.48	206.21	21.78	115.30
STAKE 284	2087009		0.20			31.36		23.89	128.95
STAKE 285	2087023			4.03			218.18		109.64
STAKE 286			0.25	4.68		28.70 29.74	201.28	20.90	117.19
	2087059 2087077		0.09	4.07	14.10		207.86	22.07 21.20	111.19
STAKE 287 STAKE 288		749269.7	0.26	4.77		28.97	202.96		78.20
STAKE 289	2087090 2087112		0.22	4.02		24.43 24.33	174.35 173.74	16.04	77.48
			0.25	4.91				15.92	
STAKE 290 STAKE 291	2087124 2087145		0.21 0.25	4.02 4.76		25.66 31.19	182.06 217.08	17.44 23.70	87.29 127.70
STAKE 291	2087145		0.23	4.76		24.68	175.91	16.32	80.05
STAKE 292 STAKE 293	2087178		0.23	4.60		33.19	229.87		142.12
STAKE 293 STAKE 294	2087178		0.23	4.60		21.75	157.65	25.93	
STAKE 294 STAKE 295	2087192	1					T	12.95	58.25
STAKE 295 STAKE 296			0.25	4.69		29.10	203.78	21.35	112.51
STAKE 296 STAKE 297	2087227 2087247	749317.7	0.23	4.05		19.97	146.58	10.87	44.83
OTANE 281	2007247	749292.8	0.25	4.72	12.49	27.95	196.51	20.05	104.13

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						95% UCL	95% UCL	Best Fit	Best Fit
		,				Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 298	2087260	749323.2	0.19	3.48		25.02	178.05		82.57
STAKE 299	2087281	749298.1	0.27	4.85		22.69	163.46	14.03	65.24
STAKE 300	2087293	749328.9	0.19	3.46		23.75	170.10	15.25	73.15
STAKE 301	2087314	749301.7	0.21	4.05		26.29	186.03	18.16	91.93
STAKE 302	2087327	749332.5	0.18	3.40		22.38	161.52	13.67	62.91
STAKE 303	2087349	749307.9	0.22	3.98	8.01	23.06	165.77	14.46	68.00
STAKE 304	2087362	749336.4	0.21	3.49	3.90	18.63	138.35	9.31	34.76
STAKE 305	2087381	749310.8	0.22	4.04	5.42	20.26	148.38	11.21	47.03
STAKE 306	2086872	749301.8	0.27	5.14	5.60	20.45	149.55	11.43	48.45
STAKE 307	2086905	749304.6	0.23	4.47	8.01	23.05	165.73	14.45	67.95
STAKE 308	2086937	749310.8	0.27	5.10	18.75	34.95	241.21	27.89	154.76
STAKE 309	2086967	749312.8	0.25	4.54	15.30	31.08	216.36	23.57	126.88
STAKE 310	2087002	749320.5	0.27	5.01	19.03	35.27	243.23	28.24	156.99
STAKE 311	2087015	749350.6	0.23	4.20	6.46	21.37	155.29	12.51	55.40
STAKE 312	2087036	749322.7	0.26	4.83	20.44	36.87	253.55	30.00	168.37
STAKE 313	2087051	749353.6	0.22	4.15	19.41	35.70	246.00	28.71	160.06
STAKE 314	2087071	749326.9	0.25	4.77	19.00	35.23	243.00	28.20	156.74
STAKE 315	2087084	749359.6	0.24	4.09	19.56	35.87	247.09	28.90	161.26
STAKE 316	2087104	749331.5	0.26	4.90	19.53	35.84	246.90	28.86	161.06
STAKE 317	2087119	749362.2	0.23	4.13	16.55	32.48	225.31	25.14	137.00
STAKE 318	2087139	749336.6	0.26	4.81	15.30	31.08	216.37	23.58	126.90
STAKE 319	2087153	749366.3	0.22	4.11	14.43	30.10	210.14	22.48	119.80
STAKE 320	2087174	749341.5	0.26	4.75	15.43	31.22	217.27	23.73	127.91
STAKE 321	2087187	749369.9	0.22	4.04	13.34	28.90	202.50	21.12	111.04
STAKE 322	2087208	749343.6	0.25	4.59	11.17	26.50	187.34	18.40	93.47
STAKE 323	2087222	.749374.9	0.22	4.00	12.84	28.34	198.97	20.49	106.98
STAKE 324	2087242	749348.2	0.26	4.86	9.63	24.81	176.74	16.47	81.02
STAKE 325	2087256	749380.6	0.22	4.06	10.55	25.82	183.09	17.63	88.50
STAKE 326	2087276	749351.4	0.26	4.78	7.89	22.92	164.92	14.30	66.98
STAKE 327	2087288	749384.1	0.18	3.36	10.36	25.61	181.74	17.39	86.92
STAKE 328	2087307	749360.4	0.22	4.25	9.45	24.62	175.55	16.26	79.62
STAKE 329	2087322	749387.5	0.09	3.34	7.04	22.00	159.17	13.23	60.09
STAKE 330	2087343	749364.8	0.22	4.15	7.36	22.35	161.35	13.64	62.70
STAKE 331	2087355	749392.3	0.14		7.78	22.81	164.21	14.17	66.13
STAKE 332	2087376	749368.1	0.22	4.17	8.77	23.88	170.91	15.40	74.12
STAKE 333	2087098	749391	0.26	4.71	10.31	25.56	181.46	17.33	86.58
STAKE 334	2087131	749394	0.23	4.27	20.21	36.61	251.87	29.71	166.53
STAKE 335	2087146		0.22	4.08		28.27	198.56	20.42	106.50
STAKE 336	2087166	749396.2	0.27	5.13		41.93	286.53		204.02
STAKE 337	2087179		0.22	3.95	1	17.48	131.28		26.01
STAKE 338	2087201	749403.7	0.23	5.43		41.43	283.26	34.98	200.53
STAKE 339	2087212	749434.2	0.22	4.07		29.23	204.59		113.45
STAKE 340	2087233	749410.4	0.20	5.80		35.69	245.93	28.70	159.98
STAKE 341	2087246	749439.8	0.24		4.00	23.44	168.18	14.90	70.86
STAKE 342	2087268	749414	0.27	4.93		28.92	202.63	21.14	111.19
STAKE 343	2087281	749443.4	0.19		A	24.04	171.94	15.59	75.34
STAKE 344	2087303	749419.4	0.28	5.14		22.28	160.92	13.56	62.18
STAKE 345	2087314		0.18			23.99	171.57	15.53	74.90
STAKE 346	2087336		0.23		+	23.05	165.73	14.45	67.94
STAKE 347	2087225		0.21	3.96	<del></del>	20.85	152.05	11.90	51.49
STAKE 348	2087259		0.19			23.46	168.28	14.92	70.99

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						95% UCL	95% UCL	Best Fit	Best Fit
		[			ĺ	Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 349	2087294		0.23	4.03		22.60	162.90	13.92	64.56
STAKE 350	2087303		0.19	2.97	1.24	15.81	121.05	5.98	13.24
STAKE 351	2087328	749483.3	0.22	4.13		24.97	177.71	16.65	82.16
STAKE 352	2087339	749514.5	0.20	3.57	2.48	17.13	129.11	7.54	23.31
STAKE 353	2086620	749178.6	0.26	4.84		24.07	172.12	15.63	75.56
STAKE 354	2086658	749183.2	0.23	4.07	15.02	30.77	214.38	23.23	124.63
STAKE 355	2086645	749153.6	0.26	5.04		21.20	154.18	12.30	54.07
STAKE 356	2086678	749157.1	0.23	4.17	31.75	50.04	340.05	44.15	259.81
STAKE 357	2086692	749188	0.14	4.40	0.68	15.23	117.48	5.28	8.75
STAKE 358	2086712	749159.1	0.27	4.97	31.29	49.49	336.41	43.58	256.10
STAKE 359	2086726	749190.7	0.22	3.42	31.44	49.66	337.57	43.76	257.28
STAKE 360	2086747	749162.7	0.28	5.09		16.17	123.21	6.40	15.96
STAKE 361	2086760	749195.2	0.22	4.07	31.08	49.23	334.70	43.31	254.34
STAKE 362	2086780	749167.6	0.25	4.92	49.28	71.55	486.31	66.08	401.44
STAKE 363	2086793	749200.2	0.21	4.05	23.86	40.78	279.02	34.27	195.99
STAKE 364	2086816	749174.3	0.25	4.72	35.96	55.08	373.82	49.42	293.83
STAKE 365	2086829	749207.4	0.22	4.03		36.56	251.60	29.67	166.23
STAKE 366	2086850	749179.5	0.23	4.60		45.07	307.15	38.89	225.80
STAKE 367	2086863	749212.2	0.22	4.13		37.99	260.85	31.23	176.35
STAKE 368	2086884	749184.5	0.25	4.66	19.41	35.70	246.03	28.72	160.10
STAKE 369	2086896	749216.6	0.22	4.11	13.20	28.74	201.50	20.94	109.90
STAKE 370	2086917	749189	0.24	4.70	15.32	31.10	216.49	23.60	127.03
STAKE 371	2086929	749221.1	0.23	4.09	11.76	27.15	191.43	19.14	98.24
STAKE 372	2086951	749193.7	0.25	4.72		28.66	201.00	20.85	109.31
STAKE 373	2086964	749226	0.23	4.28	8.38	23.45	168.24	14.91	70.94
STAKE 374	2086984	749198.3	0.25	4.77	15.85	31.69	220.28	24.26	131.32
STAKE 375	2086996	749230.5	0.24	4.18	13.74	29.34	205.32	21.62	114.28
STAKE 376	2087017	749202.9	0.27	5.12	7.82	22.85	164.48	14.22	66.45
STAKE 377	2087032	749233.3	0.23	4.21	12.54	28.01	196.88	20.12	104.56
STAKE 378	2087052	749206.3	0.27	5.27	10.53	25.80	182.92	17.60	88.30
STAKE 379	2087066	749238.4	0.23	4.08	16.54	32.47	225.24	25.13	136.92
STAKE 380	2087086	749210.5	0.28	5.04	11.81	27.20	191.76	19.20	98.62
STAKE 381	2087100		0.22	4.17	14.62	30.31	211.49	22.72	121.35
STAKE 382		749216.5	0.29	5.21	5.99	20.87	152.15	11.92	51.61
STAKE 383		749248.9	0.23	2.94		24.79	176.61	16.45	80.86
STAKE 384		749220.8	0.29	5.34		21.38	155.31	12.51	55.43
STAKE 385		749252.7	0.19	3.60		23.59	169.12	15.07	71.99
STAKE 386	2087187	749225.6	0.24			24.78	176.55	16.44	80.80
STAKE 387	2087201	749257.7	0.18	3.44		29.04	203.38	21.28	112.06
STAKE 388	2087221		0.23	4.36		25.53	181.26	17.30	86.35
STAKE 389	2087235		0.20	3.70		20.61	150.56	11.62	49.68
STAKE 390	2087255		0.23			33.54	232.13	26.32	144.65
STAKE 391	2087268		0.19	100			158.56	13.12	59.35
STAKE 392	2087288		0.22	4.06		32.98	228.54	25.70	140.63
STAKE 393	2087300		0.19			23.34	167.56	14.79	70.13
STAKE 394	2087321		0.20	4.15		28.41	199.43	20.57	107.50
STAKE 395	2087335		0.20	3.65		18.50	137.50	9.15	33.71
STAKE 396	2087356		0.16			25.44	180.69	17.19	85.68
STAKE 397	2087369		0.19				160.95	13.56	62.23
STAKE 398	2087390		0.22		<del></del>		217.28	23.74	
STAKE 399	2087401		0.19				166.13	14.52	68.43

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 400	2087423	749254.9	0.21	4.08	10.92	26.23	185.66	18.10	91.51
STAKE 401	2087437	749285.8	0.19	3.43	2.88	17.54	131.65		26.47
STAKE 402	2087457	749257.3	0.22	4.22	6.80	21.75	157.62	12.94	58.22
STAKE 403	2087471	749289.9	0.19			20.49	149.81	11.48	48.77
STAKE 404	2087491	749261.5	0.22	3.98		24.15	172.62	15.72	76.15
STAKE 405	2086562	749113.5	0.23		L	47.38	322.38	41.34	241.66
STAKE 406	2086548	749086.1	0.25		70.17	98.96	680.13	92.22	570.25
STAKE 407	2086597	749120	0.23	4.16	3.78	18.51	137.56	9.16	33.78
STAKE 408	2086581	749087.8	0.27	5.07	65.77	93.02	637.55	86.71	534.69
STAKE 409	2086630	749120.7	0.23		39.73	59.66	404.76	54.13	324.27
STAKE 410	2086616	749089.4	0.27	5.07	47.85	69.74	473.80	64.29	389.87
STAKE 411	2086664	749123.5	0.23	4.28	44.24	65.22	442.69	59.77	360.68
STAKE 412	2086649	749095.5	0.26	4.95	47.33	69.08	469.25	63.64	385.64
STAKE 413	2086695	749127.2	0.22	4.12	33.97	52.68	357.72	46.93	277.73
STAKE 414	2086684	749098.3	0.25	4.85	41.91	62.34	422.97	56.86	341.87
STAKE 415	2086731	749133.6	0.22	4.14	27.15	44.61	304.12	38.40	222.62
STAKE 416	2086717	749102.1	0.26	4.74	17.73	33.80	233.80	26.61	146.51
STAKE 417	2086766	749134.9	0.22	4.23	15.42	31.21	217.22	23.72	127.86
STAKE 418	2086753	749103.9	0.27	4.88	11.23	26.56	187.74	18.47	93.94
STAKE 419	2086802	749139.7	0.21	3.90	6.79	21.73	157.53	12.93	58.11
STAKE 420	2086791	749108.2	0.31	5.45	1.43	16.02	122.30	6.22	14.81
STAKE 421	2086838	749146	0.17	3.10	7.44	22.43	161.89	13.74	63.35
STAKE 422	2086824	749116.6	0.27	4.75	1.21	15.78	120.88	5.95	13.03
STAKE 423	2086872	749152.5	0.20	3.52	4.42	19.19	141.78	9.96	38.97
STAKE 424	2086858	749122.1	0.26	4.76	1.15	15.72	120.47	5.87	12.51
STAKE 425	2086906	749156.8	0.20	3.55	4.22	18.98	140.48	9.72	37.37
STAKE 426	2086893	749127.1	0.15	4.83	1.23	15.80	121.01	5.97	13.19
STAKE 427	2086938	749161.4	0.22	3.84	0.86	15.41	118.60	5.50	10.17
STAKE 428	2086927	749132.3	0.26	4.44	1.17	15.74	120.60	5.89	12.68
STAKE 429	2086973	749165.6	0.24	4.13	0.91	15.47	118.97	5.57	10.63
STAKE 430	2086960	749137.2	0.22	4.01	6.95	21.90	158.59	13.12	59.39
STAKE 431	2087006	749171.2	0.11	3.85	1.95	16.57	125.66	6.87	19.02
STAKE 432	2086994	749143.3	0.21	4.05	42.57	63.15	428.51	57.68	347.18
STAKE 433	2087038	749179.6	0.22	3.93	6.55	21.47	155.92	12.62	56.16
STAKE 434	2087027	749142.3	0.22	4.32	25.83	43.08	294.02	36.75	211.97
STAKE 435	2087074	749181.4	0.18	3.56	11.37	26.72	188.73	18.65	
STAKE 436	2087061	749149.3	0.13	+	25.10	42.22	288.42	35.83	
STAKE 437	2087102	749193.9	0.21	-	15.71	31.53	219.28	24.09	130.19
STAKE 438	2087091	749164.2	0.27		22.62	39.37	269.78	32.73	186.04
STAKE 439	2087136	749190.9	0.22	4.10	11.50	26.86	189.62	18.81	96.13
STAKE 440	2087124	749171.5	0.26	+	19.81	36.16	248.96	29.22	163.33
STAKE 441	2087170	749205.5	0.16			24.16	172.67	15.73	
STAKE 442	2087157	749176.1	0.28			39.58	271.19	32.97	187.56
STAKE 443	2087205	749213.6	0.24			18.09	135.00		30.61
STAKE 444	2087192			-		34.49	238.25		151.47
STAKE 445	2087243		0.25			15.62	119.91	5.76	11.81
STAKE 446	2087228	749169.9	0.29			32.13	223.08		134.48
STAKE 447	2087278	749202.7	0.26			15.59	119.70		11.55
STAKE 448	2087262	749169.2	0.27		-	28.46	199.73		1
STAKE 449	2087311	749209.3	0.12			17.92	133.93		29.30
STAKE 450	2087296	749180.1	0.25	4.64	12.95	28.47	199.78	20.64	107.91

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 451	2087344		0.22	4.13		24.43	174.35	16.04	78.20
STAKE 452	2087331	749184.3	0.29	5.19		17.07	128.76	7.47	22.88
STAKE 453	2087378	749215.8	0.19	3.45	1	26.13	185.00	17.98	90.73
STAKE 454	2087362	749186.5	0.27	4.70		15.78	120.86	5.94	13.01
STAKE 455	2087408	749218.6	0.19	3.53		23.98	171.52	15.52	74.84
STAKE 456	2087385	749189.5	0.26	4.72		15.77	120.81	5.93	12.94
STAKE 457	2087435	749222.9	0.22	3.89		15.22	117.44	5.28	8.70
STAKE 458	2087420	749191.6	0.25	4.51	1.58	16.17	123.26	6.41	16.01
STAKE 459	2086537	749056	0.12	3.79		86.75	592.88	80.80	496.52
STAKE 460	2086554	749026.5	0.22	4.27	115.74	165.39	1176.47	149.22	938.42
STAKE 461	2086562	749057.5	0.22	4.20		129.42	903.63	119.33	745.36
STAKE 462	2086580	749028.8	0.25	4.83		155.05	1097.16	140.84	884.28
STAKE 463	2086597	749061.1	0.23	4.35	i	87.56	598.62	81.57	501.49
STAKE 464	2086616	749032.5	0.24	4.73		109.41	755.97	101.73	631.70
STAKE 465	2086628	749061.8	0.25	4.55		28.65	200.91	20.84	109.21
STAKE 466	2086646	749030.8	0.23	4.50		31.11	216.58	23.61	127.13
STAKE 467	2086671	749065	0.27	4.71		15.84	121.22	6.01	13.45
STAKE 468	2086691	749039.1	0.26	4.87		51.38	349.03	45.57	268.94
STAKE 469	2086703	749068.1	0.24	4.25		15.51	119.23	5.62	10.95
STAKE 470	2086724	749042.2	0.27	5.03		58.31	395.60	52.75	315.33
STAKE 471	2086738	749071.9	0.25	4.33		15.53	119.35	5.65	11.11
STAKE 472	2086758	749046.8	0.22	4.26		63.38	430.07	57.91	348.67
STAKE 473	2086770	749077.2	0.22	4.08		15.51	119.22	5.62	10.95
STAKE 474	2086792	749049.9	0.21	3.98		53.33	362.06	47.60	282.08
STAKE 475	2086803	749079.5	0.25	4.39		15.55	119.47	5.67	11.26
STAKE 476	2086824	749059.8	0.25	4.56		27.68	194.80	19.74	102.15
STAKE 477	2086835	749081.8	0.23	4.12	0.92	15.48	119.03	5.59	10.70
STAKE 478	2087214	749139.4	0.11	4.17	15.75	31.58	219.55	24.13	130.49
STAKE 479	2087348	749158.6	0.18	3.45		26.88	189.74	18.83	96.27
STAKE 480	2087373	749135.7	0.20	3.82		25.37	180.24	17.11	85.15
STAKE 481	2087316	749152.1	0.19	3.59		25.39	180.37	17.14	85.30
STAKE 482	2087331	749131.3	0.21	3.85		25.88	183.47	17.70	88.94
STAKE 483	2087282	749148.6	0.20	3.77	12.38	27.83	195.77	19.92	103.28
STAKE 484		749125.9	0.21			24.50	174.80	16.12	78.73
STAKE 485	2087249		0.25		<del></del>	25.18	179.03	16.89	83.72
STAKE 486	2087268		0.22	4.07		27.50	193.66	19.54	100.83
STAKE 487	2087235		0.25	4.55		22.76	163.92	14.11	65.79
STAKE 488	2087183		0.24			32.34	224.45	24.99	136.03
STAKE 489	2087202		0.20			29.41	205.78	21.70	114.81
STAKE 490	2087150		0.23			29.49	206.26	21.79	115.36
STAKE 491	4	749106.5	0.26			29.65	207.29	21.97	116.54
STAKE 492	2087117		0.27			39.31	269.39	32.67	185.61
STAKE 493	2087136		0.22	4.26		28.61	200.70	20.80	108.97
STAKE 494	2087086		0.27			33.21	230.00	25.96	142.26
STAKE 495	2087106		0.29			34.29	236.95	27.16	150.02
STAKE 496	2087043		0.25			35.66	245.76	28.67	159.80
STAKE 497	2087063		0.23				196.11	19.98	103.67
STAKE 498	2087014		0.27		1	29.74	207.82	22.07	117.15
STAKE 499	2087036		0.30			48.63	330.71	42.67	
STAKE 500	2087571	749409.4	0.09	<del></del>	<del></del>	15.36	118.31	5.45	
STAKE 501		749380.9				15.26		5.33	

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-						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted		l
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Predicted Am-241	Predicted Pu-239/240
STAKE 502	2087525		0.20	3.65		15.41	118.62	5.51	10.19
STAKE 503	2087537	749469	0.20	3.96		16.14	123.07	6.37	15.78
STAKE 504	2087555		0.21			15.34	118.17	5.42	9.62
STAKE 505	2087573	749469.7	0.13	3.95	<u> </u>	15.65	120.08	5.79	12.02
STAKE 506	2087591	749500.3	0.21	4.21	7.14	22.12	159.91	13.37	60.97
STAKE 507	2087608	749469.1	0.20	3.79	6.03	20.92	152.45	11.98	51.98
STAKE 508	2087625	749497.9	0.20	3.69	5.46	20.30	148.65	11.26	47.36
STAKE 509	2087640	749469.1	0.13	3.97	4.82	19.62	144.43	10.46	42.20
STAKE 510	2087659	749498.4	0.22	3.63		20.45	149.55	11.43	48.45
STAKE 510	2087674	749467.3	0.19	4.00		20.43	146.77	10.91	45.07
STAKE 512	2087692	749496	0.21	3.57	5.18	20.00	146.76	10.90	45.06
STAKE 513	20877092	749467.6	0.19	3.89	6.02	20.91	152.39	11.96	51.90
STAKE 514	2087725	749494.4	0.21	3.63		19.36	142.84	10.16	40.26
STAKE 514	2087742	749467.8	0.20	3.84	4.71	19.50	143.70	10.10	41.31
STAKE 516	2087785	749330.5	0.21	3.83		19.00	140.60	9.74	37.52
STAKE 517	2087606	749535.1	0.21	3.29		17.72	132.76	8.24	27.84
STAKE 517 STAKE 518	2087644	749535.1	0.16	3.29	5.59	20.45	149.54	11.43	48.43
STAKE 518	2086484	748886.6	0.14	4.12	35.32	54.30	368.57	48.61	288.60
STAKE 519	2086492	748850.9	0.23	4.12		18.81	139.44	9.52	36.09
STAKE 520	2086513	748881.4	0.27	4.93	33.75	52.42	355.98	46.66	275.97
STAKE 521	2086523	748850.7	0.22	5.57	33.73	18.38	136.82	9.02	32.87
STAKE 522 STAKE 523	2086546	748874.4	0.36	4.08	36.33	55.53	376.83	49.88	296.82
STAKE 523 STAKE 524	2086548	748846.1	0.12	5.04		22.04	159.45	13.28	60.42
STAKE 524 STAKE 525	2086575	748876.2	0.27	3.87	27.80	45.37	309.11	39.21	227.86
STAKE 525	2086582	748844.4	0.21	5.48	4.67	19.45	143.40	10.27	40.95
STAKE 520 STAKE 527	2086608	748872.6	0.30	3.46		45.71	311.34	39.57	230.18
STAKE 527	2086624	748840.2	0.21	5.46		18.81	139.47	9.52	36.12
STAKE 528	2086638	748872.1	0.29	3.76	4.07 13.27	28.82	202.01	21.03	110.48
STAKE 529 STAKE 530	2086660	748840.9	0.20	5.50	4.90	19.70	144.95	10.56	42.84
STAKE 530	2086681	748863.6	0.15	3.98	16.22	32.10	222.89	24.72	134.27
STAKE 531		748833.7						8.50	29.52
	2086694		0.30	5.54	3.25	17.94 34.21	134.11	27.06	149.43
STAKE 533	2086716	748861.1	0.23	4.28	18.09		236.42		
STAKE 534 STAKE 535	2086730 2086749	748827.7 748856.6	0.28	5.13 4.32	8.26 24.78	23.32 41.86	167.42 286.02	14.76 35.43	69.96 203.47
STAKE 535						25.71	182.39		87.68
	2086762		0.27	5.00				17.50	
STAKE 537	2086780	<u></u>	0.24	<del></del>		33.29	230.54	26.05	142.87
STAKE 538	2086793		0.28			28.13	197.62	20.25	105.41
STAKE 539	2086813		0.30			23.12	166.14	14.52	68.43
STAKE 540	2086826		0.27	5.07		15.93	121.76	6.12	14.13
STAKE 541	2086845	<u> </u>	0.23			16.12	122.92	6.34	15.59
STAKE 542	2086858		0.27	5.00		19.34	142.71	10.14	40.10
STAKE 543	2086888		0.27					9.98	39.06
STAKE 544	2086871		0.14	+		15.37	118.39	5.46	9.90
STAKE 545	2086904		0.25		<del></del>	23.38	167.76	14.82	70.37
STAKE 546	2086495		0.13			85.16	581.58	79.29	
STAKE 547	2086531	748906.1	0.20			87.27	596.59	81.30	
STAKE 548	2086566		0.21			36.03	248.14	29.08	
STAKE 549	2086599		0.22			45.39	309.26	39.23	228.01
STAKE 550	2086633					42.58	290.74	36.21	208.49
STAKE 551	2086656		0.22			34.10	235.74	26.95	
STAKE 552	2086697	748886.4	0.24	4.73	18.58	34.76	239.95	27.67	153.36

						050/ 1101	059/ 1101	Doot Fit	Doot Fit
						95% UCL	95% UCL Predicted	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	U-235	U-238	Am 241	Predicted		Predicted	Predicted
STAKE NOMBER	2086731	Northing 748883.1	0.22		Am-241	Am-241	Pu-239/240	Am-241 30.23	Pu-239/240
STAKE 553	2086766	748879.4	0.22	4.03		37.08	254.91		169.86
STAKE 555	2086799	748875.6	0.23	4.58		34.89	240.78	27.82	154.29
STAKE 556	2086832	748875.4	0.22	4.15 4.71	19.68 16.28	36.00 32.17	247.98 223.33	29.05 24.79	162.25
STAKE 557	2086850	748903.1	0.23	4.71	15.10	30.85	214.90	23.32	134.77 125.22
STAKE 557	2086881	748903.1	0.22	4.02		27.26	192.13	19.26	99.05
STAKE 559	2086904	748926.7	0.23	4.23		37.37	256.81	30.55	171.93
STAKE 560	2086870	748933.5	0.24	5.21		32.15	223.24	24.78	134.67
STAKE 561	2086835	748934.5	0.26	4.82	17.36	33.38	231.10	26.15	143.50
STAKE 562	2086804		0.20	5.27	14.25	29.90			118.36
STAKE 562 STAKE 563	2086813	748943.3					208.88	22.25	
STAKE 563	2086768	748908.1	0.26	4.79	18.87	35.09	242.10	28.04	155.74
STAKE 565	2086782	748939.4	0.29 0.27	5.37	21.02	37.54	257.89	30.73 33.54	173.11
STAKE 566		748911.7		5.04	23.27	40.11	274.59	33.54	191.23
STAKE 567	2086737	748938.5	0.28	5.36	23.80	40.72	278.60		195.54
	2086750	748912	0.27	5.16	23.34	40.19	275.15	33.63	191.83
STAKE 568	2086705	748938.1	0.29	5.46	23.11	39.92	273.40	33.34	189.94
STAKE 569 STAKE 570	2086716	748910.6	0.29	5.30	28.35	46.01	313.36	39.89	232.28
	2086673	748949.5	0.25	4.77	25.76	42.99	293.49	36.66	211.41
STAKE 571	2086681	748918.6	0.33	4.81	23.97	40.92	279.89	34.42	196.92
STAKE 572	2086646	748953.2	0.28	5.25	28.65	46.36	315.67	40.27	234.69
STAKE 573	2086662	748926.5	0.29	5.50		48.02	326.67	42.03	246.08
STAKE 574	2086621	748938.8	0.30	5.66		56.63	384.23	51.02	304.15
STAKE 575	2086595	748927.8	0.27	5.19		55.60	377.31	49.96	297.30
STAKE 576	2086569	748943.9	0.24	4.34	23.22	40.05	274.25	33.48	190.87
STAKE 577	2086540	748927.1	0.25	4.66	39.60	59.49	403.63	53.96	323.17
STAKE 578	2086522	748932.1	0.25	4.70	31.53	49.77	338.29	43.88	258.02
STAKE 579	2086486	748943	0.25	4.49	4.03	18.77	139.19	9.47	35.79
STAKE 580 STAKE 581	2086512	748967.8	0.21	4.00	42.86	63.51	431.00	58.05	349.56 180.39
STAKE 581	2086542	748960	0.23	4.25	21.93	38.57	264.57	31.86	
STAKE 582	2086534	748992.6	0.22	4.40	77.20	108.60	750.10	101.01	627.02
	2086568	748981.4	0.23	4.32	34.13	52.87	358.99	47.12	278.99
STAKE 584	2086602	748986.4	0.22	4.14	40.94	61.14	414.85	55.65	334.04
STAKE 585	2086592	748960.7	0.25	4.48	28.01	45.62	310.76	39.47	229.58
STAKE 586	2086624		0.25			35.89	247.26	28.93	161.45
STAKE 587	2086642	749006.2	0.24		34.06	52.79	358.42	47.04	278.42
STAKE 588	2086660		0.24				244.66	28.48	158.58
STAKE 589	2086678			4.22		27.89	196.14	19.99	103.71
STAKE 590	2086712		0.22	4.09		32.21	223.60	24.84	135.07
STAKE 591	2086744		0.24	4.41		33.82	233.89	26.63	146.61
STAKE 592	2086775		0.28	5.48		37.13	255.26	30.29	170.24
STAKE 593	2086806		0.13	4.59		29.92	209.00	22.28	118.50
STAKE 594	2086935		0.23	4.34		25.64	181.92	17.42	87.13
STAKE 595	2086950		0.24			54.42	369.37	48.74	289.40
STAKE 596	2086969		0.26	4.95	·	49.40	335.80	43.48	255.47
STAKE 597	2086957	749050.8	0.23			41.87	286.11	35.45	203.57
STAKE 598	2086993		0.20			36.86	253.52	29.99	168.34
STAKE 599	2087025					45.58	310.52	39.43	
STAKE 600	2087058		0.24			37.04	254.66	30.18	
STAKE 601	2087093		0.25	4.67		35.59	245.32	28.59	
STAKE 602	2087121	749069.6	0.24			34.40	237.65	27.28	
STAKE 603	2087157	749072.4	0.27	5.22	15.02	30.76	214.37	23.22	124.63

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 604	2087141	749046	0.25	4.66		39.53	270.81	32.90	187.15
STAKE 605	2087080	749040.8	0.26	5.09	24.04	41.00	280.45	34.51	197.52
STAKE 606	2087119	749044.4	0.26	4.94		44.70	304.70	38.49	223.23
STAKE 607	2087046	749035.9	0.31	5.74		47.20	321.18	41.15	240.41
STAKE 608	2087015	749031.6	0.29	5.54	20.73	37.20	255.74	30.37	170.76
STAKE 609	2086978	749028.2	0.26	4.74	22.66	39.41	270.05	32.78	186.33
STAKE 610	2086946	749026	0.29	5.44	32.61	51.06	346.88	45.23	266.76
STAKE 611	2086967	748998.3	0.22	3.99	17.04	33.02	228.80	25.75	140.92
STAKE 612	2087003	749001.8	0.18	6.13	35.81	54.89	372.53	49.22	292.54
STAKE 613	2087035	749005.3	0.25	4.59	21.72	38.33	263.01	31.60	178.70
STAKE 614	2087057	749008.5	0.29	5.48	25.51	42.70	291.54	36.34	209.34
STAKE 615	2087058	749007.3	0.27	4.86	19.63	35.95	247.65	28.99	161.88
STAKE 616	2087019	748975.7	0.31	5.73	15.65	31.47	218.85	24.01	129.71
STAKE 617	2086921	748956.8	0.16	5.00	29.53	47.40	322.55	41.37	241.83
STAKE 618	2086956	748962.6	0.29	5.38	21.58	38.17	261.97	31.42	177.57
STAKE 619	2087095	749014.8	0.25	4.65	21.42	37.98	260.80	31.22	176.29
STAKE 620	2086708	748990.8	0.24	4.48	17.98	34.09	235.63	26.93	148.55
STAKE 621	2086735	748991.8	0.22	4.01	14.97	30.70	213.98	23.15	124.17
STAKE 622	2086763	748992.1	0.23	4.49	17.94	34.04	235.34	26.88	148.23
STAKE 623	2086801	748993.8	0.25	4.54	16.72	32.67	226.52	25.35	138.35
STAKE 624	2086834	748997.5	0.29	5.45	21.00	37.50	257.68	30.70	172.89
STAKE 625	2086980	749107.3	0.25	4.71	19.08	35.32	243.56	28.29	157.37
STAKE 626	2087001	749084.9	0.23	4.19	18.28	34.42	237.80	27.30	150.97
STAKE 627	2086012	748785.6	0.27	5.03	7.01	21.97	159.00	13.20	59.88
STAKE 628	2085996	748755.7	0.24	4.56	5.79	20.66	150.84	11.67	50.02
STAKE 629	2085980	748784.9	0.30	5.47	9.12	24.26	173.30	15.84	76.96
STAKE 630	2085962	748757.3	0.27	4.86	11.52	26.88	189.76	18.84	96.29
STAKE 631	2085949	748778.1	0.26	4.81	21.68	38.28	262.71	31.55	178.37
STAKE 632	2085932	748755.7	0.30	4.33	5.05	19.86	145.93	10.75	44.04
STAKE 633	2085899	748693.8	0.29	5.42	7.84	22.86	164.57	14.23	66.56
STAKE 634	2085914	748722	0.25	4.66	2.66	17.32	130.25	7.76	24.74
STAKE 635	2085928	748692.4	0.23	4.39	34.27	53.04	360.09	47.30	280.11
STAKE 636	2085945	748721.6	0.20	3.79	4.49	19.27	142.26	10.05	39.56
STAKE 637	2085962	748698.5	0.25	4.70	3.45	18.15	135.39	8.74	31.10
STAKE 638	2085974	748723.2	0.20	3.83	2.89	17.56	131.78	8.05	26.63
STAKE 639	2085995	748691.5	0.29	4.91	2.05	16.67	126.31	7.00	19.83
STAKE 640	2086015	748722	0.22	4.07	16.81	32.76	227.14	25.46	139.06
STAKE 641	2086028	748693.2	0.26	4.89	42.92	63.59	431.53	58.13	350.07
STAKE 642	2086045	748720.2	0.23	4.20	64.75	91.65	627.76	85.43	526.41
STAKE 643	2086062	748694.7	0.27	4.97	96.08	135.61	949.95	124.63	779.57
STAKE 644	2086079	748721.4	0.23	4.31	75.34	106.03	731.35	98.68	612.00
STAKE 645	2086095	748690.6	0.34	6.06	7.89	22.92	164.94	14.30	67.00
STAKE 646	2086112	748718	0.29	5.15	4.20	18.95	140.30	9.68	37.15
STAKE 647	2086130		0.28	5.20	1	48.49	329.77	42.52	249.28
STAKE 648	2086145	748719.6	0.26	4.69	1.25	15.82	121.12	5.99	13.33
STAKE 649	2086157	748694.5	0.29	5.25	18.37	34.52	238.45	27.42	151.69
STAKE 650	2086172	748723.2	0.27	4.74	0.81	15.36	118.30	5.44	9.79
STAKE 651	2086189	748693.3	0.24	4.32	45.43	66.70	452.87	61.26	370.30
STAKE 652	2086205	748719.6	0.27	5.08	58.75	83.74	571.56	77.93	477.97
STAKE 653	2086229	748690.8	0.25	4.71	33.21	51.77	351.63	45.98	271.58
STAKE 654	2086245	748718.7	0.29	5.60	48.41	70.45	478.70	65.00	

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 655	2086213	748661.4	0.26	4.98		44.84	305.64	38.64	224.21
STAKE 656	2086179	748662.3	0.25	4.51	27.97	45.57	310.41	39.42	229.21
STAKE 657	2086148	748663.5	0.29	5.49	1	66.89	454.15	61.45	371.51
STAKE 658	2086133	748634.6	0.28	5.09		39.61	271.35	32.99	187.73
STAKE 659	2086120	748663.3	0.32	5.96		70.23	477.18	64.78	393.01
STAKE 660	2086103	748634.9	0.27	4.94	The state of the s	36.82	253.27	29.95	168.06
STAKE 661	2086083	748663.6	0.13	5.54		59.69	404.95	54.16	324.45
STAKE 662	2086060	748634.2	0.27	4.90	47.74	69.60	472.81	64.15	388.95
STAKE 663	2086044	748662.5	0.31	5.75	19.18	35.43	244.30	28.42	158.18
STAKE 664	2086028	748635.4	0.22	4.13	4.06	18.81	139.41	9.51	36.05
STAKE 665	2086014	748662.6	0.23	4.40	4.51	19.28	142.35	10.07	39.66
STAKE 666	2085992	748633.6	0.22	4.02	2.52	17.17	129.35	7.59	23.62
STAKE 667	2085978	748666.6	0.25	4.67	2.09	16.71	126.55	7.05	20.13
STAKE 668	2085961	748634.8	0.13	4.40		35.07	241.96	28.02	155.59
STAKE 669	2085947	748667.5	0.23	4.27	35.31	54.29	368.53	48.61	288.56
STAKE 670	2085932	748639.7	0.24	4.47	14.18	29.83	208.43	22.17	117.85
STAKE 671	2085917	748667.3	0.23	4.25	17.63	33.69	233.08	26.49	145.71
STAKE 672	2085893	748639.7	0.21	4.00	0.56	15.10	116.71	5.13	7.78
STAKE 673	2085883	748672.2	0.22	4.11	2.22	16.85	127.42	7.21	21.21
STAKE 674	2085866	748643.5	0.11	4.69	1.90	16.51	125.35	6.81	18.63
STAKE 675	2085848	748670.3	0.22	4.18	1.56	16.15	123.13	6.38	15.86
STAKE 676	2085828	748649.9	0.17	4.31	2.40	17.04	128.57	7.43	22.64
STAKE 677	2085846	748620.3	0.26	4.86		15.63	119.93	5.76	11.83
STAKE 678	2085831	748589.2	0.26	4.71	1.23	15.80	121.01	5.97	13.19
STAKE 679	2085876	748610.2	0.20	3.84	0.92	15.47	118.98	5.58	10.64
STAKE 680	2085863	748583	0.22	4.22	1.93	16.54	125.51	6.84	18.84
STAKE 681	2085913		0.23	4.15		22.80	164.17	14.16	66.08
STAKE 682	2085893		0.25	4.67	5.39	20.23	148.18	11.17	46.78
STAKE 683	2085942	748608.4	0.23	4.14	16.34	32.24	223.77	24.87	135.27
STAKE 684	2085925	748579.4	0.24	4.48		27.44	193.29	19.47	100.40
STAKE 685	2085975	748605.6	0.21	4.03		24.85	177.00	16.52	81.33
STAKE 686	2085958	748576.6	0.22	4.12	7.23	22.21	160.46	13.47	61.64
STAKE 687	2086008	748604.7	0.24	4.37	2.25	16.88	127.61	7.25	21.44
STAKE 688	2085995		0.12	4.56		22.29	160.99	13.57	62.27
STAKE 689	2086042	748602.8	0.21	3.85		33.69	233.11	26.49	145.74
STAKE 690	2086023		0.24	797777777777777777777777777777777777777		24.71	176.08	16.35	80.24
STAKE 691	2086080		0.22	4.13		32.20	223.53	24.83	134.99
STAKE 692	2086062	748573.3	0.22	4.33		65.43	444.15	59.99	362.06
STAKE 693	2086105		0.31	5.27		37.44	257.27	30.63	172.44
STAKE 694	2086087	748575.2	0.27	5.06	i	28.38	199.25	20.54	107.29
STAKE 695	2086010	748542.4	0.21	3.88		25.85	183.27	17.66	88.71
STAKE 696	2086045	748547	0.24	4.51	1	32.29	224.13	24.93	135.66
STAKE 697	2085977	748547.9	0.20	3.81	<u></u>	23.95	171.32	15.48	74.60
STAKE 698	2085956 2085943	748516.6	0.25	4.63		22.65 22.67	163.26	13.99	64.99 65.10
STAKE 699 STAKE 700	2085943		0.22 0.26	4.04 4.82		22.67	163.35 160.42	14.01	61.58
STAKE 700	2085924	748520.7 748549.3	0.26	4.82		22.20	150.42	13.46 11.58	49.39
STAKE 701	2085894	748525.3	0.25	4.12		23.95	171.37	15.49	74.67
STAKE 702	2085883		0.25	3.93		23.95	169.09	15.49	74.67
STAKE 703	2085863	748551.4 748524	0.13	4.60			167.95	15.07	71.96
STAKE 704 STAKE 705	2085850			3.56		23.41	167.95		
DIANE 100	2000000	146004.4	0.19	3.56	8.03	23.08	105.90	14.48	68.15

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						95% UCL	95% UCL	Post Fit	Dont Eit
}	}	}			1	Predicted	Predicted	Best Fit Predicted	Best Fit Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 706	2085828	748528.9	0.25	4.64			159.83		60.88
STAKE 707	2085817	748560	0.22	4.16		15.54	119.42	5.66	11.19
STAKE 708	2085793	748532.1	0.24	4.67	5.90	20.78	151.60	11.82	50.94
STAKE 709	2085782	748563.6	0.22	4.02		17.43	130.93	7.89	25.57
STAKE 710	2085763	748534.9	0.26	4.91		18.11	135.16	8.70	30.81
STAKE 711	2085776	748505.7	0.21	3.84		17.57	131.81	8.06	26.67
STAKE 712	2085756	748478.2	0.21	5.13		16.77	126.91	7.12	20.58
STAKE 713	2085809	748500.6	0.21	3.82		18.47	137.34	9.12	33.51
STAKE 714	2085792	748472.8	0.25	4.88	3.19	17.87	133.68	8.42	28.98
STAKE 715	2085844	748500.4	0.22	3.80		20.36	149.01	11.33	47.80
STAKE 716	2085823	748469.7	0.25	4.84		18.19	135.63	8.79	31.40
STAKE 717	2085876	748493.3	0.22	4.08	6.00	20.88	152.26	11.94	51.74
STAKE 718	2085854	748466.6	0.25	4.74	4.45	19.22	141.99	10.00	39.22
STAKE 719	2085803	748446.6	0.25	4.69		16.94	127.96	7.32	21.89
STAKE 720	2085767	748447.7	0.22	4.02	1.12	15.69	120.29	5.83	12.29
STAKE 721	2085740	748447.4	0.25	4.71	1.79	16.39	124.59	6.67	17.68
STAKE 722	2085752	748421.9	0.21	3.91	1.55	16.14	123.08	6.37	15.79
STAKE 723	2085707	748453.2	0.23	4.48	1.36	15.94	121.83	6.13	14.22
STAKE 724	2085718	748426	0.16	4.31	1.68	16.28	123.93	6.54	16.85
STAKE 725	2086043	748778.4	0.22	4.13		24.93	177.50	16.61	81.92
STAKE 726	2086026	748753.5	0.26	4.91	11.25	26.59	187.91	18.50	94.13
STAKE 727	2086076	748777.2	0.25	4.64	15.25	31.02	216.01	23.51	126.48
STAKE 728	2086059	748750.7	0.29	5.43	17.09	33.07	229.14	25.80	141.29
STAKE 729	2086111	748777.8	0.26	4.70	39.42	59.27	402.15	53.74	321.72
STAKE 730	2086093	748749.4	0.30	5.46	25.38	42.54	290.53	36.17	208.27
STAKE 731	2086135	748779.4	0.26	4.93	21.06	37.57	258.12	30.77	173.36
STAKE 732	2086126	748767	0.34	6.28	4.92	19.72	145.07	10.58	42.99
STAKE 733	2086179	748774.9	0.26	4.82	13.48	29.04	203.43	21.29	112.12
STAKE 734	2086159	748749.2	0.35	6.31	10.36	25.62	181.80	17.40	86.98
STAKE 735	2086215	748770.3	0.26	4.84	65.14	92.17	631.48	85.92	529.56
STAKE 736	2086197	748746.4	0.36	6.49	4.85	19.65	144.59	10.49	42.41
STAKE 737	2086246	748776	0.23	4.53	17.65	33.71	233.19	26.51	145.84
STAKE 738	2086228	748742.4	0.30	5.66	47.87	69.76	473.94	64.31	390.00
STAKE 739	2086279	748770.9	0.25	4.57	20.87	37.36	256.76	30.54	171.88
STAKE 740	2086264	748747.3	0.16	5.87	61.45	87.27	596.59	81.30	499.73
STAKE 741	2086316	748776.4	0.27	4.97	15.58	31.38	218.30	23.91	129.09
STAKE 742	2086296	748748.2	0.30	5.53	23.76	40.67	278.30	34.15	195.21
STAKE 743	2086329	748801.6	0.25	4.65	27.06	44.51	303.43	38.28	221.90
STAKE 744	2086344	748826.8	0.27	5.15	45.79	67.16	455.99	61.72	373.24
STAKE 745	2086298	748803	0.18	4.62	41.88	62.30	422.72	56.82	341.63
STAKE 746	2086317	748831.6	0.13	5.10	45.10	66.30	450.08	60.85	367.67
STAKE 747	2086264	748802.5	0.23	4.57	32.81	51.29	348.42	45.47	268.32
STAKE 748	2086286	748835.3	0.27	5.15	65.40	92.52	633.96	86.24	531.66
STAKE 749	2086830	748714.6	0.23		1		178.30	16.76	82.86
STAKE 750	2086847	748687.2	0.26			31.17	216.97	23.68	127.58
STAKE 751	2086872	748715.8	0.22			21.77	157.74		58.37
STAKE 752	2086881	748680.1	0.25			30.22	210.93		120.70
STAKE 753	2086912	748674.8	0.26			28.50	199.97	20.67	108.13
STAKE 754	2086948		0.11				145.27	10.62	43.24
STAKE 755	2086893		0.15			26.43	186.93		
STAKE 756	2086928	.748645.5	0.22	3.99	5.80	20.67	150.91	11.69	50.11

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 757	2086980	748664.2	0.24	4.27	1.02	15.58	119.64	5.70	11.47
STAKE 758	2086961	748641.3	0.11	4.71	6.80	21.75	157.62	12.94	58.22
STAKE 759	2086907	748618.8	0.21	3.94	7.64	22.65	163.21	13.98	64.94
STAKE 760	2086871	748622.8	0.24	4.58	8.90	24.02	171.76	15.56	75.13
STAKE 761	2086780	748609.3	0.22	4.04	13.17	28.71	201.31	20.91	109.68
STAKE 762	2086819	748602.9	0.26	4.72	10.90	26.20	185.49	18.07	91.31
STAKE 763	2086851	748597.4	0.23	4.16	8.87	23.98	171.55	15.52	74.88
STAKE 764	2086882	748593.5	0.25	4.89	8.99	24.12	172.41	15.68	75.90
STAKE 765	2086760	748581.8	0.22	4.04	11.14	26.47	187.14	18.36	93.24
STAKE 766	2086794	748576.1	0.27	4.65	12.43	27.88	196.09	19.98	103.65
STAKE 767	2086827	748569.4	0.17	4.63		26.68	188.47	18.60	94.79
STAKE 768	2086862	748563.2	0.20	3.79	5.44	20.28	148.54	11.24	47.22
STAKE 769	2086895	748558.5	0.25	4.84		23.16	166.40	14.57	68.75
STAKE 770	2086927	748550.6	0.21	3.84		20.19	147.94	11.13	46.49
STAKE 771	2087045	748892.7	0.24	4.24	7.50	22.50	162.27	13.81	63.81
STAKE 772	2087049	748928	0.25	4.41	3.26	17.95	134.13	8.50	29.55
STAKE 773	2087080	748904.4	0.22	3.95	5.35	20.19	147.95	11.13	46.50
STAKE 774	2087092	748926.9	0.26	4.77	9.20	24.34	173.81	15.94	77.56
STAKE 775	2087066	748956.7	0.22	3.94	9.37	24.53	174.95	16.15	78.91
STAKE 776	2087099	748961.1	0.07	1.31	0.38	14.91	115.55	4.91	6.32
STAKE 777	2087076	748988.3	0.22	3.99	10.80	26.09	184.80	17.94	90.50
STAKE 778	2087108	748992.9	0.24	4.40	17.21	33.21	230.02	25.96	142.29
STAKE 779	2087144	748996.9	0.22	4.10	3.92	18.65	138.45	9.33	34.87
STAKE 780	2087178	749001.4	0.14	4.31	3.50	18.20	135.70	8.80	31.48
STAKE 781	2087132	749022.5	0.21	3.82	19.30	35.57	245.21	28.57	159.18
STAKE 782	2087165	749026	0.24	4.40		15.89	121.55	6.08	13.87
STAKE 783	2087198	749029	0.19	4.11	4.45	19.22	141.98	10.00	39.21
STAKE 784	2087176	749055	0.23	4.33	4.75	19.54	143.94	10.37	41.61
STAKE 785	2087189	749066.9	0.21	3.76		23.61	169.23	15.09	72.12
STAKE 786	2087208	749053	0.24	4.42	23.06	39.87	273.06	33.28	189.58
STAKE 787	2087218	749070.6	0.20	3.75	11.80	27.19	191.73	19.19	98.58
STAKE 788	2087241	749055	0.22	4.28	10.31	25.56	181.45	17.33	86.57
STAKE 789	2087255	749080.2	0.20	3.79	14.00	29.63	207.13	21.94	116.36
STAKE 790	2087279		0.23			24.66	175.78	16.30	79.89
STAKE 791	2087288		0.15			26.64	188.26	18.57	94.54
STAKE 792	2087311		0.24			38.93	266.95	32.26	182.98
STAKE 793	2087321	749094.8	0.20			27.63	194.51	19.69	101.82
STAKE 794	2087346		0.23	4.32		26.48	187.22	18.38	93.33
STAKE 795	2087356		0.08			26.97	190.34	18.94	
STAKE 796	2087375		0.23		-		174.41	16.05	78.27
STAKE 797	2087390		0.20			***********	184.80	17.94	90.50
STAKE 798	2087415		0.22	4.10		25.05	178.27	16.75	82.82
STAKE 799	2087423		0.21	3.95		26.25	185.80	18.12	91.67
STAKE 800	2087453		0.18			27.19	191.73	19.19	98.58
STAKE 801	2087488		0.21	4.00		19.84	145.82	10.73	
STAKE 802	2087527	749127.6	0.23	4.09		15.65	120.05	5.78	
STAKE 803	2087512		0.21	3.85		16.61	125.93	6.93	
STAKE 804	2087480		0.19	3.49		22.78	164.04	14.14	
STAKE 805	2087445		0.20	3.70		25.55	181.36	17.32	
STAKE 806	2087469		0.21	4.05	<u> </u>	26.94	190.14	18.91	96.74
STAKE 807	2087433	749055.6	0.23	4.09	11.72	27.11	191.17	19.09	97.94

		*				95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 808	2087399	749055.4	0.20	3.77	12.40	27.85	195.91	19.94	103.43
STAKE 809	2087503	749070	0.20	3.53	6.98	21.93	158.77	13.16	59.60
STAKE 810	2087494	749036.1	0.23	4.24	11.53	26.90	189.88	18.86	96.43
STAKE 811	2087475	749007.9	0.20	3.64	12.50	27.97	196.60	20.07	104.24
STAKE 812	2087456	749029.4	0.18	4.14	14.07	29.71	207.64	22.03	116.94
STAKE 813	2086429	748423.7	0.23	4.13	6.05	20.94	152.58	12.00	52.12
STAKE 814	2086409	748400.8	0.25	4.76	7.43	22.42	161.83	13.73	63.28
STAKE 815	2086464	748412.9	0.24	4.28	6.08	20.97	152.80	12.04	52.40
STAKE 816	2086438	748390.2	0.25	4.90	6.57	21.50	156.05	12.65	56.32
STAKE 817	2086494	748410.3	0.23	4.18	4.25	19.01	140.67	9.75	37.60
STAKE 818	2086475	748386.1	0.27	5.12		21.63	156.88	12.80	57.33
STAKE 819	2086624	748451.8	0.22	4.07	6.29	21.19	154.18	12.30	54.06
STAKE 820	2086658	748448.2	0.25	4.71	8.19	23.25	166.97	14.68	69.42
STAKE 821	2086233	748516.3	0.24	4.29	10.84	26.14	185.11	18.00	90.86
STAKE 822	2086223	748550.2	0.26	4.80	13.37	28.92	202.67	21.15	111.24
STAKE 823	2086210	748491.6	0.22	4.17	8.38	23.45	168.22	14.91	70.92
STAKE 824	2086200	748525.6	0.25	4.81	12.36	27.81	195.61	19.89	103.09
STAKE 825	2086188	748468.5	0.23	4.19		19.82	145.64	10.69	43.69
STAKE 826	2086178	748499.4	0.25	4.79		23.69	169.74	15.19	72.73
STAKE 827	2086163	748442	0.22	4.18		19.25	142.17	10.04	39.44
STAKE 828	2086153	748473.7	0.24	4.43		21.28	154.73	12.40	54.73
STAKE 829	2086143	748419.8	0.22	2.55		19.58	144.22	10.42	41.95
STAKE 830	2086131	748448.2	0.23	4.45		20.58	150.37	11.58	49.45
STAKE 831	2086108	748422	0.24	4.59		20.41	149.33	11.39	48.19
STAKE 832	2086167	748530	0.24	4.43		25.40	180.45	17.15	85.40
STAKE 833	2086145	748499.1	0.12	4.51	8.01	23.05	165.73	14.45	67.95
STAKE 834	2086124	748480.8	0.23	4.25		22.23	160.59	13.50	61.79
STAKE 835	2086092	748491.4	0.19	4.53		22.22	160.56	13.49	61.75
STAKE 836	2086098	748458.2	0.10	4.28		20.32	148.78	11.28	47.51
STAKE 837	2086066	748467.5	0.24			20.75	151.42		50.72
STAKE 838	2086217	748458.7	0.25	4.66		21.29	154.76	12.41	54.76
STAKE 839	2086227	748425.9	0.27	4.97		19.96	146.52	10.86	44.76
STAKE 840	2086241	748481.1	0.26	4.69		27.36	192.77	19.38	99.80
STAKE 841		748450.1	0.27	5.04		15.93	121.79	6.12	14.17
STAKE 842	2086272	748470.2	0.28	4.98		15.70	120.35	5.84	12.37
STAKE 843	2086264	748419	0.29	5.34		15.90	121.60	6.09	13.94
STAKE 844	2086268	748507.4	0.27	4.86		18.50	137.55	9.16	33.77
STAKE 845	2086297	748499.7	0.27	5.07		25.54	181.28		86.38
STAKE 846	2087230		0.22	4.20		30.91	215.31	23.39	125.69
STAKE 847	2087252		0.22	3.98		26.98	190.37	18.95	97.00
STAKE 848	L	749032.1	0.22	4.21		28.62	200.77	20.81	109.06
STAKE 849	2087287	749005.6	0.15	4.02		31.08	216.41	23.58	126.94
STAKE 850	2087272		0.23	4.29		29.73	207.79	22.06	117.12
STAKE 851	2087289		0.22	3.98		16.55	125.58	6.86	18.92
STAKE 852	2087305		0.23	4.22		30.59	213.25	23.03	123.34
STAKE 853	2087326	748947	0.11	3.96		29.46	206.06	21.75	115.13
STAKE 854	2087316		0.24			25.40	180.46	17.15	85.41
STAKE 855	2087343		0.23			28.01	196.92	20.12	104.60
STAKE 856	2087331	748888.5	0.25			23.07	165.82	14.47	68.05
									82.83
									52.08
STAKE 850 STAKE 857 STAKE 858	2087366 2087352			4.12	9.85	25.06 20.93	178.28 152.54	16.75	82.8

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						95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 859	2087386	748864.3	0.24	4.29		22.84	164.40	14.20	66.35
STAKE 860	2087302	749039.4	0.22	4.13		31.02	216.00	23.51	126.47
STAKE 861	2087334	749026.8	0.09	3.83		25.06	178.32	16.76	82.88
STAKE 862	2087307	749005.3	0.23	4.15		28.12	197.57	20.24	105.36
STAKE 863	2087349	748994.2	0.21	3.89		28.09	197.42	20.21	105.19
STAKE 864	2087338	748974.5	0.23	4.27	15.36	31.14	216.76	23.64	127.33
STAKE 865	2087373	748972.3	0.21	3.86		26.28	186.00	18.16	91.90
STAKE 866	2087357	748952.8	0.12	4.25		28.58	200.46	20.76	108.70
STAKE 867	2087390	748943.9	0.22	4.06	10.70	25.99	184.12	17.82	89.70
STAKE 868	2087373	748917.1	0.24	4.30	13.45	29.01	203.24	21.25	111.89
STAKE 869	2087405	748916.2	0.22	3.98		24.75	176.35	16.40	80.57
STAKE 870	2087390	748887.7	0.27	4.74	12.23	27.67	194.73	19.73	102.07
STAKE 871	2087425	748885.8	0.22	3.96	4	24.67	175.87	16.31	80.00
STAKE 872	2087406	748856.9	0.26	4.79	11.74	27.13	191.31	19.12	98.10
STAKE 873	2087445	748800.5	0.12	3.30	6.73	21.66	157.10	12.85	57.59
STAKE 874	2087428	748829.3	0.26	4.78		24.23	173.09	15.80	76.70
STAKE 875	2087403	749028.5	0.21	3.88	13.06	28.59	200.55	20.77	108.80
STAKE 876	2087368	749028.8	0.24	4.49	18.11	34.22	236.52	27.08	149.54
STAKE 877	2087417	748995.7	0.14	3.87	13.18	28.72	201.37	20.92	109.74
STAKE 878	2087387	748996.6	0.22	4.16	13.01	28.52	200.14	20.70	108.33
STAKE 879	2087438	748967.9	0.22	3.89	13.11	28.64	200.88	20.83	109.18
STAKE 880	2087406	748971.2	0.23	4.39	8.54	23.63	169.37	15.12	72.28
STAKE 881	2087456	748942.7	0.20	3.81	6.56	21.49	156.00	12.64	56.26
STAKE 882	2087419	748940.6	0.23	4.38	10.69	25.97	184.04	17.80	89.61
STAKE 883	2087440	748909.2	0.21	3.84	8.01	23.06	165.77	14.46	68.00
STAKE 884	2087474	748910.6	0.24	4.43	11.34	26.69	188.56	18.62	94.90
STAKE 885	2087455	748878	0.22	3.97	7.25	22.22	160.58	13.49	61.78
STAKE 886	2087476	748845.4	0.26	4.85	8.50	23.59	169.07	15.07	71.93
STAKE 887	2087446	749005.8	0.21	3.80	13.78	29.38	205.58	21.67	114.58
STAKE 888	2087461	748974.6	0.24	4.54	13.74	29.33	205.28	21.62	114.23
STAKE 889	2087485	748948.2	0.21	3.85	9.05	24.18	172.80	15.75	76.36
STAKE 890	2087498	748976.8	0.13	4.65	15.99	31.85	221.29	24.44	132.46
STAKE 891	2087507	748919.9	0.21	3.85	8.47	23.55	168.85	15.02	71.66
STAKE 892	2087518	748952.1	0.23	4.27	11.05	26.36	186.50	18.25	92.49
STAKE 893	2087560	748899.1	0.20	3.61	5.22	20.04	147.05	10.96	45.41
STAKE 894	2087540	748925.5	0.23	4.41	10.85	26.14	185.11	18.00	90.87
STAKE 895	2087530	748984.5	0.21	3.92	9.90	25.11	178.61	16.81	83.22
STAKE 896	2087511	749008.4	0.24	4.39	15.83	31.66	220.10	24.23	131.12
STAKE 897	2087383	749160.8	0.19	2.91	10.76	26.05	184.55	17.89	90.21
STAKE 898	2087402	749129.3	0.21	4.12	11.12	26.44	186.99	18.34	93.06
STAKE 899	2087417	749167.5	0.23	4.11	0.94	15.50	119.15	5.61	10.86
STAKE 900	2087437	749144	0.21	4.04	10.02	25.25	179.46	16.97	84.23
STAKE 901	2087444		0.20	3.94			119.04	5.59	10.72
STAKE 902	2087463	749150.1	0.27	4.83		15.83	121.17	6.00	
STAKE 903	2087493		0.17	4.02	d	14.92	115.63	4.92	6.42
STAKE 904	2086777	748558.2	0.25			22.43	161.84	13.73	
STAKE 905	2086808	748549	0.23			26.03	184.38	17.86	
STAKE 906	2086843		0.24		1	25.99	184.13	17.82	
STAKE 907	2086881	748537.2	0.22			19.87	145.96	10.75	
STAKE 908	2086888	748504.3			,	20.44	149.48	11.42	
STAKE 909	2086906	748527	0.23	4.17	5.42	20.26	148.42	11.22	47.07

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	1					95% UCL	95% UCL	Best Fit	Best Fit
						Predicted	Predicted	Predicted	Predicted
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Pu-239/240
STAKE 910	2086863	748480.9	0.25	4.76		22.87	164.63	14.25	66.63
STAKE 911	2086850	748511.1	0.23	4.34		22.68	163.41	14.02	65.17
STAKE 912	2086832	748485.1	0.26	4.71	9.63	24.82	176.77	16.48	81.06
STAKE 913	2086819	748518.2	0.23	4.26		25.97	184.04	17.80	89.61
STAKE 914	2086848	748456.1	0.26	4.97	7.65	22.66	163.30	14.00	65.04
STAKE 915	2086814	748457.2	0.25	4.50		22.58	162.81	13.91	64.46
STAKE 916	2086931	748613.9	0.24	4.55		23.14	166.27	14.55	68.60
STAKE 917	2086536	748395.5	0.23	4.14		20.26	148.42	11.22	47.07
STAKE 918	2086941	748701	0.27	4.89		24.54	175.01	16.16	78.98
STAKE 919	2086928	748733.2	0.25	4.43		18.66	138.54	9.34	34.98
STAKE 920	2086972	748698.8	0.27	4.86		15.87	121.38	6.04	13.66
STAKE 921	2086961	748730.5	0.16	4.50		15.75	120.67	5.91	12.76
STAKE 922	2086901	748707	0.21	3.89		25.26	179.55	16.99	84.34
STAKE 923	2087197	748973.9	0.22	4.18		15.71	120.45	5.86	12.49
STAKE 924	2087161	748981.7	0.22	4.03		18.09	134.99	8.67	30.61
STAKE 925	2087203	748943.9	0.24	4.25		15.71	120.42	5.86	12.45
STAKE 926	2087180	748943	0.24	4.37	3.84	18.56	137.93	9.23	34.23
STAKE 927	2087182	748912.9	0.26	4.79		16.74	126.70	7.07	20.31
STAKE 928	2087210	748906	0.11	4.01	6.81	21.76	157.68	12.95	58.29
STAKE 929	2087195	748880.8	0.26	4.72	1.15	15.72	120.51	5.87	12.57
STAKE 930	2087227	748877	0.20	2.88	0.71	15.26	117.68	5.32	9.01
STAKE 931	2087209	748847.9	0.26	4.64		16.36	124.39	6.63	17.43
STAKE 932	2087239	748843.7	0.36	3.96		18.56	137.87	9.22	34.16
STAKE 933	2087223	748808.9	0.23	4.09		15.69	120.33	5.84	12.34
STAKE 934	2087249	748809.8	0.25	4.38	3.26	17.95	134.13	8.50	29.54
STAKE 935	2087270	748785.6	0.22	3.90	2.02	16.64	126.09	6.96	19.56
STAKE 936	2087236	748778.7	0.28	4.95	1.30	15.88	121.45	6.06	13.74
STAKE 937	2087308	748790.2	0.18	4.02	0.91	15.47	118.96	5.57	10.61
STAKE 938	2087301	748764.3	0.25	4.59	5.53	20.38	149.12	11.35	47.93
STAKE 939	2087335	748804.8	0.23	4.00	0.81	15.36	118.32	5.45	9.81
STAKE 940	2087332	748771.9	0.25	4.65	4.53	19.30	142.47	10.09	39.81
STAKE 941	2087313	748827.6	0.22	4.02	2.04	16.65	126.21	6.98	19.70
STAKE 942	2087342	748837.6	0.25	4.62	3.22	17.91	133.88	8.46	29.24
STAKE 943	2087314	748858.2	0.22	3.93	5.81	20.67	150.95	11.69	50.16
STAKE 944	2087296	748888	0.25	4.49	7.09	22.05	159.52	13.30	60.50
STAKE 945	2087287	748919.7	0.22	3.82	6.58	21.51	156.15	12.67	56.45
STAKE 946	2087258	748935.6	0.16	4.52	4.62	19.40	143.08	10.21	40.56
STAKE 947	2087248	748968.4	0.17	3.98	5.37	20.21	148.06	11.15	46.63
STAKE 948	2087224	748994.3	0.26	4.75	11.25	26.58	187.88	18.50	94.10
STAKE 949	2087034	748860.4	0.25	4.37	1.01	15.57	119.56	5.69	11.37
STAKE 950	2087072	748871.9	0.30	5.42	2.64	17.29	130.12	7.73	24.58
STAKE 951	2087061	748842.1	0.28	4.87	1.74	16.34	124.26	6.60	17.27
STAKE 952	2087037	748824.3	0.29	5.26	1.84	16.44	124.91	6.73	18.08
STAKE 953	2087526	749038.4	0.21	4.08	3.81	18.54	137.79	9.20	34.05
STAKE 954	2087534	749073.4	0.21	4.00	1.08	15.65	120.04	5.78	11.97
STAKE 955	2087537	749011.5	0.21	3.72	4.82	19.62	144.41	10.46	42.19
STAKE 956	2087555	749040.9	0.25	4.49	1.15	15.72	120.47	5.87	12.52
STAKE 957	2087576	749012.1	0.19	3.52	0.85	15.40	118.54	5.49	10.09
STAKE 958	2087586	749039.6	0.24	4.41	1.13	15.70	120.34	5.84	12.36
STAKE 959	2087610	749013.9	0.20	3.63	0.81	15.37	118.33	5.45	9.82
STAKE 960	2087576	749009.9	0.21	4.00	1.06	15.63	119.92	5.76	11.83

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						95% UCL	95% UCL	Best Fit	Doot Fit
						Predicted	Predicted	Predicted	Best Fit
STAKE NUMBER	Easting	Northing	U-235	U-238	Am-241	Am-241	Pu-239/240	Am-241	Predicted Pu-239/240
STAKE 961	2087587	748960.4	0.19	3.56	0.79	15.34	118.19	5.42	9.65
STAKE 962	2087555	748958.3	0.15	4.67	9.31	24.46	174.55	16.07	78.43
STAKE 963	2086065	748808.7	0.32	3.85	6.17	21.06	153.35	12.14	53.06
STAKE 964	2086033	748809.2	0.25	4.71	22.90	39.68	271.83	33.08	188.26
STAKE 965	2086052	748838.4	0.24	4.24	24.75	41.82	285.77	35.39	203.20
STAKE 966	2086018	748836.1	0.26	4.83	31.63	49.89	339.09	44.00	258.83
STAKE 967	2086036	748864.6	0.23	4.16	3.27	17.96	134.22	8.52	29.66
STAKE 968	2086000	748865.6	0.24	4.41	4.12	18.87	139.80	9.59	36.54
STAKE 969	2086095	748862.1	0.25	4.40	10.87	26.17	185.28	18.03	91.06
STAKE 970	2086061	748862.4	0.19	4.77	7.39	22.38	161.54	13.67	62.93
STAKE 971	2086109	748833.6	0.23	4.23	33.93	52.64	357.43	46.88	277.43
STAKE 972	2086076	748833.6	0.26	4.83	20.92	37.42	257.14	30.61	172.30
STAKE 973	2086126	748805.1	0.21	3.84	36.69	55.95	379.69	50.32	299.65
STAKE 974	2086094	748804.7	0.23	4.40	12.87	28.38	199.20	20.53	107.24
STAKE 975	2086198	748811.7	0.22	3.98	14.59	30.28	211.27	22.68	121.09
STAKE 976	2086159	748806.9	0.22	4.36	23.34	40.19	275.11	33.62	191.79
STAKE 977	2087577	748929.1	0.22	4.03	1.12	15.68	120.26	5.83	12.25
STAKE 978	2087607	748930.5	0.22	4.14	1.12	15.69	120.31	5.83	12.31
STAKE 979	2087533	748892.6	0.23	4.28	9.97	25.19	179.12	16.91	83.83
STAKE 980	2087587	748873.1	0.24	4.31	1.10	15.67	120.19	5.81	12.17
STAKE 981	2087523	748859.2	0.23	4.32	6.21	21.10	153.63	12.20	53.39
STAKE 982	2087562	748984.1	0.21	3.96	1.72	16.32	124.14	6.58	17.12
STAKE 983	2085961	748811.2	0.27	4.91	3.16	17.85	133.52	8.39	28.79
STAKE 984	2085993	748810.6	0.25	4.70	17.02	33.00	228.66	25.72	140.76
STAKE 985	2086149	748839.1	0.24	4.54	21.60	38.20	262.18	31.46	177.80
STAKE 986	2086173	748836.5	0.25	4.70	20.35	36.77	252.93	29.89	167.69
STAKE 987	2086220	748837.2	0.24	4.54	24.35	41.36	282.78	34.90	200.01
STAKE 988	2086250	748838	0.24	4.55	32.85	51.35	348.79	45.53	268.70
STAKE 989	2086235	748808.2	0.21	3.98	7.85	22.88	164.67	14.25	66.67
STAKE 990	2086368	748853.4	0.24	4.56	38.38	58.01	393.55	52.44	313.32
STAKE 991	2086391	748876.5	0.25	4.59	16.09	31.96	222.00	24.56	133.27
STAKE 992	2086336	748865.9	0.23	4.47	43.74	64.60	438.43	59.15	356.64
STAKE 993	2086349	748882.5	0.22	4.19	48.36	70.38	478.23	64.93	393.98
STAKE 994	2086303	748870.9	0.24	4.44	9.43	24.59	175.38	16.22	79.42
STAKE 995	2086326	748894.3	0.12	4.11	7.14	22.11	159.84	13.36	60.89
STAKE 996	2085772	748593	0.25	4.56	1.20	15.77	120.81	5.93	12.94
STAKE 997	2085797	748592.9	0.11	4.19	0.78	15.32	118.08	5.40	9.50
STAKE 998	2085736	748595.3	0.25	4.61	2.37	17.01	128.36	7.39	22.39
STAKE 999	2085748	748566.4	0.22	3.93	0.92	15.48	119.01	5.58	10.68

								7	Pu			
						U-233/234	U-235	U-238	239/240	Am-241	RFCA Tier I	RFCA Tier II
Borehole	EASTING	NORTHING	Material	Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
86006	2085611	749212 asphalt	phalt	9.0-0.0	PCI/G	606.0	0.034	0.888	0.042	0.065	0.003	0.015
90198	2085686		sphalt	0.0-0.5	PCI/G	0.842	0.039	0.919	0.029	0.015	0.002	0.014
90398	2085835	749215 asphalt	sphalt	0.0-0.4	PCI/G	0.746	0.041	0.791	0.097	0.043	0.002	0.013
86906	2085685	749139 asphalt	sphalt	0.0-0.5	PCI/G	0.672	0.038	0.607	0.001	0.016	0.002	0.010
90798	2085760	749137 asphalt	sphalt	0.0-0.4	PCI/G	0.859	0.035	0.851	0.01	0.053	0.002	0.014
91198	2085685	749064 asphalt	sphalt	0.0-0.4	PCI/G	0.782	0.012	0.736	0.047	0.03	0.002	0.011
91298	2085760	749062 asphalt	sphalt	0.0-0.5	PCI/G	0.665	0.04	0.596	-0.002	0.048	0.002	0.011
91898	2085834		sphalt	9.0-0.0	PCI/G	1.13	0.133	0.75	1.22	0.341	0.005	0.030
91998	2085909	748990 asphalt	sphalt	0.0-0.5	PCI/G	0.663	0.049	0.598	0.034	0.022	0.002	0.011
96098	2085612	749211 bedrock	drock	15.8-16.0	PCI/G	0.185	-0.006	0.215	0.042	-0.049	0.000	0.001
96198	2085687	749213 bedrock	drock	15.5-15.8	PCI/G	0.412	0.047	0.707	0.25	0.036	0.002	0.012
96298	2085611	749135 bedrock	drock	15.9-16.1	PCI/G	0.515	0.064	0.795	0.008	0.007	0.002	0.012
96398	2085610	749061 bedrock	drock	16.0-16.2	PCI/G	0.731	0.073	0.69	0.041	0.007	0.002	0.012
96498	2085910		drock	21.4-22.0	PCI/G	0.538	0.009	0.782	0.186	0.075	0.002	0.012
96298	2085867	749147 bedrock	drock	22.7-22.9	PCI/G	0.904	0.063	0.842	0.044	0.017	0.003	0.014
96698	2085846	749128 bedrock	drock	22.8-23.0	PCI/G	0.603	0.113	0.43	0.048	0	0.002	0.011
96898	2085713	749095 bedrock	drock	16.2-16.4	PCI/G	0.402	0.048	0.388	0.357	0.207	0.002	0.014
96998	2085711	749038 bedrock	drock	17.5-17.6	PCI/G	0.337	0.01	0.693	0.008	0.076	0.002	0.010
92008	2085611	748986 bedrock	drock	16.2-16.5	PCI/G	0.444	0.017	0.618	0.032	0.054	0.002	0.010
97198			drock	24.2-24.4	PCI/G	0.404	0.015	0.526	0.038	0	0.001	0.007
97298	2085930	748844 bedrock	drock	17.9-18.1	PCI/G	0.358	0.054	0.748	0.019	0.068	0.002	0.013
86006	2085611	749212 fill		0.6-1.0	PCI/G	0.837	0.077	1.09	2.93	0.655	0.008	0.045
90198		749214 fill		0.5-0.9	PCI/G	0.913	0.033	0.857	2.62	0.536	0.007	0.037
90298	2085761	749211 fill		0.5-0.8	PCI/G	1.06	0.051	1.24	20.5	5.21	0.042	0.236
90398				0.4-0.8	PCI/G	0.837	0.029	0.939	1.37	0.309	0.005	0.027
86906				0.5-0.8	PCI/G	0.956	0.035	1.21	0.686	0.105	0.004	0.022
90798	2085760	749137 fill		0.4-0.8	PCI/G	1.08	0.079	1.08	8.13	1.7	0.017	0.094
91198				0.4-0.9	PCI/G	0.728	0.042	0.844	4.6	0.908	0.010	0.054
91298		·		0.5-1.0	PCI/G	1.12	0.066	1.24	7.45	1.41	0.015	0.085
91798	2085759	748989 fill		0.5-1.1	PCI/G	1.22	0.055	1.16	4.36	0.801	0.010	0.056
91898	2085834	748990 fill		0.6-1.1	PCI/G	2.02	0.487	2.77	558	126	0.986	5.584
91998	2085909			0.5-0.9	PCI/G	0.907	0.058	0.174	0.41	0.084	0.002	0.011
92298		748914 fill		0.5-0.9	PCI/G	0.997	0.066	1.2	34	6.43	0.057	0.322
91198			ative		PCI/G	0.412	0	0.613	0.01	0.02	0.001	0.008
91198			ative	15.1-15.5	PCI/G	0.467	0.04	0.574	0.073	0.028	0.002	0.010
91198	2085685	749064 native	ative	18.6-19.1	PCI/G	0.48	0.031	0.603	0.009	0.007	0.002	0.00

						11-233/234	U-235	11-238	Pu 239/240	Am-241	RECA Tier I	RECA Tier II
Borehole	EASTING	NORTHING	Material	Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
91198	2085685	749064 native	native	19.8-20.2	PCI/G	0.578	0.037	0.698	0.047	0.077	0.002	0.012
91198	2085685	749064 native	native	7.4-7.7	PCI/G	0.315	0.009	0.341	0.009	0.007	0.001	0.005
92598	2085560	749064 native	native	12.0-12.5	PCI/G	0.379	0.027	4.0	0.056	0.041	0.001	0.008
92598	2085560	749064 native	native	16.0-16.75	PCI/G	0.353	0.027	0.437	0.033	-0.005	0.001	0.007
92598	2085560	749064 native	native	3.5-4.0	PCI/G	0.491	0.017	0.532	0.609	0.072	0.002	0.012
92598	2085560	749064 native	native	7.5-8.0	PCI/G	0.433	0.024	0.455	0.021	0.016	0.001	0.007
95998	2085893	749140 native		. 12.2-12.4	PCI/G	0.475	0.137	0.61	0.027	0.035	0.003	0.014
95998	2085893	749140 native	native	15.2-15.4	PCI/G	0.572	0.118	0.773	0.004	0	0.003	0.014
95998	2085893	749140 native	native	17.5-17.9	PCI/G	9.0	0.106	0.483	0.023	0	0.002	0.011
95998	2085893	749140 native	native	20.2-20.6	PCI/G	0.455	0.21	1.08	-0.019	0.016	0.004	0.021
95998	2085893	749140 native	native	4.8-5.0	PCI/G	0.315	0.194	0.657	-0.003	0	0.003	0.015
95998	2085893	749140 native	native	8.2-8.4	PCI/G	0.636	0.147	0.692	0	0.033	0.003	0.016
96098	2085612	749211 native	native	12.3-12.5	PCI/G	0.743	0.015	1.35	0.602	0.844	0.007	0.041
96098	2085612	749211 native	native	4.3-4.5	PCI/G	0.312	0.033	0.705	0.047	0.003	0.002	0.010
96098		749211 native	native	8.2-8.5	PCI/G	0.386	0	0.583	0.067	0.079	0.002	0.00
96198	2085687	749213 native	native	11.8-12.0	PCI/G	909'0	0.025	0.688	0.231	0.103	0.002	0.013
96198	2085687	749213 native	native	4.2-4.4	PCI/G	0.505	0.017	0.677	0.021	0.083	0.002	0.011
96198	2085687	749213 native	native	7.7-8.1	PCI/G	0.539	0.016	0.484	0.093	0.075	0.002	0.009
96298	2085611	749135 native	native	11.9-12.25	PCI/G	0.546	0.016	0.752	0.068	0.075	0.002	0.012
96298	2085611	749135 native	native	4.0-4.3	PCI/G	0.585	0.003	0.848	2.84	0.323	0.005	0.030
96298	2085611	749135 native	native	7.0-8.0	PCI/G	0.656	0.113	1.06	1.63	1.8	0.013	0.071
96398		749061 native	native	12.2-12.4	PCI/G	0.588	0.046	0.715	1.83	0.677	900'0	0.036
96398	2085610	749061 native	native	4.0-4.3	PCI/G	0.539	0.016	0.563	1.99	0.231	0.004	0.022
96398		749061 native	native	8.2-8.4	PCI/G	0.309	0.05	0.442	0.522	0.188	0.003	0.014
96498	2085910	749141 native	native	12.2-13.0	PCI/G	0.382	0.012	0.562	0.077	0.051	0.002	0.009
96498	2085910	749141 native	native		PCI/G	0.45	0.033	0.544	0.504	0.191	0.003	0.015
96498	2085910	749141 native	native	17.7-18.0	PCI/G	0.366	0.01	0.468	0.361	0.101	0.002	0.010
96498		749141 native	native	4.4-4.8	PCI/G	0.349	0.027	0.296	1.1	0.132	0.002	0.013
96498	2085910	749141 native	native	9.0-9.5	PCI/G	0.398	0.031	0.533	0.528	90.0	0.002	0.011
96298	2085867	749147 native	native	11.4-11.6	PCI/G	0.422	0.04	0.55	0.032	0.011	0.002	0.009
96298	2085867	749147 native	native	15.6-15.8	PCI/G	0.589	0.019	0.654	0.031	0.05	0.002	0.010
96598	2085867	749147 native	native	18.4-18.6	PCI/G	0.43	0	0.449	0.027	0	0.001	900'0
96298	2085867	749147 native	native	4.0-4.2	PCI/G	0.417	0.033	0.389	0.071	0	0.001	0.007
96298	2085867	749147 native	native	8.2-8.4	PCI/G	0.413	0.016	0.398	-0.006	0.016	0.001	900'0
86996	2085846	749128 native	native	12.2-12.4	PCI/G	0.403	0.003	0.542	0.00	0.008	0.001	0.007
96698	2085846	749128 native	native	17 5-17 7	PCI/G	0.629	0 0	0.678	0.01	2100	COOO	0.50

						U-233/234	U-235	U-238	239/240	Am-241	RFCA Tier I	RFCA Tier II
Borehole	EASTING	NORTHING	Material	Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
86996	2085846	749128 native	native	20.0-20.2	PCI/G	0.383	0.163	0.364	0.448	0.09	0.003	0.016
86996	2085846	749128 native	native	4.0-4.2	PCI/G	0.669	0.034	0.584	0.008	0	0.002	0.009
86996	2085846	749128 native	native	8.2-8.4	PCI/G	0.504	0.009	0.597	0.025	0.041	0.002	0.009
96298	2085866	749108 native	native	12.2-12.5	PCI/G	0.647	0.071	0.788	0.017	0.026	0.002	0.013
96798	2085866	749108 native	native	16.6-16.8	PCI/G	0.506	0.026	0.796	-0.008	0.036	0.002	0.011
96298	2085866	749108 native	native	20.0-20.4	PCI/G	0.578	0.055	0.52	0	0.053	0.002	0.011
96798	2085866	749108 native	native	4.2-4.4	PCI/G	1.4	0.097	1.46	· 0.017	0	0.004	0.023
96798	2085866	749108 native	native	8.2-8.4	PCI/G	0.281	0.019	0.693	0.047	0.018	0.002	0.009
96898	2085713	749095 native	native	12.1-12.3	PCI/G	0.389	0.016	0.325	0.121	0.295	0.002	0.013
96898		749095 native	native	4.2-4.4	PCI/G	0.479	0.003	0.54	0.348	0.098	0.002	0.011
96898	2085713	749095 native	native	8.2-8.4	PCI/G	0.435	600.0	0.495	0.459	0.044	0.002	0.010
86696	2085711	749038 native	native	12.2-12.4	PCI/G	0.614	0.032	0.69	0.013	-0.007	0.002	0.010
86696	2085711	749038 native	native	4.2-4.4	PCI/G	0.502	0.03	0.652	0.052	0.069	0.002	0.011
86696	2085711	749038 native	native	8.2-8.4	PCI/G	0.523	0.017	0.566	-0.006	0.002	0.001	0.008
92008	2085611	748986 native	native	12.2-12.4	PCI/G	0.82	0.00	0.783	0.198	0.05	0.002	0.013
92008	2085611	748986 native	native	4.0-4.2	PCI/G	0.472	-0.012	0.608	1.33	0.508	0.005	0.026
92008	2085611	748986 native	native	8.2-8.4	PCI/G	0.564	0.002	0.657	1.24	0.163	0.003	0.018
97198	2085611	748911 native	native		PCI/G	0.776	0.035	0.967	0.049	0.105	0.003	0.016
97198	2085611	748911 native	native	15.4-15.5	PCI/G	0.406	0	0.451	0.013	0.108	0.002	0.009
97198	2085611	748911 native	native		PCI/G	0.367	0.047	0.531	0.163	0.037	0.002	0.010
97198	2085611	748911 native	native	4.2-4.4	PCI/G	0.613	0.063	0.697	0.118	0.085	0.002	0.014
97198	2085611	748911 native	native	7.0-7.3	PCI/G	0.573	0.014	0.557	0.482	0.153	0.002	0.014
97298		748844 native	native	12.2-12.4	PCI/G	0.592	0.053	0.512	0.098	0.067	0.002	0.011
97298	2085930	748844 native	native	16.2-16.4	PCI/G	0.387	0.058	0.423	0.157	0.046	0.002	0.010
97298	2085930	748844 native	native	4.4-4.6	PCI/G	0.441	0.012	0.779	0.023	0.032	0.002	0.010
97298		748844 native	native	8.2-8.4	PCI/G	0.673	0.031	0.617	0.009	0.016	0.002	0.010
9298		749135 native	native	11.6-11.8	PCI/G	0.511	0.042	0.695	0.019	0	0.002	0.010
9298	2085880	749135 native	native	13.9-14.1	PCI/G	0.38	0.021	0.62	0	0	0.001	0.008
9298	2085880	749135 native	native	16.1-16.3	PCI/G	0.442	0.122	0.687	0.018	0.034	0.003	0.014
9298	2085880	749135 native	native	18.0-18.2	PCI/G	0.527	0.144	0.977	0.048	0.018	0.003	0.018
9298	2085880	749135 native	native	19.8-20.0	PCI/G	0.473	-0.01	0.486	0	0	0.001	900.0
9298	2085880	749135 native	native	4.2-4.6	PCI/G	0.519	0.122	0.5	90.0	0.011	0.002	0.012
9298	2085880	749135 native	native	8.6-8.8	PCI/G	0.4	0.08	0.538	0.021	0.039	0.002	0.011
86006		749212 native	native 1	1.0-1.5	PCI/G	1.14	0.071	1.68	4.85	0.958	0.012	0.067
90198		749214 native	native 1	0.9-1.4	PCI/G	1.58	0.384	1.9	711	87	0.909	5.150
90298	2085761	749211 native 1	native 1	0.8-1.1	בי/וטם	2.11	0.040	0	2770	0747	077 07	

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200602		۱ د		null code	pCI/g	B/IDd	6/10	PCI/g	PCI/g	(Sum of Ratio)	(Sum of Ratio)
200002		ाबा।४६ -	0.0-1.3	טן סיי	0.740	0.020	O.834	3.01	766.0	0.007	0.040
2085910	-	native 1	0.7-1.2	PCI/G	1.37	0.158	2.68	284	50.4	0.440	2.490
2085610	749137 native	native 1	1.1-1.6	PCI/G	0.842	0.038	1.59	142	33.9	0.261	1.475
2085685		native 1	0.8-1.5	PCI/G	5.14	0.577	7.92	10670	1880	16.232	91.933
2085760	749137 native	native 1	0.8-1.5	PCI/G	0.973	0.134	1.91	260	69.5	0.510	2.888
2085835	5 749140 native	native 1	0.9-1.4	PCI/G	3.56	0.169	5.21	685	158	1.226	6.945
2085910	749141 native	native 1	0.8-1.3	PCI/G	10.8	0.566	26.8	1210	268	2.149	12.173
2085610	749062 native	native 1	1.4-1.9	PCI/G	0.749	0.091	1.23	2500	377	3.506	19.860
91198 2085685	5 749064 native	native 1	0.9-1.3	PCI/G	0.848	0.032	1.54	125	21.8	0.192	1.089
91298 2085760	749062 native	native 1	1.0-1.5	PCI/G	0.798	0.066	1.51	242	36.3	0.342	1.936
91398 2085834	1 749065 native	native 1	0.8-1.3	PCI/G	178	16.9	780	0099	1210	11.805	66.889
91498 2085909		native 1	0.8-1.3	PCI/G	6.18	1.74	15.2	768	146	1.259	7.130
91598 2085610	748987 native	native 1	1.5-2.0	PCI/G	19.8	7.2	28.2	152260	31670	253.965	1438.266
91698 2085684	748989 native	native 1	0.9-1.4	PCI/G	1.83	-0.913	0.913	389	3930	18.547	104.941
91798 2085759		native 1	1.1-1.6	PCI/G	0.838	0.045	1.72	7960	535	8.062	45.688
		native 1	1.1-1.6	PCI/G	10.7	2.52	13.2	2420	554	4.318	24.450
91998 2085909		native 1	0.9-1.4	PCI/G	2.53	0.961	2.69	581	116	0.959	5.433
		native 1	0.9-1.4	PCI/G	1.3	0.038	1.03	0.969	12.4	0.061	0.346
92298 2085760		native 1	0.9-1.6	PCI/G	0.764	0.029	0.866	18	3.88	0.033	0.186
		native 1	0.7-1.2	PCI/G	1.37	0.048	0.62	104	19.8	0.167	0.946
92398 2085834		native 1	1.3-1.8	PCI/G	0.797	0.073	0.656	10	1.41	0.016	0.089
		native 1	1.1-1.6	PCI/G	0.758	0.092	1.1	474	59.5	0.611	3.464
92598 2085560		native 1	0.0-0.2	PCI/G	0.966	0.18	1.15	93.6	16.7	0.147	0.833
92698 2085551		native 1	0.0-0.4	PCI/G	0.788	0.062	0.789	5.83	0.99	0.011	0.062
***************************************		native 1	0.0-0.4	PCI/G	1.05	0.045	0.852	3.49	0.565	0.007	0.042
		native 1	0.5-1.0	PCI/G	_	0.038	0.994	0.817	0.154	0.004	0.022
		native 1	0.0-0.5	PCI/G	0.418	0.016	0.494	90.5	15.6	0.137	0.775
		native 1	0.0-0.5	PCI/G	0.866	0.017	0.863	37.6	7.86	0.065	0.368
		native 1	0.0-0.5	PCI/G	1.29	-0.196	2.53	808	128	1.164	6.595
	·	native 1	0.0-0.5	PCI/G	0.963	0.051	1.42	45.9	9.3	0.079	0.446
93398 2085857		native 1	0.0-0.5	PCI/G	1.34	0.033	1.33	19.1	3.39	0.032	0.184
		748702 native 1	0.0-0.5	PCI/G	1.05	0.066	1.56	326	56.1	0.493	2.791
		native 1	0.0-0.4	PCI/G	0.893	0.169	1.82	417	80.5	0.671	3.801
		native 1	0.0-0.5	PCI/G	1.13	0.086	3.78	1170	225	1.873	10.608
93798 2086300		native 1	0.0-0.45	PCI/G	1.27	0.123	0.538	472	75.6	0.684	3.877
2086406		749003 native 1	0.0-0.5	PCI/G	0.803	0.017	1.16	196	35.9	0.307	1.737

					U-233/234	U-235	U-238	Pu 239/240	Am-241	RFCA Tier I	RFCA Tier II
Borehole	EASTING	NORTHING Material	Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
93398	2086000	749123 native 1	0.0-0.5	PCI/G	0.98	0.053	1.15	39.3	8	0.068	0.383
94098	2086128	749117 native 1	0.0-0.4	PCI/G	35.8	4.17	7.5.7	14950	3140	25.247	142.982
94198	2086298	749123 native 1	0.0-0.4	PCI/G	1.13	0.051	1.66	229	35.7	0.330	1.870
94298	2086438	749112 native 1	0.0-0.5	PCI/G	0.859	0.033	1.03	56.3	10	0.088	0.501
94398	2085550	749129 native 1	0.0-0.3	PCI/G	1.06	0.032	1.06	2.32	0.497	0.007	0.037
94498	2085552	749264 native 1	0.0-0.3	PCI/G	0.949	0.096	0.949	4.9	0.839	0.010	0.058
. 94598	2085703	749265 native 1	0.0-0.5	PCI/G	0.801	0.014	0.995	19.2	2.91	0.029	0.166
94698	2085852	749265 native 1	0.0-0.45	PCI/G	0.822	0.034	0.905	9.32	2.14	0.019	0.106
94798	2086000	749266 native 1	0.0-0.5	PCI/G	0.587	0.064	0.795	30.6	5.05	0.047	0.267
94898	2086149	749243 native 1	0.0-0.4	PCI/G	0.798	0.056	1.32	362	80.8	0.632	3.581
94998	2086298	749244 native 1	0.0-0.5	PCI/G	0.997	0.085	1.31	162	36.7	0.288	1.628
95098	2086447	749243 native 1	0.0-0.5	PCI/G	-	-0.012	0.993	18.8	3.34	0.031	0.175
95198	2086149	749188 native 1	0.0-0.5	PCI/G	3.28	0.122	8.66	3300	980	6.420	36.353
95298	2086066	749123 native 1	0.0-0.5	PCI/G	0.78	0.062	0.827	10.6	1.96	0.019	0.107
95398	2086211	749120 native 1	0.0-0.5	PCI/G	1.94	0.188	6.34	978	182	1.544	8.746
95498	2086078	748987 native 1	0.0-0.45	PCI/G	0.772	0.022	1.01	49.8	8.51	7200	0.435
95598	2086229	748984 native 1	0.0-0.5	PCI/G	1.14	0.055	2.74	828	176	1.425	8.069
95698	2086077	749248 native 1	0.0-0.5	PCI/G	0.765	0.046	1.54	135	26.9	0.223	1.263
95798	2086148	749268 native 1	0.0-0.5	PCI/G	0.911	0.049	0.962	40.3	69.9	0.062	0.350
92838	2086219	749244 native 1	0.0-0.5	PCI/G	0.94	0.056	1.3	27.3	5.03	0.046	0.259
97398	2086096	748827 native 1	0.0-0.5	PCI/G	0.884	0.116	0.917	278	45	0.407	2.304
97498	2086182	748770 native 1	0.0-0.45	PCI/G	0.762	0.004	1.14	82.7	11.6	0.114	0.647
97598	2086247	748845 native 1	0.0-0.5	PCI/G	1.2	0.018	1.47	7.5.7	15.7	0.129	0.732
86006	2085611	749212 native 2	1.5-2.0	PCI/G	0.587	0.027	0.598	0.135	0.031	0.002	0.010
90198	2085686	749214 native 2	1.4-1.9	PCI/G	0.491	0.022	0.651	0.656	0.122	0.003	0.015
90298	2085761	749211 native 2	1.1-1.7	PCI/G	1.63	0.105	3.5	25	6.26	0.054	0.308
90398	2085835	749215 native 2	1.3-1.8	PCI/G	0.565	0.011	0.594	0.403	0.306	0.003	0.018
90498	2085910	749216 native 2	1.2-1.7	PCI/G	0.721	0.034	0.87	50.1	9.35	0.081	0.457
90298	2085610	749137 native 2	1.6-2.1	PCI/G	0.502	0.029	0.58	0.224	0.05	0.002	0.011
86906	2085685	749139 native 2	1.5-2.1	PCI/G	0.383	0.018	0.394	12.3	1.89	0.018	0.104
90798	2085760	749137 native 2	1.5-2.0	PCI/G	0.36	0.02	0.397	6.22	0.917	0.010	0.055
90898	2085835	749140 native 2	1.4-1.9	PCI/G	0.324	0.032	0.379	0.848	0.296	0.003	0.017
86606	2085910	749141 native 2	1.3-1.8	PCI/G	2.85	0.227	15.7	13.6	2.4	0.051	0.288
91098		749062 native 2	1.9-2.4	PCI/G	0.914	0.056	0.967	21.7	3.93	0.036	0.204
91198	2085685	749064 native 2	1.3-1.9	PCI/G	0.39	0.012	0.304	5.52	0.744	0.008	0.046
Q1208	2085760	749062 native 2	15-20	0/10	7000	0000	CFCC	7	000		

				. :	,	U-233/234	U-235	U-238	239/240	Am-241	RFCA Tier I	RFCA Tier II
Borehole	Щ	NORTHING		Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
91398			ative 2	1.3-1.8	PCI/G	0.436	0.065	0.721	201	10.3	0.191	1.080
91498	2085909		ative 2	1.3-1.8	PCI/G	0.723	0.045	2.35	9.1	1.69	0.019	0.108
91598	2085610	-	ative 2	2.0-2.5	PCI/G	0.977	0.137	1.12	167	33.2	0.275	1.556
91698	2085684	748989 native 2	ative 2	1.4-1.9	PCI/G	1.45	0.252	1.89	0.937	7.05	0.039	0.223
91798	2085759	748989 native 2	ative 2	1.6-2.0	PCI/G	0.537	0.046	0.771	5.98	1.08	0.011	0.063
91898	2085834	748990 native 2	ative 2	1.6-2.1	PCI/G	1.65	0.379	1.38	212	29.5	0.290	1.644
91998	2085909	748990 native 2	ative 2	1.4-1.9	PCI/G	4.11	6.57	8.51	1480	256	2.296	13.003
92098	2085609	748913 native	ative 2	1.4-1.9	PCI/G	0.904	0.022	0.72	0.381	0.172	0.003	0.017
92198	2085684	748914 native 2	ative 2	1.2-1.7	PCI/G	0.04	0.05	0.824	0.16	0.15	0.003	0.015
92298	2085760	748914 native 2	ative 2	1.6-2.0	PCI/G	0.963	0.043	0.996	1.79	0.28	0.005	0.029
92398	2085834	748915 native 2	ative 2	1.8-2.3	PCI/G	0.652	0.039	0.69	2.93	0.591	0.007	0.038
92498	2085909	748915 native 2	ative 2	1.6-2.1	PCI/G	0.56	0.045	0.54	0.408	0.055	0.002	0.012
92598	2085560	749064 native 2	ative 2	0.2-1.0	PCI/G	0.726	0.03	0.832	14	2.64	0.024	0.137
92698	2085551	748977 native	ative 2	0.4-0.9	PCI/G	0.442	0.022	0.516	1.22	0.345	0.004	0.021
92798	2085553	748827 native	ative 2	0.4-0.9	PCI/G	0.621	0.011	0.694	0.303	0.049	0.002	0.012
92898	2085703	748830 native	ative 2	1.0-1.5	PCI/G	0.926	0.051	0.972	0.932	0.177	0.004	0.023
92998	2085853	748830 native 2	ative 2	0.5-1.0	PCI/G	0.607	0.014	0.551	5.76	1.1	0.011	090.0
93098	2086005	748817 native 2	ative 2	0.5-1.0	PCI/G	0.961	0.066	0.877	6.1	1.33	0.013	0.074
93198	2086167	748839 native 2	ative 2	0.5-1.0	PCI/G	0.941	0.028	1.29	62.8	9.88	0.093	0.526
93298	2085755	748671 native	ative 2	0.5-1.0	PCI/G	0.825	-0.007	0.854	0.906	0.114	0.003	0.017
93398	2085857	748698 native 2	ative 2	0.5-1.0	PCI/G	1.27	0.046	1.25	1.87	0.45	0.007	0.037
93498	2086198	748702 native 2	ative 2	0.5-1.0	PCI/G	0.694	0.066	1.09	9.01	1.67	0.017	0.095
93298	2085978	748977 native 2	ative 2	0.4-0.8	PCI/G	0.499	0.015	0.522	9.34	1.25	0.014	0.077
93698	2086153	748988 native 2	ative 2	0.5-1.0	PCI/G	0.511	0.032	0.764	49.5	9.95	0.083	0.469
93798	2086300	748976 native	ative 2	0.45-0.9	PCI/G	0.413	0.033	0.369	4.12	0.957	0.008	0.048
93898	2086406	749003 native	ative 2	0.5-1.0	PCI/G	0.915	0.035	1.15	34.6	5.46	0.052	0.297
93998	2086000	749123 native 2	ative 2	0.5-1.0	PCI/G	0.492	0.029	0.541	4.64	0.668	0.008	0.044
94098	2086128	749117 native 2	ative 2	0.4-0.8	PCI/G	0.679	0.051	0.988	28.6	4.96	0.046	0.258
94198	2086298	749123 native 2	ative 2	0.4-0.8	PCI/G	0.569	0.028	0.545	13.9	2.51	0.023	0.130
94298	2086438		ative 2	0.5-1.0	PCI/G	0.862	0.049	0.911	25.4	2.93	0.034	0.192
94398	2085550	749129 native 2	ative 2	0.3-0.7	PCI/G	0.74	0.014	0.565	0.149	0.052	0.002	0.010
94498		749264 native	ative 2	0.3-0.8	PCI/G	0.876	0.061	0.729	1.26	0.302	0.004	0.025
94598			ative 2	0.5-1.0	PCI/G	0.918	0.038	1.03	11.4	2.44	0.022	0.124
94698	2085852		ative 2	0.45-0.9	PCI/G	0.662	0.072	0.811	23.3	3.43	0.035	0.196
94798	2086000	749266 native 2	ative 2	0.5-1.0	PCI/G	0.725	0.066	0.883	27	4.47	0.042	0.238
OOOFO	077000	7402/3 pative 2	otive 2	8070	ט כי	101	7200	000	705		101	,,,,

U-235         U-236         Z39/Z40         Am-241         RFCA Tietrol         RFCA Tietrol         CATOLIGA           DC0023         1.5         pCl/g         pCl/g         Commof Ratio)         (Sum of Ratio)         (Sum of Ratio)           0.0023         0.875         0.814         0.096         3.176         1           0.0024         0.875         1.820         406         3.176         1           0.0077         1.06         37.6         8.42         0.068         1           0.0077         1.06         37.6         8.42         0.068         1           0.0077         1.06         37.6         8.42         0.068         0.006           0.007         1.24         4.12         8.95         0.007         0.007           0.018         1.24         4.12         8.95         0.004         0.004           0.018         1.24         4.2         0.028         0.004         0.004           0.018         1.24         4.5         0.72         0.004         0.004           0.023         1.06         4.5         0.72         0.004         0.004           0.024         0.057         0.081         0.044										Pu			
RASTING NORM-HIND MARINED MARIN							U-233/234	U-235	U-238	239/240	Am-241	RFCA Tier I	RFCA Tier II
2086249 AgAL-flative 2         0.5-1.0 D PCI/IG         1.19 D 0.023         1.15 D 0.004         4.4 D 0.004         0.004           2086440 AgAL-flative 2         0.5-1.0 P PCI/IG         0.755 D 0.002         0.15 D 0.004         0.003         0.15 D 0.004         0.003           2086140 AgAGLATIR Intere 2         0.5-1.0 P PCI/IG         0.26 D 0.15 D 0.004         0.006         0.003           2086060 7-449178 Intere 2         0.5-1.0 P PCI/IG         1.26 D 0.007         0.067 D 0.004         0.006         0.008           2086077 7-44918 Intere 2         0.5-1.0 P PCI/IG         1.26 D 0.007         0.07 D 0.009         0.009         0.009           2086077 7-44918 Intere 2         0.5-1.0 P PCI/IG         1.26 D 0.004         0.009         0.007         0.009         0.009         0.009           2086077 7-44918 Intere 2         0.5-1.0 PCI/IG         0.409         0.009	Borehole	EASTING	Š	Material		unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
2086414         748245 januárus 2         0.5-1.0         PCI/G         2.025         0.026         0.054<	94998			native 2	0.5-1.0	PCI/G	1.19	0.023	1.5	192	44.4	0.344	1.950
2086149         749168         DCIA         0.154         0.004           2.086077         7.49246         native 2         0.54.10         PCI/G         0.154         0.044         0.048         0.048         0.006         0.006           2.086077         7.49246         native 2         0.54.10         PCI/G         0.908         0.048         1.04         0.008 <td>95098</td> <td></td> <td>749243</td> <td>native 2</td> <td>0.5-1.0</td> <td>PCI/G</td> <td>0.725</td> <td>0.002</td> <td>0.875</td> <td>0.814</td> <td>0.096</td> <td>0.003</td> <td>0.017</td>	95098		749243	native 2	0.5-1.0	PCI/G	0.725	0.002	0.875	0.814	0.096	0.003	0.017
2086066         749123 native 2         05-10         PCLIG         0.085         0.077         1.06         8.42         0.068           2086271         749123 native 2         0.5-10         PCLIG         1.63         0.047         1.07         683         1.36         1.121           2086272         748987 native 2         0.5-10         PCLIG         1.2         0.047         2.97         689         170         1.121           2086273         748984 native 2         0.5-10         PCLIG         0.412         0.047         2.97         689         170         1.070           2086148         749248 native 2         0.5-10         PCLIG         0.412         0.049         0.88         0.768         0.008           2086182         748270 native 2         0.5-10         PCLIG         0.933         0.028         1.98         0.768         0.008           2086182         748270 native 2         0.5-10         PCLIG         0.746         0.028         1.88         0.772         0.008           2086182         748270 native 2         0.5-10         PCLIG         0.746         0.048         0.78         0.008         0.008         0.707           2086182         748270 native 2 <td>95198</td> <td></td> <td>749188</td> <td>native 2</td> <td>0.5-1.0</td> <td>PCI/G</td> <td>2.05</td> <td>0.153</td> <td>6.79</td> <td>1820</td> <td>406</td> <td>3.176</td> <td>17.985</td>	95198		749188	native 2	0.5-1.0	PCI/G	2.05	0.153	6.79	1820	406	3.176	17.985
2086211         749120 native 2         0.5-1.0         PCI/G         1.63         0.087         5.07         669         170         1.266           20862728         748987 native 2         0.5-1.0         PCI/G         0.912         0.047         2.97         669         170         1.266           20862728         748984 native 2         0.5-1.0         PCI/G         0.912         0.018         1.2         4.12         0.329         0.004           2086748         7489248 native 2         0.5-1.0         PCI/G         0.915         0.018         1.2         4.12         0.329         0.004           2086748         74824 native 2         0.5-1.0         PCI/G         0.935         0.068         1.58         3.16         0.000           208678         74824 native 2         0.5-1.0         PCI/G         0.935         0.068         1.58         3.16         0.000           2086547         74824 native 2         0.5-1.0         PCI/G         0.99         0.18         1.87         3.86         0.07         0.000           2086547         74824 native 2         0.5-1.0         PCI/G         0.99         0.18         1.8         3.16         0.000           20865761	95298	Silverio de la companio del la companio de la compa		native 2	0.5-1.0	PCI/G	0.855	0.077	1.06	37.6	8.42	0.068	0.387
2086078         748987 native 2         0.45-0.9         PCI/G         0.047         2.97         669         17.0         1.266           20860778         748984 native 2         0.5-1.0         PCI/G         0.950         0.028         17.24         412         89.5         0.707           20860777         748248 native 2         0.5-1.0         PCI/G         0.950         0.049         0.896         15.0         0.004           2086178         74824 native 2         0.5-1.0         PCI/G         0.933         0.033         1.06         4.5         0.072           2086182         74827 native 2         0.5-1.0         PCI/G         0.933         0.063         1.06         4.5         0.072           2086182         74827 native 2         0.5-1.0         PCI/G         0.933         0.026         1.86         0.072         0.008           2086586         74827 native 2         0.5-1.0         PCI/G         0.79         0.026         0.657         0.009         0.000           208658         74824 native 2         0.5-1.0         PCI/G         0.78         0.026         0.057         0.001         0.002           208658         74824 native 3         1.7-2.4         PCI/G	95398		749120	native 2	0.5-1.0	PCI/G	1.63	0.087	5.07	683	136	1.121	6.347
2086279         748964 Inative 2         0.5-1.0         PCI/G         0.905         1.24         412         88.5         0.707           2086677         749246 Inative 2         0.5-1.0         PCI/G         0.412         0.018         1.2         3.86         0.788         0.004           2086148         749246 Inative 2         0.5-1.0         PCI/G         0.186         1.2         3.86         0.788         0.004           2086148         749246 Inative 2         0.5-1.0         PCI/G         0.905         0.049         1.5         3.16         0.002           2086189         748845 Inative 2         0.5-1.0         PCI/G         0.936         0.063         1.06         4.5         0.072         0.009           2086581         748845 Inative 2         0.5-1.0         PCI/G         0.94         0.026         0.567         0.005         0.005         0.004           2086581         74921 Inative 3         1.2-2         PCI/G         0.746         0.026         0.567         0.041         0.063         0.044         0.062         0.567         0.041         0.062         0.044         0.062         0.044         0.062         0.064         0.014         0.062         0.064         0.074 </td <td>95498</td> <td>***************************************</td> <td>748987</td> <td>native 2</td> <td>0.45-0.9</td> <td>PCI/G</td> <td>1.2</td> <td>0.047</td> <td>2.97</td> <td>699</td> <td>170</td> <td>1.265</td> <td>7.163</td>	95498	***************************************	748987	native 2	0.45-0.9	PCI/G	1.2	0.047	2.97	699	170	1.265	7.163
2086047         749249 Indive 2         0.5-1.0         PCI/G         0.412         0.008         0.397         1.9         0.229         0.004           2086148         749268 Indive 2         0.5-1.0         PCI/G         0.108         0.108         1.29         0.768         0.010           208618         749268 Indive 2         0.5-1.0         PCI/G         0.933         0.03         1.06         4.5         0.72         0.008           208688         74827 Indive 2         0.5-1.0         PCI/G         0.933         0.037         1.06         0.002         0.004           208688         74827 Indive 2         0.5-1.0         PCI/G         0.93         0.18         1.8         0.025         0.004           208688         74827 Indive 2         0.5-2.5         PCI/G         0.746         0.026         0.857         0.005         0.005           208680         74827 Indive 3         1.7-2.2         PCI/G         0.746         0.026         0.456         0.004         0.004           208680         74927 Indive 3         1.7-2.2         PCI/G         0.38         0.026         0.456         0.004         0.005         0.004           208680         74827 Indive 3         1.7	95598	*	748984	native 2	0.5-1.0	PCI/G	0.905	0.029	1.24	412	89.5	0.707	4.006
2086148         749268 Inative 2         05-1.0         PCI/G         1.18         0.108         1.2         3.98         0.768         0.010           20862148         749268 Inative 2         0.5-1.0         PCI/G         0.906         0.049         0.896         1.58         3.16         0.008           20860396         74827 native 2         0.5-1.0         PCI/G         0.936         0.085         0.062         0.009           2086182         748770 native 2         0.5-1.0         PCI/G         0.94         0.026         0.062         0.009           2086184         74871 native 3         1.5-2.4         PCI/G         0.446         0.05         0.087         0.006         0.005           2085868         74921 native 3         1.7-2.4         PCI/G         0.446         0.05         0.081         0.014         0.002           2085686         74921 native 3         1.7-2.4         PCI/G         0.485         0.026         0.044         0.002           2085610         74921 native 3         1.7-2.5         PCI/G         0.485         0.006         0.044         0.002           2085610         74921 native 3         1.7-2.5         PCI/G         0.446         0.026         0.044 <td>95698</td> <td>*</td> <td>749248</td> <td>native 2</td> <td>0.5-1.0</td> <td>PCI/G</td> <td>0.412</td> <td>0.018</td> <td>0.397</td> <td>1.9</td> <td>0.329</td> <td>0.004</td> <td>0.022</td>	95698	*	749248	native 2	0.5-1.0	PCI/G	0.412	0.018	0.397	1.9	0.329	0.004	0.022
2086219         7492241 native 2         0.5-1.0         PCI/G         0.996         0.049         0.886         1.5         3.16         0.028           20860696         7482271 native 2         0.5-1.0         PCI/G         0.933         0.063         1.06         4.4         0.027         0.009           2086247         748827 native 2         0.5-1.0         PCI/G         1.09         0.118         1.87         389         72.5         0.004           2086247         748241 native 2         0.5-1.0         PCI/G         0.746         0.026         0.083         0.005         0.001           20856761         74821 native 3         1.9-2.4         PCI/G         0.746         0.056         0.006         0.005           20856761         74821 native 3         1.7-2.4         PCI/G         0.486         0.016         0.043         0.001           20856761         74821 native 3         1.7-2.2         PCI/G         0.386         0.026         0.044         0.043         0.001           20856761         74821 native 3         1.7-2.2         PCI/G         0.38         0.026         0.245         0.041         0.002           20856861         74810-1         native 3         1.2-2.6	95798			native 2	0.5-1.0	PCI/G	1.18	0.108	1.2	3.98	0.768	0.010	0.056
2086056         748827 native 2         0.5-1.0         PCI/G         0.933         0.063         4.5         0.72         0.009           2086182         748770 native 2         0.5-1.0         PCI/G         1.09         0.127         1.10         0.489         0.082         0.004           2086182         748770 native 2         0.5-0.0         PCI/G         0.746         0.026         0.853         0.006         -0.006         0.002           2086561         749212 native 3         1.0-2.4         PCI/G         0.746         0.026         0.857         0.081         0.014         0.002           2085661         749214 native 3         1.7-2.4         PCI/G         0.38         0.017         0.373         0.041         0.003           2085691         749216 native 3         1.7-2.4         PCI/G         0.38         0.017         0.373         0.041         0.002           2085691         749216 native 3         1.7-2.4         PCI/G         0.38         0.017         0.373         0.041         0.002           2085691         749124 native 3         1.7-2.4         PCI/G         0.38         0.026         0.227         0.071         0.073           2085805         749140 native 3 </td <td>95898</td> <td></td> <td>ľ</td> <td>native 2</td> <td>0.5-1.0</td> <td>PCI/G</td> <td>0.905</td> <td>0.049</td> <td>0.896</td> <td>15.8</td> <td>3.16</td> <td>0.028</td> <td>0.160</td>	95898		ľ	native 2	0.5-1.0	PCI/G	0.905	0.049	0.896	15.8	3.16	0.028	0.160
2086182         748770 native 2         0.45-0.9         PCI/G         109         0.127         1.01         0.489         0.082         0.004           2086247         748845 native 2         0.5-1.0         PCI/G         0.79         0.118         1.87         389         72.5         0.614           2085686         742814 native 3         1.92-4         PCI/G         0.744         0.05         0.067         0.001         0.014         0.002           2085761         749214 native 3         1.72-4         PCI/G         0.783         0.026         0.456         0.004         0.014         0.002           2085761         749216 native 3         1.72-4         PCI/G         0.486         0.07         0.044         0.005           2085861         749137 native 3         1.72-2         PCI/G         0.386         0.07         0.037         0.002           2085861         749137 native 3         2.1-2.6         PCI/G         0.504         0.026         0.227         0.07         0.002           2085861         749137 native 3         2.0-2.5         PCI/G         0.504         0.026         0.227         0.07         0.02           2085861         74914 native 3         1.0-2.5	97398				0.5-1.0	PCI/G	0.933	0.063	1.06	4.5	0.72	600.0	0.053
2086247         748846 lative 2         16.1.0         PCI/IG         0.018         1.87         388         72.5         0.614           2086561         748846 lative 3         12.0.2.5         PCI/IG         0.746         0.056         0.005         0.002           20865681         749214 native 3         1.7.2.4         PCI/IG         0.444         0.05         0.644         0.0081         0.014         0.002           2086561         749214 native 3         1.7.2.4         PCI/IG         0.486         0.017         0.353         0.061         0.014         0.002           20856761         749216 native 3         1.7.2.2         PCI/IG         0.38         0.026         0.456         0.044         0.003           20856861         749137 native 3         2.1-2.8         PCI/IG         0.587         0.029         0.526         0.227         0.07         0.002           20856868         749136 native 3         1.9-2.4         PCI/IG         0.567         0.029         0.526         0.227         0.07         0.002           2085686         749137 native 3         1.9-2.4         PCI/IG         0.567         0.029         0.526         0.227         0.07         0.029           2085610	97498			native 2	0.45-0.9	PCI/G	1.09	0.127	1.01	0.489	0.082	0.004	0.023
2085681         749212         native 3         2.0-2.5         PCIVIG         0.746         0.026         0.867         0.006         -0.005         0.002           2085688         749214         native 3         1.9-2.4         PCIVIG         0.444         0.05         0.657         0.081         0.014         0.002           2085685         749214         native 3         1.7-2.4         PCIVIG         0.383         0.026         0.456         0.043         0.001           2085685         749216         native 3         1.7-2.2         PCIVIG         0.383         0.026         0.456         0.011         0.002           20856910         749216 native 3         2.1-2.6         PCIVIG         0.384         0.027         0.379         0.031         0.002           20856910         749137 native 3         2.1-2.6         PCIVIG         0.567         0.029         0.527         0.037         0.002           20858010         749140 native 3         1.9-2.4         PCIVIG         0.501         0.028         0.482         0.032         0.032         0.032           2085810         749140 native 3         1.9-2.4         PCIVIG         0.501         0.028         0.482         0.032         <	97598		748845	native 2	0.5-1.0	PCI/G	6.0	0.118	1.87	389	72.5	0.614	3.478
2085686         749214 native 3         1.9-2.4         PCI/IG         0.444         0.05         0.567         0.081         0.014         0.002           2088561         749214 native 3         1.7-2.4         PCI/IG         0.68         0.01         0.44         0.05         0.667         0.044         0.013           2088583         74921 native 3         1.7-2.2         PCI/IG         0.38         0.02         0.042         0.013         0.001           2088581         74921 native 3         2.1-2.6         PCI/IG         0.485         0.008         0.567         0.379         0.031         0.002           2088561         74913 native 3         2.1-2.6         PCI/IG         0.507         0.029         0.527         0.07         0.002           2088562         749140 native 3         2.1-2.8         PCI/IG         0.501         0.029         0.527         0.07         0.002           2088561         749140 native 3         1.9-2.4         PCI/IG         0.501         0.029         0.324         0.03         0.002           2088561         74916 native 3         1.8-2.3         PCI/IG         0.561         0.029         0.324         0.03         0.032           2088568	86006		749212		2.0-2.5	PCI/G	0.746	0.026	0.853	0.006	-0.005	0.002	0.012
2088761         749211 native 3         1.7-24         PCI/G         0.038         0.026         0.456         0.054         0.051         0.013           2088835         749216 native 3         1.7-22         PCI/G         0.393         0.026         0.456         0.044         0.043         0.001           2085810         749216 native 3         1.7-22         PCI/G         0.885         0.007         0.376         0.037         0.011         0.002           2085681         74917 native 3         2.1-2.6         PCI/G         0.507         0.029         0.526         0.227         0.07         0.002           2085682         749140         native 3         2.1-2.6         PCI/G         0.507         0.029         0.526         0.217         0.07         0.002           2085610         749140         native 3         2.0-2.5         PCI/G         0.501         0.029         0.526         0.027         0.002           2085610         74902         native 3         2.0-2.5         PCI/G         0.501         0.202         0.013         0.002           2085610         74902         native 3         2.0-2.6         PCI/G         0.561         0.029         0.526         0.022	90198				1.9-2.4	PCI/G	0.444	0.05	0.567	0.081	0.014	0.002	0.010
2085835         749215 native 3         1.8-2.3         PCI/G         0.393         0.026         0.456         0.044         0.043         0.001           2085810         749216 native 3         1.7-2.2         PCI/G         0.38         0.017         0.373         0.482         0.111         0.002           2085610         749137 native 3         2.1-2.6         PCI/G         0.686         0.029         0.526         0.227         0.07         0.002           2085760         749137 native 3         2.0-2.5         PCI/G         0.507         0.029         0.526         0.137         0.007         0.002           2085760         749140 native 3         1.9-2.4         PCI/G         0.501         0.028         0.492         0.032         0.019           2085760         749160 native 3         1.9-2.4         PCI/G         0.501         0.028         0.492         0.032         0.039           2085760         74916 native 3         1.9-2.5         PCI/G         0.501         0.028         0.344         9.24         0.002           2085810         74906 native 3         1.9-2.5         PCI/G         0.495         0.029         0.524         0.068         0.008           2085804	90298		749211	native 3	1.7-2.4	PCI/G	1.68	0.1	4	3.23	0.561	0.013	0.076
2085510         749216 native 3         1.7-2.2         PCI/G         0.38         0.017         0.373         0.482         0.111         0.002           2085610         74913 native 3         21-2.6         PCI/G         0.485         0.008         0.557         0.379         0.031         0.002           2085685         749139 native 3         21-2.6         PCI/G         0.567         0.022         0.013         0.002           2085858         749140 native 3         1.9-2.4         PCI/G         0.504         0.021         0.022         0.013         0.002           2085610         749141 native 3         1.9-2.4         PCI/G         0.504         0.027         0.035         0.089         0.002           2085610         749062 native 3         1.8-2.3         PCI/G         0.563         0.224         0.002         0.013           2085610         749062 native 3         1.9-2.5         PCI/G         0.263         0.054         0.027         0.002           2085610         749066 native 3         1.8-2.3         PCI/G         0.242         0.024         0.024         0.002           2085610         748066 native 3         1.8-2.4         PCI/G         0.495         0.024         0	90398		749215	native 3	1.8-2.3	PCI/G	0.393	0.026	0.456	0.044	0.043	0.001	0.008
2085610         749137 native 3         2.1-2.6         PCI/G         0.485         0.008         0.557         0.379         0.031         0.002           2085685         749137 native 3         2.1-2.8         PCI/G         0.567         0.029         0.556         0.227         0.07         0.002           2085760         74913 native 3         2.0-2.5         PCI/G         0.567         0.028         0.032         0.013         0.002           2085760         74914 native 3         1.9-2.4         PCI/G         0.561         0.024         0.032         0.032         0.032           2085610         749064 native 3         1.8-2.3         PCI/G         0.263         0.022         0.346         0.032         0.032           2085610         749062 native 3         1.9-2.5         PCI/G         0.263         0.022         0.346         0.037         0.098         0.002           2085634         749064 native 3         1.9-2.5         PCI/G         0.296         0.013         0.345         0.067         0.246         0.007           2085609         749066 native 3         1.8-2.3         PCI/G         0.246         0.021         0.245         0.067         0.045         0.002	90498		749216	native 3	1.7-2.2	PCI/G	0.38	0.017	0.373	0.482	0.111	0.002	0.010
2085685         749139 native 3         2.1-2.8         PCI/G         0.507         0.029         0.526         0.227         0.07         0.002           2085760         749137 native 3         2.0-2.5         PCI/G         0.364         0.021         0.456         0.202         0.113         0.002           2085835         749140 native 3         1.9-2.4         PCI/G         0.501         0.024         0.032         0.089         0.002           2085810         749141 native 3         1.8-2.3         PCI/G         0.512         0.374         0.089         0.002           2085810         749062 native 3         1.9-2.5         PCI/G         0.249         0.024         0.067         0.078         0.002           2085810         749062 native 3         1.9-2.5         PCI/G         0.249         0.024         0.067         0.278         0.002           2085610         749065 native 3         1.9-2.4         PCI/G         0.249         0.034         0.057         0.245         0.002           2085610         748086 native 3         1.9-2.4         PCI/G         0.346         0.024         0.024         0.024           2085624         748089 native 3         2.0-2.4         PCI/G <t< td=""><td>90598</td><td></td><td></td><td>native 3</td><td>2.1-2.6</td><td>PCI/G</td><td>0.485</td><td>0.008</td><td>0.557</td><td>0.379</td><td>0.031</td><td>0.002</td><td>0.010</td></t<>	90598			native 3	2.1-2.6	PCI/G	0.485	0.008	0.557	0.379	0.031	0.002	0.010
2085760         749137 native 3         2.0-2.5         PCI/G         0.364         0.021         0.456         0.202         0.113         0.002           2085835         749140 native 3         1.9-2.4         PCI/G         0.501         0.028         0.492         0.032         0.089         0.002           2085910         749141 native 3         1.9-2.4         PCI/G         0.501         0.028         0.492         0.032         0.089         0.002           2085610         749141 native 3         1.8-2.3         PCI/G         0.263         0.024         9.1         4.8.4         9.24         0.096           2085610         749062 native 3         1.9-2.5         PCI/G         0.263         0.022         0.524         0.067         0.278         0.002           2085610         749062 native 3         1.8-2.3         PCI/G         0.296         0.013         0.131         0.245         0.002           2085610         748066 native 3         1.8-2.3         PCI/G         0.296         0.028         0.327         0.162         0.002           2085610         748080 native 3         1.9-2.4         PCI/G         0.236         0.028         0.024         0.024         0.024	86906		749139	native 3	2.1-2.8	PCI/G	0.507	0.029	0.526	0.227	0.07	0.002	0.011
2085835         749140         native 3         1.9-2.4         PCI/G         0.501         0.028         0.492         0.032         0.089         0.002           2085910         749141         native 3         1.8-2.3         PCI/G         3.12         0.274         9.1         48.4         9.24         0.096           2085610         749062         native 3         1.8-2.3         PCI/G         1.15         0.059         1.32         1.44         2.86         0.027           2085685         749062         native 3         1.9-2.5         PCI/G         0.263         0.022         0.368         0.934         0.098         0.002           2085687         749062         native 3         1.9-2.5         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           2085876         749066         native 3         1.8-2.3         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           2085610         748089         native 3         1.9-2.4         PCI/G         0.246         0.021         0.246         0.024         0.057           2085684         748899         native 3         1.9-2.4	90798		749137	native 3	2.0-2.5	PCI/G	0.364	0.021	0.456	0.202	0.113	0.002	0.010
2085910         749141         native 3         1.8-2.3         PCI/G         3.12         0.274         9.1         48.4         9.24         0.096           2085610         749062         native 3         2.4-2.9         PCI/G         1.15         0.059         1.32         14.4         2.86         0.027           2085685         749062         native 3         2.4-2.9         PCI/G         0.263         0.022         0.368         0.934         0.098         0.002           2085760         749062         native 3         1.9-2.5         PCI/G         0.296         0.013         0.315         0.078         0.002           2085834         749062         native 3         1.8-2.3         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           208509         749066         native 3         1.8-2.3         PCI/G         0.34         0.026         0.037         0.162         0.002           2085684         748989         native 3         1.9-2.4         PCI/G         0.472         0.028         0.546         1.2         1.87         0.002           2085759         748989         native 3         1.9-2.4         PCI/G	90898			native 3	1.9-2.4	PCI/G	0.501	0.028	0.492	0.032	0.089	0.002	0.010
2085610         749062 native 3         2.4-2.9         PCI/G         1.15         0.059         1.32         14.4         2.86         0.027           2085685         749064 native 3         1.9-2.5         PCI/G         0.263         0.022         0.368         0.934         0.098         0.002           2085760         749062 native 3         1.9-2.5         PCI/G         0.495         0.022         0.524         0.067         0.278         0.003           2085834         749065 native 3         1.8-2.3         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           2085809         748906 native 3         1.8-2.3         PCI/G         0.472         0.028         0.546         0.245         0.002           2085610         748989 native 3         2.5-3.0         PCI/G         0.472         0.028         0.546         0.292         0.054         0.002           2085759         748989 native 3         2.0-2.4         PCI/G         0.45         0.023         0.516         0.52         0.526         0.057         0.292         0.054         0.094           2085769         748990 native 3         2.0-2.4         PCI/G         0.58         0.065	86606		749141	native 3	1.8-2.3	PCI/G	3.12	0.274	9.1	48.4	9.24	0.096	0.545
2085685         749064 native 3         1.9-2.5         PCI/G         0.263         0.022         0.368         0.934         0.098         0.002           2085760         749062 native 3         2.0-2.6         PCI/G         0.495         0.022         0.524         0.067         0.278         0.003           2085834         749065 native 3         1.8-2.3         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           2085909         749066 native 3         1.8-2.3         PCI/G         0.37         0.028         0.157         0.162         0.002           2085684         748987 native 3         2.5-3.0         PCI/G         0.472         0.028         0.546         12.2         1.87         0.002           2085789         748989 native 3         2.0-2.4         PCI/G         0.645         0.075         0.516         5.13         1.1         0.002           2085834         748990 native 3         2.1-2.6         PCI/G         0.554         0.076         0.577         29.9         2.94         0.036           2085609         748990 native 3         1.9-2.4         PCI/G         0.569         0.056         0.577         29.9         2.94	91098		749062	native 3	2.4-2.9	PCI/G	1.15	0.059	1.32	14.4	2.86	0.027	0.151
2085760         749062 native 3         2.0-2.6         PCI/G         0.495         0.022         0.524         0.067         0.278         0.003           2085834         749065 native 3         1.8-2.3         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           2085909         749066 native 3         1.8-2.3         PCI/G         0.34         0.007         0.367         0.327         0.162         0.002           2085610         748987 native 3         2.5-3.0         PCI/G         0.645         0.031         0.745         0.292         0.024         0.002           2085759         748989 native 3         2.0-2.4         PCI/G         0.38         0.023         0.516         5.13         1.1         0.010           2085834         748989 native 3         2.1-2.6         PCI/G         0.38         0.076         0.577         29.9         0.004         0.001           2085834         748980 native 3         2.1-2.6         PCI/G         0.58         0.076         0.577         29.9         2.94         0.036           2085809         748991 native 3         1.9-2.4         PCI/G         0.356         0.356         0.206         0.576	91198		749064		1.9-2.5	PCI/G	0.263	0.022	0.368	0.934	0.098	0.002	0.012
2085834         749065 native 3         1.8-2.3         PCI/G         0.296         0.013         0.315         0.131         0.245         0.002           2085909         749066 native 3         1.8-2.3         PCI/G         0.37         0.028         0.546         12.2         1.87         0.002           2085610         748986 native 3         2.5-3.0         PCI/G         0.645         0.031         0.745         0.292         0.024         0.019           2085684         748989 native 3         1.9-2.4         PCI/G         0.645         0.023         0.516         5.13         1.1         0.010           2085834         748989 native 3         2.0-2.4         PCI/G         0.554         0.076         0.577         29.9         2.94         0.016           2085909         748990 native 3         1.9-2.4         PCI/G         0.659         0.066         0.625         3.39         0.605         0.007           2085609         748913 native 3         1.9-2.4         PCI/G         0.352         0.358         0.206         0.112         0.007           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.01         0.01         0.01         0.003         <	91298		749062		2.0-2.6	PCI/G	0.495	0.022	0.524	0.067	0.278	0.003	0.015
2085909         749066 native 3         1.8-2.3         PCI/G         0.31         0.007         0.367         0.367         0.162         0.002           2085610         748987 native 3         1.8-2.3         PCI/G         0.472         0.028         0.546         12.2         1.87         0.019           2085684         748989 native 3         1.9-2.4         PCI/G         0.645         0.031         0.745         0.292         0.024         0.002           2085834         748990 native 3         2.1-2.6         PCI/G         0.554         0.076         0.577         29.9         2.94         0.036           2085909         748910 native 3         1.9-2.4         PCI/G         0.659         0.066         0.625         3.39         0.605         0.007           2085609         748913 native 3         1.9-2.4         PCI/G         0.352         0.358         0.358         0.206         0.112         0.007           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.017         0.015         0.023         0.019         0.003           2085760         748914 native 3         2.0-2.3         PCI/G         0.043         0.043         0.015         0.019	91398		749065		1.8-2.3	PCI/G	0.296	0.013	0.315	0.131	0.245	0.002	0.012
2085610         748987 native 3         2.5-3.0         PCI/G         0.472         0.028         0.546         12.2         1.87         0.019           2085684         748989 native 3         1.9-2.4         PCI/G         0.645         0.031         0.745         0.292         0.024         0.002           2085759         748989 native 3         2.0-2.4         PCI/G         0.58         0.026         0.516         5.13         1.1         0.010           2085834         748990 native 3         2.1-2.6         PCI/G         0.554         0.076         0.577         29.9         2.94         0.036           2085609         748913 native 3         1.9-2.4         PCI/G         0.659         0.066         0.625         3.39         0.605         0.007           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.017         0.015         0.016         0.015         0.003           2085760         748914 native 3         1.7-2.2         PCI/G         0.043         1.22         0.015         0.019         0.003	91498			native 3	1.8-2.3	PCI/G	0.31	0.007	0.367	0.327	0.162	0.002	0.010
2085684         748989 native 3         1.9-2.4         PCI/G         0.645         0.031         0.745         0.292         0.024         0.002           2085759         748989 native 3         2.0-2.4         PCI/G         0.38         0.023         0.516         5.13         1.1         0.010           2085834         748999 native 3         1.9-2.4         PCI/G         0.659         0.066         0.657         29.9         2.94         0.036           2085609         748990 native 3         1.9-2.4         PCI/G         0.659         0.066         0.625         3.39         0.605         0.007           2085609         748913 native 3         1.9-2.4         PCI/G         0.035         0.358         0.358         0.206         0.112         0.004           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.043         1.22         0.023         0.019         0.003	91598			native 3	2.5-3.0	PCI/G	0.472	0.028	0.546	12.2	1.87	0.019	0.106
2085759         748989 native 3         2.0-2.4         PCI/G         0.354         0.023         0.516         5.13         1.1         0.010           2085834         748990 native 3         2.1-2.6         PCI/G         0.554         0.076         0.577         29.9         2.94         0.036           2085909         748990 native 3         1.9-2.4         PCI/G         0.659         0.066         0.625         3.39         0.605         0.007           2085609         748913 native 3         1.9-2.4         PCI/G         0.352         0.358         0.358         0.206         0.112         0.004           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.017         0.15         0.023         0.001           2085760         748914 native 3         2.0-2.3         PCI/G         1.06         0.043         1.22         0.023         0.019         0.003	91698			native 3	1.9-2.4	PCI/G	0.645	0.031	0.745	0.292	0.024	0.002	0.012
2085834748990 native 32.1-2.6PCI/G0.5540.0760.57729.92.940.0362085909748990 native 31.9-2.4PCI/G0.6590.0660.6653.390.6050.0072085609748913 native 31.9-2.4PCI/G0.3520.3580.3580.2060.1120.0042085684748914 native 31.7-2.2PCI/G0.010.0170.150.0230.0012085760748914 native 32.0-2.3PCI/G1.060.0431.220.0230.0190.003	91798		748989	native 3	2.0-2.4	PCI/G	0.38	0.023	0.516	5.13	1:1	0.010	0.057
2085909         748990 native 3         1.9-2.4         PCI/G         0.659         0.066         0.625         3.39         0.605         0.007           2085609         748913 native 3         1.9-2.4         PCI/G         0.352         0.358         0.206         0.112         0.004           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.043         1.22         0.023         0.019         0.003	91898		748990	native 3	2.1-2.6	PCI/G	0.554	0.076	0.577	29.9	2.94	0.036	0.207
2085609         748913 native 3         1.9-2.4         PCI/G         0.352         0.358         0.206         0.112         0.004           2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.017         0.15         0.023         0.001           2085760         748914 native 3         2.0-2.3         PCI/G         1.06         0.043         1.22         0.023         0.019         0.003	91998		748990	native 3	1.9-2.4	PCI/G	0.659	0.066	0.625	3.39	0.605	0.007	0.040
2085684         748914 native 3         1.7-2.2         PCI/G         0.01         0.017         0.1         0.15         0.023         0.001           2085760         748914 native 3         2.0-2.3         PCI/G         1.06         0.043         1.22         0.023         0.019         0.003	92098			native 3	1.9-2.4	PCI/G	0.352	0.358	0.358	0.206	0.112	0.004	0.023
2085760 748914 native 3 2.0-2.3 PCI/G 1.06 0.043 1.22 0.023 0.019 0.003	92198			native 3	1.7-2.2	PCI/G	0.01	0.017	0.1	0.15	0.023	0.001	0.003
	92298		748914	native 3	2.0-2.3	PCI/G	1.06	0.043	1.22	0.023	0.019	0.003	0.018

						U-233/234	U-235	U-238	Pu 239/240	Am-241	RFCA Tier I	RFCA Tier II
Borehole	EASTING	NORTHING	Material	Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
92398		748915 native		2.3-2.8	PCI/G	0.489	0.033	0.396	0.433	90.0	0.002	0.010
92498	2085909	748915 native	native 3	2.1-2.6	PCI/G	0.27	0.05	0.29	0.059	0.124	0.002	0.009
92598	2085560	749064 native	native 3	1.0-1.5	PCI/G	0.806	0.038	0.888	0.936	0.197	0.004	0.022
92698	2085551	748977 native 3	native 3	0.9-1.4	PCI/G	0.946	0.041	0.786	0.071	0.168	0.003	0.017
92798	2085553	748827 native 3	native 3	0.9-1.4	PCI/G	0.354	0.013	0.458	0.09	90.0	0.001	0.008
92898	2085703	748830 native 3	native 3	1.5-2.0	PCI/G	0.769	0.039	0.77	0.137	0.053	0.002	0.014
92998	2085853	748830 native 3	native 3	1.0-1.5	PCI/G	0.766	0.023	0.896	1.75	0.216	0.004	0.025
93098	2086005	748817 native 3	native 3	1.0-1.5	PCI/G	1.02	0.099	0.76	11.8	2.22	0.021	0.120
93198	2086167	748839 native	native 3	1.0-1.5	PCI/G	0.934	0.055	0.974	28	4.15	0.042	0.235
93298	2085755	748671 native 3	native 3	1.0-1.5	PCI/G	0.706	0.018	0.776	0.322	-0.012	0.002	0.012
93398	2085857	748698 native	native 3	1.0-1.5	PCI/G	1.2	0.07	1.14	5.46	0.818	0.011	0.061
93498	2086198	748702 native 3	native 3	1.0-1.5	PCI/G	0.823	0.064	1.15	5.55	_	0.011	0.065
93298	2085978	748977 native 3	native 3	0.8-1.2	PCI/G	0.556	0.003	0.632	3.64	0.447	900'0	0.034
93698	2086153	748988 native	native 3	1.0-1.5	PCI/G	0.372	0.012	0.401	54.1	8.39	0.078	0.441
93798	2086300	748976 native	native 3	0.9-1.35	PCI/G	0.367	0.04	0.308	0.154	0.097	0.002	0.009
93898	2086406		native 3	1.0-1.5	PCI/G	0.761	0.049	0.776	17.4	3.21	0.029	0.166
93998	2086000	749123 native 3	native 3	1.0-1.5	PCI/G	0.544	0.042	0.655	0.058	0.047	0.002	0.011
94098	2086128	749117 native 3	native 3	0.8-1.2	PCI/G	0.671	0.036	0.769	19.2	2.96	0.029	0.165
94198		749123 native 3	native 3	0.8-1.2	PCI/G	0.316	0.017	0.341	0.346	0.059	0.001	0.008
94298	2086438	749112 native 3	native 3	1.0-1.5	PCI/G	969.0	0.05	0.738	0.278	0.164	0.003	0.017
94398		749129 native	native 3	0.7-1.1	PCI/G	0.677	0.042	0.713	0.257	0.048	0.002	0.013
94498			native 3	0.8-1.3	PCI/G	0.423	0.025	0.468	0.058	0.027	0.001	0.008
94598			native 3	1.0-1.5	PCI/G	0.636	0.025	0.567	1.04	0.165	0.003	0.017
94698		749265 native 3	native 3	0.9-1.35	PCI/G	0.568	0.04	0.617	2.1	0.415	0.005	0.029
94798	2086000	749266 native 3	native 3	1.0-1.5	PCI/G	0.588	0.037	0.512	0.521	0.245	0.003	0.017
94898	2086149	749243 native 3	native 3	0.8-1.2	PCI/G	1.48	0.124	3.12	247	54.4	0.433	2.452
94998		749244 native	native 3	1.0-1.5	PCI/G	0.843	0.017	1.22	26.6	4.56	0.043	0.241
92038	2086447		native 3	1.0-1.5	PCI/G	0.426	0.023	0.618	1.52	0.311	0.004	0.023
95198	2086149	749188 native	native 3	1.0-1.5	PCI/G	1.29	0.138	2.71	115	25.8	0.207	1.172
95298	2086066	749123 native 3	native 3	1.0-1.5	PCI/G	0.956	0.037	0.944	45.1	8.92	0.075	0.428
95398	2086211	749120 native 3	native 3	1.0-1.5	PCI/G	0.841	0.062	1.19	46.5	8.89	0.077	0.435
95498	2086078	748987 native 3	native 3	0.9-1.35	PCI/G	0.827	0.063	1.76	156	29.5	0.250	1.418
95298	2086229	748984 native 3	native 3	1.0-1.5	PCI/G	0.489	0.015	0.572	38.1	5.93	0.056	0.315
95698	2086077	749248 native 3	native 3	1.0-1.5	PCI/G	0.544	0.00	0.622	10.7	2.07	0.019	0.105
95798			native 3	1.0-1.5	PCI/G	0.562	-0.013	1.02	1.34	0.273	0.004	0.024
95898	2086219	749244 native 3	native 3	1.0-1.5	PCI/G	0.805	0.003	0.751	11.4	2.49	0.021	0.121

	_	
Material Interval(ft) unit_code pCi/g	Material Interval(ft) unit_code	Interval(ft) unit_code
3 1.0-1.5	3 1.0-1.5	1.0-1.5
	3 0.9-1.35	0.9-1.35
1.0-1.5	1.0-1.5	1.0-1.5
,,,,,,	2.5-3.0	2.5-3.0
	2.4-2.9	
2.4-3.0	2.4-3.0	
	2:3-2.8	4 2:3-2.8
4	4 2.2-2.7	4 2.2-2.7
4 2.6-3.1	4 2.6-3.1	2.6-3.1
4	4 2.5-3.1	2.5-3.1
ative 4 2.4-2.9 PCI/G	4 2.4-2.9	2.4-2.9
4	4 2.3-2.8	4 2.3-2.8
4 2.9-3.4	4 2.9-3.4	4 2.9-3.4
4	4 2.5-3.1	4 2.5-3.1
tive 4 2.3-2.8 PCI/G	4 2.3-2.8	4 2.3-2.8
4 2.3-2.8	4 2.3-2.8	4 2.3-2.8
4	4 3.0-3.5	3.0-3.5
	2.4-2.9	2.4-2.9
2.6-3.1	2.6-3.1	2.6-3.1
2.4-2.9	2.4-2.9	
4 2.4-2.9	4 2.4-2.9	4 2.4-2.9
4 2.2-2.7	4 2.2-2.7	4 2.2-2.7
4 2.8-3.3	4 2.8-3.3	4 2.8-3.3
2.6-3.1	2.6-3.1	2.6-3.1
1.5-2.0	1.5-2.0	4 1.5-2.0
4 1.4-1.9	4 1.4-1.9	4 1.4-1.9
4 1.4-1.9	4 1.4-1.9	4 1.4-1.9
4 2.0-2.4	4 2.0-2.4	4 2.0-2.4
ative 4 1.5-2.0 PCI/G	4 1.5-2.0	1.5-2.0
ative 4 1.5-2.0 PCI/G	1.5-2.0	
ative 4 1.5-2.0 PCI/G	1.5-2.0	
	1.5-2.0	
4	4 1.5-2.0	4 1.5-2.0
ative 4 1.5-2.0 PCI/G	4 1.5-2.0	4 1.5-2.0
1.2-1.4	1.2-1.4	1.2-1.4
748988 native 4 1.5-2.0 PCI/G	15,00	

									Pu			
					,	U-233/234	U-235	U-238	239/240	Am-241	RFCA Tier I	RFCA Tier II
Borehole		EASTING NORTHING Material	Material	Interval(ft)	nnit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g	(Sum of Ratio)	(Sum of Ratio)
93798	2086300	748976 native	native 4	1.35-1.8	PCI/G	0.371	0.025	0.311	1.03	0.307	0.003	0.017
93898	2086406	749003 native 4	native 4	1.5-2.0	PCI/G	0.385	0.033	0.576	14.3	2.07	0.021	0.119
93998	2086000	749123 native 4	native 4	1.5-2.0	PCI/G	0.637	0.014	0.548	0.037	0.358	0.003	0.018
94098	2086128	749117 native	native 4	1.2-1.5	PCI/G	0.522	-0.047	1.11	<b>5</b> 2	5.25	0.064	0.363
94198	2086298	749123 native 4	native 4	1.2-1.6	PCI/G	0.464	0.017	0.36	2.86	0.293	0.004	0.025
94298	2086438	749112 native	native 4	1.5-2.0	PCI/G	0.686	0.034	0.773	0.471	0.026	0.002	0.014
94398	2085550	749129 native 4	native 4	1.1-1.4	PCI/G	0.668	0.032	0.702	0.267	0.024	· 0.002	0.012
94498	2085552	749264 native 4	native 4	1.3-1.8	PCI/G	0.37	0.047	0.449	0.014	0.019	0.001	0.008
94598	2085703	749265 native	native 4	1.5-2.0	PCI/G	0.802	0.043	0.813	0.081	0.032	0.002	0.013
94698	2085852	749265 native 4	native 4	1.35-1.8	PCI/G	0.651	0.055	0.878	5.62	1.16	0.012	0.066
94798	2086000	749266 native 4	native 4	1.5-2.0	PCI/G	0.483	0.016	0.611	0.121	0.051	0.002	0.010
94898	2086149	749243 native	native 4	1.2-1.7	PCI/G	0.946	0.079	1.97	34.5	7.63	0.064	0.363
94998	2086298	749244 native 4	native 4	1.5-2.0	PCI/G	0.491	0.048	0.685	6.95	1.33	0.013	0.073
95098	2086447	749243 native 4	native 4	1.5-2.0	PCI/G	0.652	0.062	0.664	0.57	0.152	0.003	0.017
95198	2086149	749188 native 4	native 4	1.5-2.0	PCI/G	0.523	0.031	0.716	5.32	0.969	0.010	0.057
95298	2086066	749123 native	native 4	1.5-2.0	PCI/G	0.562	0.023	0.595	1.31	0.238	0.004	0.020
95398	2086211	749120 native 4	native 4	1.5-2.0	PCI/G	0.713	0.032	0.813	34.5	99.9	0.057	0.324
95498	2086078	748987 native 4	native 4	1.35-1.75	PCI/G	0.52	0.034	0.593	12.3	2.26	0.021	0.117
95298	2086229	748984 native	native 4	1.5-2.0	PCI/G	0.359	-0.011	0.265	1.37	0.272	0.003	0.016
95698	2086077	749248 native 4	native 4	1.5-2.0	PCI/G	0.477	0.017	0.505	4.49	1.06	00:00	0.053
95798	2086148	749268 native 4	native 4	1.5-2.0	PCI/G	0.654	0.017	0.792	0.816	0.13	0.003	0.017
95838	2086219	749244 native 4	native 4	1.5-2.0	PCI/G	0.538	0.041	0.552	20.1	4.46	0.036	0.206
97398	2086096	748827 native 4	native 4	1.5-2.0	PCI/G	0.76	0.044	0.917	0.549	0.169	0.003	0.020
97498	2086182	748770 native 4	native 4	1.35-1.8	PCI/G	0.617	0.04	0.559	0	0.032	0.002	0.010
97598	2086247	748845 native 4	native 4	1.5-2.0	PCI/G	0.978	0.077	0.89	0.913	0.194	0.004	0.024

		·	95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 001	2086660.36	749529.79	0.16	0.93	0.04	0.24
STAKE 002	2086695.36	749530.93	0.18	1.02	0.06	0.34
STAKE 003	2086678.06	749501.13	0.16	0.93	0.04	0.24
STAKE 004	2086712.63	749504.23	0.19	1.08	0.07	0.42
STAKE 005	2086731.69	749533.84	0.17	0.98	0.05	0.30
STAKE 006	2086748.75	749506.28	0.20	1.14	0.09	0.49
STAKE 007	2086762.45	749535.74	0.19	1.08	0.07	0.42
STAKE 008	2086781.30	749506.72	0.21	1.19	0.10	0.54
STAKE 009	2086799.56	749538.23	0.20	1.14	0.09	0.49
STAKE 010	2086818.67	749508.67	0.21	1.21	0.10	0.56
STAKE 011	2086833.03	749539.60	0.19	1.05	0.07	0.38
STAKE 012	2086852.47	749510.94	0.21	1.17	0.09	0.52
STAKE 013	2086870.74	749541.20	0.20	1.12	0.08	0.46
STAKE 014	2086887.32	749514.29	0.22	1.24	0.11	0.60
STAKE 015	2086902.84		0.21	1.17	0.09	0.53
STAKE 016	2086920.38	749517.65	0.21	1.21	0.10	0.57
STAKE 017	2086937.28	749548.87	0.18	1.04	0.06	0.37
STAKE 018	2086956.59	749519.03	0.20	1.16	0.09	0.51
STAKE 019	2086975.17	749548.25	0.19	1.07	0.07	0.40
STAKE 020	2086991.16	749523.05	0.20	1.12	0.08	0.46
STAKE 021	2087006.84	749551.73	0.19	1.09	0.08	0.43
STAKE 022	2087025.48	749523.74	0.20	1.16	0.09	0.50
STAKE 023	2087040.76	749553.56	0.20	1.13	0.08	0.47
STAKE 024	2087060.79	749527.84	0.21	1.22	0.10	0.58
STAKE 025	2087074.45	749557.95	0.19	1.07	0.07	0.41
STAKE 026	2087094.45	749529.46	0.19	1.09	0.08	0.43
STAKE 027	2087112.06	749557.07	0.18	1.02	0.06	0.35
STAKE 028	2087128.65	749532.50	0.17	0.98	0.05	0.29
STAKE 029	2087145.52	749562.17	0.19	1.08	0.07	0.41
STAKE 030	2087180.07	749564.78	0.17	0.95	0.05	0.26
STAKE 031	2087045.63	749494.74	0.17	0.95	0.05	0.26
STAKE 032	2087011.42	749491.93	0.23	1.30	0.12	0.67
STAKE 033	2086976.64	749489.91	0.24	1.38	0.14	0.77
STAKE 034	2086940.34	749488.57	0.24	1.34	0.13	0.72
STAKE 035	2086907.58	749485.31	0.24	1.33	0.13	0.71
STAKE 036	2086873.63	749483.37	0.25	1.40	0.14	0.79
STAKE 037	2086838.28	749480.70	0.22	1.26	0.11	0.63
STAKE 038	2086802.35	749478.14	0.23	1.29	0.12	0.66
STAKE 039	2086768.76	749475.99	0.21	1.19	0.10	0.54
STAKE 040	2086733.01	749474.44	0.17	0.97	0.05	0.28
STAKE 041	2086699.40	749471.91	0.17	0.94	0.04	0.25
STAKE 043	2086685.15	749441.65	0.24	1.34	0.13	0.72
STAKE 044	2086719.39	749444.02	0.23	1.32	0.12	0.69
STAKE 045	2086752.83	749445.04	0.24	1.36	0.13	0.74
STAKE 046	2086789.28	749447.22	0.28	1.58	0.17	0.99
STAKE 047	2086822.32	749449.26	0.24	1.35	0.13	0.73
STAKE 048	2086858.28	749451.80	0.33	1.87	0.23	1.31

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 049	2086892.23		0.34	1.93	0.24	1.38
STAKE 050	2086923.40		0.26	1.47	0.15	0.87
STAKE 051	2086958.26		0.21	1.17	0.09	0.52
STAKE 052	2086874.82		0.17	0.94	0.04	0.25
STAKE 053	2086839.57		0.17	0.95	0.05	0.26
STAKE 054	2086803.25		0.20	1.11	0.08	0.45
STAKE 055	2086684.68		0.17	0.94	0.04	0.25
STAKE 056	2086716.93		0.17	0.99	0.05	0.31
STAKE 057	2086752.10		0.17	0.95	0.05	0.26
STAKE 058	2086786.96		0.18	1.01	0.06	0.33
STAKE 059	2086821.82		0.19	1.06	0.07	0.39
STAKE 060	2086856.06		0.21	1.19	0.10	0.55
STAKE 061	2086887.41		0.24	1.35	0.13	0.73
STAKE 062	2086919.87		0.22	1.23	0.10	0.58
STAKE 063	2086948.78		0.19	1.10	0.08	0.44
STAKE 064	2086981.45		0.23	1.33	0.12	0.70
STAKE 065	2087013.46		0.22	1.25	0.11	0.61
STAKE 066	2087044.99		0.22	1.23	0.10	0.59
STAKE 067	2086650.05		0.17	0.94	0.04	0.24
STAKE 068	2086616.24		0.17	0.98	0.05	0.29
STAKE 069	2086580.76		0.17	0.95	0.05	0.26
STAKE 070	2086547.39		0.17	0.94	0.04	0.25
STAKE 071	2086434.71	748842.45	0.17	0.96	0.05	0.27
STAKE 072	2086465.63		0.16	0.93	0.04	0.24
STAKE 073	2086499.39		0.17	0.96	0.05	0.27
STAKE 074	2086533.69		0.17	0.99	0.05	0.30
STAKE 075	2086567.57		0.17	0.96	0.05	0.27
STAKE 076	2086602.13		0.19	1.07	0.07	0.40
STAKE 077	2086444.59		0.24	1.35	0.13	0.73
STAKE 078	2086475.62		0.37	2.11	0.28	1.57
STAKE 079	2086511.98		0.39	2.20	0.29	1.66
STAKE 080	2086547.46		0.35	1.96	0.25	1.41
STAKE 081	2086581.44		0.45	2.56	0.36	2.04
STAKE 082	2086615.42		0.42	2.38	0.33	1.85
STAKE 083	2086636.75		0.23	1.31	0.12	0.68
STAKE 084	2086650.32	748778.60	0.32	1.81	0.22	1.24
STAKE 085	2086671.08	748803.76	0.22	1.25	0.11	0.61
STAKE 086	2086682.40	748772.89	0.32	1.83	0.22	1.26
STAKE 087	2086706.10	748797.99	0.25	1.39	0.14	0.77
STAKE 088	2086718.18		0.32	1.83	0.22	1.27
STAKE 089	2086742.98	748793.02	0.21	1.20	0.10	0.55
STAKE 090	2086755.46		0.30	1.72	0.20	1.15
STAKE 091	2086775.50		0.20	1.13	0.08	0.46
STAKE 092	2086788.19		0.28	1.60	0.18	1.01
STAKE 093	2086812.24		0.17	0.99	0.05	0.30
STAKE 094	2086821.86		0.30	1.70	0.20	1.12
STAKE 095	2086843.65		0.17	0.99	0.05	0.30

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 096	2086857.89		0.26	1.47	0.15	0.86
STAKE 097	2086891.87		0.22	1.25	0.11	0.61
STAKE 098	2086452.32		0.51	2.91	0.42	2.40
STAKE 099	2086430.55		0.50	2.85	0.41	2.34
STAKE 100	2086467.37	748745.06	0.36	2.07	0.27	1.52
STAKE 1000	2085697.36		0.16	0.93	0.04	0.23
STAKE 1001	2085713.42		0.18	1.00	0.06	0.31
STAKE 1002	2085666.30		0.17	0.95	0.05	0.26
STAKE 1003	2085682.74		0.17	0.95	0.05	0.26
STAKE 1004	2085630.39		0.17	0.95	0.05	0.26
STAKE 1005	2085646.16		0.17	0.93	0.04	0.24
STAKE 1006	2085596.99		0.17	0.95	0.05	0.26
STAKE 1007	2085614.36		0.17	0.94	0.04	0.25
STAKE 1008	2086111.37	748894.07	0.51	2.91	0.42	2.40
STAKE 1009	2086142.52		0.26	1.49	0.16	0.89
STAKE 101	2086487.41	748769.45	0.35	1.99	0.25	1.44
STAKE 1010	2086124.81		0.23	1.33	0.12	0.70
STAKE 1011	2086157.18		0.24	1.34	0.13	0.72
STAKE 1012	2085795.06	748647.80	0.19	1.10	0.08	0.43
STAKE 1013	2085761.62	748642.77	0.17	0.97	0.05	0.29
STAKE 1014	2085723.41	748644.14	0.17	0.96	0.05	0.28
STAKE 1015	2085708.41	748673.78	0.19	1.06	0.07	0.39
STAKE 1016	2085739.45		0.13	1.16	0.09	0.51
STAKE 1017		748672.11	0.16	0.93	0.04	0.24
STAKE 1018	2085792.01	748696.51	0.25	1.42	0.14	0.81
STAKE 1019	2085826.30	748700.00	0.40	2.29	0.31	1.76
STAKE 102	2086501.74	748741.81	0.40	2.27	0.31	1.74
STAKE 1020	2085858.72		0.20	1.11	0.08	0.45
STAKE 1021	2085881.61		0.28	1.58	0.17	0.99
STAKE 1022	2085893.14		0.19	1.07	0.07	0.40
STAKE 1023	2085811.84		0.22	1.25	0.10	0.59
STAKE 1024	2085778.11		0.18	1.02	0.06	0.34
STAKE 1025	2086290.76		0.26	1.44	0.15	0.84
STAKE 1026	2087595.12		0.17	0.95	0.05	0.26
STAKE 1027	2087575.61		0.17	0.94	0.04	0.24
STAKE 1028	2087554.62		0.17	0.95	0.05	0.26
STAKE 1029	2087501.95		0.24	1.34	0.13	0.72
STAKE 103	2086525.16		0.45	2.52	0.35	2.01
STAKE 1030	2087545.46		0.17	0.94	0.04	0.25
STAKE 1031	2087508.70		0.22	1.26	0.11	0.62
STAKE 1032	2087410.40		0.23	1.32	0.12	0.70
STAKE 1033	2087399.69		0.24	1.36	0.13	0.74
STAKE 1034	2087380.84		0.20	1.14	0.09	0.48
STAKE 1035	2087370.15		0.21	1.21	0.10	0.56
STAKE 1036	2087437.88		0.23	1.29	0.12	0.66
STAKE 1037	2087145.40		0.17	0.97	0.12	0.28
STAKE 1038	2087122.73		0.23	1.29	0.12	0.20

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 1039	2087139.33		0.18	1.01	0.06	0.34
STAKE 104	2086540.73	748734.16	0.30	1.72	0.20	1.15
STAKE 1040	2087113.25	748909.62	0.18	1.04	0.07	0.37
STAKE 1041	2087064.10	748811.65	0.18	0.99	0.05	0.31
STAKE 1042	2087066.33	748782.26	0.17	0.99	0.05	0.30
STAKE 1043	2087043.78	748794.50	0.17	0.98	0.05	0.29
STAKE 1044	2087012.33	748790.49	0.17	0.97	0.05	0.28
STAKE 1045	2087034.88	748761.91	0.17	0.94	0.04	0.25
STAKE 1046	2087009.01	748757.54	0.17	0.96	0.05	0.27
STAKE 1047	2086985.72	748775.12	0.17	0.96	0.05	0.27
STAKE 1048	2086983.38	748748.37	0.17	0.97	0.05	0.28
STAKE 1049	2086958.42	748764.99	0.17	0.96	0.05	0.27
STAKE 105	2086561.54	748756.44	0.38	2.18	0.29	1.64
STAKE 1050	2086936.95	748759.90	0.17	0.96	0.05	0.27
STAKE 1051	2086967.48	748789.43	0.18	1.04	0.07	0.37
STAKE 1052	2086944.97	748784.83	0.25	1.39	0.14	0.77
STAKE 1053	2086985.62	748804.36	0.17	0.94	0.04	0.25
STAKE 1054	2087013.27	748807.72	0.17	0.98	0.05	0.30
STAKE 1055	2087419.52	749317.34	0.23	1.28	0.11	0.65
STAKE 1056	2087478.98	749229.91	0.26	1.50	0.16	0.90
STAKE 1057	2087512.58	749232.28	0.23	1.31	0.12	0.68
STAKE 1058	2087463.14	749198.06	0.17	0.97	0.05	0.28
STAKE 1059	2087497.51	749199.80	0.17	0.95	0.05	0.26
STAKE 106	2086577.33	748729.36	0.34	1.94	0.24	1.38
STAKE 1060	2087545.02	749234.62	0.24	1.38	0.13	0.76
STAKE 1061	2087534.13	749204.52	0.29	1.66	0.19	1.08
STAKE 1062	2087518.74	749171.72	0.18	0.99	0.05	0.31
STAKE 1063	2087566.74	749205.12	0.27	1.54	0.17	0.95
STAKE 1064	2087554.35	749177.38	0.27	1.53	0.17	0.94
STAKE 1065	2087585.29	749178.11	0.20	1.13	0.08	0.47
STAKE 1066	2087601.08	749207.17	0.17	0.96	0.05	0.27
STAKE 1067	2087634.88	749209.87	0.17	0.96	0.05	0.27
STAKE 1068	2087579.57	749236.50	0.19	1.09	0.08	0.43
STAKE 1069	2087619.57	749181.17	0.17	0.94	0.04	0.25
STAKE 107	2086596.90	748755.86	0.32	1.83	0.22	1.27
STAKE 1070	2087590.85	749270.42	0.17	0.96	0.05	0.27
STAKE 1071	2087612.18	749240.67	0.17	0.97	0.05	0.28
STAKE 1072	2087603.61	749154.03	0.17	0.94	0.04	0.25
STAKE 1073	2087558.80	749266.95	0.23	1.29	0.12	0.66
STAKE 1074	2087573.60	749152.54	0.17	0.95	0.05	0.27
STAKE 1075	2087524.83		0.22	1.27	0.11	0.63
STAKE 1076	2087504.75	749291.60	0.25	1.40	0.14	0.79
STAKE 1077	2087539.89		0.17	0.95	0.05	0.27
STAKE 1078	2087506.15	749141.11	0.17	0.96	0.05	0.27
STAKE 1079	2087592.18	749126.36	0.17	0.94	0.04	0.25
STAKE 108	2086609.40	748724.35	0.33	1.84	0.23	1.28
STAKE 1080	2086738.52	749415.43	0.18	1.03	0.06	0.35

	T		95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 1081	2086770.51	749416.66	0.17	0.95	0.04	0.25
STAKE 1082	2086755.47	749388.07	0.17	0.94	0.04	0.25
STAKE 1083	2086784.55	749386.97	0.17	0.96	0.05	0.27
STAKE 1084	2086823.55	749395.37	0.17	0.94	0.04	0.24
STAKE 1085	2086855.28	749399.38	0.17	0.96	0.05	0.27
STAKE 1086	2086911.26	749426.41	0.16	0.93	0.04	0.24
STAKE 1087	2086941.10	749429.38	0.17	0.96	0.05	0.27
STAKE 1088	2086977.99	749442.76	0.16	0.93	0.04	0.24
STAKE 1089	2086993.98	749463.40	0.17	0.99	0.05	0.31
STAKE 109	2086630.58	748750.48	0.29	1.65	0.19	1.06
STAKE 1090	2087044.51	749394.52	0.22	1.25	0.11	0.61
STAKE 1091	2087074.85	749413.45	0.26	1.48	0.15	0.88
STAKE 1092	2087105.01	749427.89	0.19	1.05	0.07	0.38
STAKE 1093	2087135.90	749446.25	0.20	1.12	0.08	0.47
STAKE 1094	2087166.38	749463.61	0.18	1.01	0.06	0.33
STAKE 1095	2087193.79	749482.13	0.17	0.94	0.04	0.25
STAKE 1096	2087225.89	749500.92	0.18	1.00	0.06	0.32
STAKE 1097	2087255.01	749520.72	0.17	0.96	0.05	0.27
STAKE 1098	2087562.21	749114.89	0.16	0.93	0.04	0.23
STAKE 1099	2086602.30	749205.91	0.36	2.02	0.26	1.47
STAKE 110	2086642.37	748719.75	0.31	1.75	0.21	1.18
STAKE 1100	2086591.90	749178.98	0.28	1.57	0.17	0.98
STAKE 1101	2086569.87	749203.17	0.17	0.96	0.05	0.27
STAKE 1102	2086560.45	749176.37	0.17	0.94	0.04	0.25
STAKE 1103	2086577.43	749146.63	0.27	1.55	0.17	0.96
STAKE 1104	2086551.62	749145.33	0.19	1.09	0.08	0.43
STAKE 1105	2086521.59	749021.23	0.56	3.19	0.47	2.68
STAKE 1106	2086516.42	749271.95	0.16	0.93	0.04	0.23
STAKE 1107	2086516.09	749240.76	0.17	0.94	0.04	0.25
STAKE 1108	2086515.92	749205.28	0.16	0.93	0.04	0.24
STAKE 1109	2086512.60	749174.27	0.35	1.98	0.25	1.43
STAKE 111	2086664.44	748744.49	0.28	1.61	0.18	1.02
STAKE 1110	2086511.44	749138.34	0.35	1.97	0.25	1.42
STAKE 1111	2086508.84	749107.28	0.40	2.27	0.31	1.74
STAKE 112	2086677.81	748714.94	0.31	1.75	0.21	1.18
STAKE 113	2086697.38	748740.33	0.30	1.70	0.20	1.12
STAKE 114	2086708.47	748710.68	0.28	1.56	0.17	0.96
STAKE 115	2086731.98	748735.66	0.29	1.66	0.19	1.08
STAKE 116	2086744.07	748704.69	0.29	1.65	0.19	1.07
STAKE 117	2086763.71	748729.33	0.26	1.50	0.16	0.90
STAKE 118	2086777.42		0.27	1.54	0.17	0.95
STAKE 119	2086795.34	748724.26	0.27	1.50	0.16	0.90
STAKE 120	2086814.91	748696.05	0.26	1.46	0.15	0.86
STAKE 121	2086856.24		0.29	1.63	0.19	1.05
STAKE 122	2086836.31	748630.65	0.26	1.50	0.16	0.89
STAKE 123	2086824.56	748663.22	0.25	1.44	0.15	0.83
STAKE 124	2086804.70	748637.80	0.27	1.51	0.16	0.90

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 125	2086792.43		0.27	1.54	0.17	0.95
STAKE 126	2086769.71		0.26	1.47	0.15	0.86
STAKE 127	2086756.52	748672.93	0.27	1.54	0.17	0.95
STAKE 128	2086733.39	748648.35	0.29	1.67	0.19	1.09
STAKE 129	2086724.01	748670.71	0.28	1.59	0.18	1.00
STAKE 130	2086704.21	748651.68	0.30	1.69	0.20	1.11
STAKE 131	2086693.21	748680.85	0.26	1.46	0.15	0.86
STAKE 132	2086663.84	748663.05	0.22	1.25	0.11	0.61
STAKE 133	2086654.82	748689.43	0.32	1.79	0.22	1.23
STAKE 134	2086634.72	748659.43	0.35	1.96	0.25	1.40
STAKE 135	2086621.87	748692.32	0.34	1.91	0.24	1.35
STAKE 136	2086601.48	748663.84	0.24	1.37	0.13	0.75
STAKE 137	2086586.72	748694.81	0.33	1.87	0.23	1.31
STAKE 138	2086567.49	748671.19	0.25	1.41	0.14	0.80
STAKE 139	2086554.53	748700.16	0.35	2.00	0.26	1.45
STAKE 140	2086534.72	748675.28	0.31	1.78	0.21	1.21
STAKE 141	2086519.26	748704.71	0.36	2.05	0.27	1.51
STAKE 142	2086491.54	748681.27	0.32	1.82	0.22	1.26
STAKE 143	2086475.73		0.45	2.53	0.36	2.02
STAKE 144	2086456.25	748686.66	0.28	1.60	0.18	1.01
STAKE 145	2086443.58	748717.76	0.46	2.60	0.37	2.09
STAKE 146	2086423.15		0.37	2.09	0.27	1.55
STAKE 147	2086410.48	748721.88	0.47	2.65	0.38	2.14
STAKE 148	2086390.78	748696.45	0.39	2.21	0.30	1.67
STAKE 149	2086380.12	748639.92	0.34	1.94	0.24	1.39
STAKE 150	2086400.89	748664.61	0.41	2.31	0.32	1.78
STAKE 1500	2086364.84		0.41	2.35	0.32	1.82
STAKE 151	2086412.82	748635.10	0.45	2.55	0.36	2.03
STAKE 152	2086432.75	748657.62	0.36	2.04	0.26	1.49
STAKE 153	2086445.69	748627.70	0.43	2.42	0.33	1.89
STAKE 154	2086464.72	748652.36	0.29	1.67	0.19	1.09
STAKE 155	2086478.07	748623.14	0.34	1.94	0.24	1.39
STAKE 156	2086499.60	748646.91	0.31	1.78	0.21	1.21
STAKE 157	2086517.62	748617.20	0.30	1.70	0.20	1.12
STAKE 158	2086541.86	748641.85	0.27	1.52	0.16	0.92
STAKE 159	2086553.01	748612.42	0.31	1.78	0.21	1.21
STAKE 160	2086578.20	748634.30	0.26	1.49	0.16	0.89
STAKE 161	2086595.25	748606.49	0.25	1.41	0.14	0.80
STAKE 162	2086613.32	748633.70	0.36	2.03	0.26	1.48
STAKE 163	2086627.58	748601.76	0.22	1.24	0.11	0.60
STAKE 164	2086645.19	748626.16	0.24	1.38	0.13	0.76
STAKE 165	2086658.71	748597.83	0.22	1.26	0.11	0.62
STAKE 166	2086679.99	748625.22	0.27	1.56	0.17	0.96
STAKE 167	2086690.25	748595.17	0.28	1.58	0.17	0.99
STAKE 168	2086712.71	748621.30	0.26	1.45	0.15	0.84
STAKE 169	2086724.99	748587.90	0.25	1.40	0.14	0.79
STAKE 170	2086745.60	748613.41	0.26	1.46	0.15	0.85

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 171	2086350.85	748643.12	0.38	2.15	0.28	1.61
STAKE 172	2086356.14	748611.69	0.47	2.64	0.38	2.13
STAKE 173	2086390.94	748606.28	0.39	2.23	0.30	1.70
STAKE 174	2086367.98	748580.79	0.36	2.06	0.27	1.51
STAKE 175	2086421.24	748599.38	0.32	1.81	0.22	1.25
STAKE 176	2086400.82	748574.15	0.33	1.87	0.23	1.31
STAKE 177	2086455.63	748595.63	0.26	1.47	0.15	0.86
STAKE 178	2086437.16	748569.19	0.36	2.01	0.26	1.47
STAKE 179	2086493.66	748591.13	0.27	1.53	0.16	0.93
STAKE 180	2086469.78	748566.54	0.31	1.78	0.21	1.21
STAKE 181	2086531.10	748585.80	0.29	1.67	0.19	1.09
STAKE 182	2086508.41	748560.72	0.31	1.76	0.21	1.18
STAKE 183	2086569.35	748579.76	0.26	1.46	0.15	0.85
STAKE 184	2086546.33	748555.32	0.30	1.69	0.20	1.11
STAKE 185	2086603.84	748573.74	0.27	1.53	0.16	0.93
STAKE 186	2086582.46	748549.05	0.30	1.72	0.20	1.15
STAKE 187	2086637.59	748569.79	0.27	1.53	0.16	0.93
STAKE 188	2086617.93	748543.50	0.29	1.64	0.19	1.06
STAKE 189	2086667.82	748563.32	0.26	1.46	0.15	0.85
STAKE 190	2086648.93	748538.99	0.29	1.67	0.19	1.09
STAKE 191	2086709.45	748560.24	0.23	1.28	0.12	0.65
STAKE 192	2086687.56	748530.22	0.31	1.73	0.20	1.16
STAKE 193	2086740.61	748555.52	0.26	1.50	0.16	0.90
STAKE 194	2086720.40	748524.01	0.24	1.36	0.13	0.74
STAKE 195	2086801.36	748492.80	0.26	1.47	0.15	0.86
STAKE 196	2086754.60	748525.70	0.26	1.49	0.16	0.89
STAKE 197	2086781.66	748464.81	0.22	1.27	0.11	0.63
STAKE 198	2086786.01	748520.88	0.25	1.41	0.14	0.80
STAKE 199	2086766.64	748495.40	0.22	1.26	0.11	0.62
STAKE 200	2086748.92	748471.76	0.23	1.32	0.12	0.69
STAKE 201	2086734.51	748501.66	0.26	1.45	0.15	0.84
STAKE 202	2086711.99	748473.46	0.24	1.37	0.13	0.76
STAKE 203	2086698.80	748503.18	0.24	1.39	0.14	0.77
STAKE 204	2086676.08	748478.46	0.23	1.28	0.11	0.65
STAKE 205	2086660.95	748509.58	0.24	1.35	0.13	0.73
STAKE 206	2086642.53	748484.44	0.23	1.29	0.12	0.66
STAKE 207	2086631.19	748515.07	0.27	1.53	0.16	0.93
STAKE 208	2086606.07	748490.01	0.23	1.30	0.12	0.67
STAKE 209	2086594.29	748523.82	0.27	1.52	0.16	0.92
STAKE 210	2086571.30	748498.04	0.25	1.42	0.14	0.80
STAKE 211	2086558.34	748524.58	0.30	1.70	0.20	1.12
STAKE 212	2086538.60	748497.69	0.26	1.45	0.15	0.85
STAKE 213	2086523.59	748529.09	0.27	1.54	0.17	0.94
STAKE 214	2086499.53	748505.28	0.27	1.52	0.16	0.92
STAKE 215	2086488.24	748536.68	0.26	1.50	0.16	0.90
STAKE 216	2086464.48		0.27	1.51	0.16	0.91
STAKE 217	2086451.21		0.32	1.81	0.22	1.24

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 218	2086430.95		0.25	1.42	0.14	0.81
STAKE 219	2086417.75		0.33	1.87	0.14	1.31
STAKE 220	2086396.77	748522.21	0.29	1.62	0.23	1.03
STAKE 221	2086381.98		0.29	1.65	0.18	1.03
STAKE 222	2086363.55		0.29	1.98	0.19	1.07
STAKE 223	2086348.43		0.33	1.95	0.25	1.43
STAKE 224	2086327.97		0.34	1.72	0.25	
STAKE 224	2086341.61	748330.80	0.30	1.72	0.20	1.14
STAKE 225 STAKE 226	2086341.61		0.32	1.40	0.14	0.78
STAKE 220 STAKE 227	2086371.44		0.32	1.48	0.22	1.23
STAKE 227 STAKE 228	2086352.06		0.26			0.88
STAKE 228 STAKE 229				1.76	0.21	1.18
	2086407.40		0.24	1.39	0.14	0.77
STAKE 230 STAKE 231	2086389.04 2086440.16		0.29 0.23	1.62 1.33	0.18 0.12	1.03
STAKE 231						0.70
	2086420.64		0.31	1.73	0.20	1.15
STAKE 233	2086475.81		0.25	1.39	0.14	0.78
STAKE 234	2086455.12		0.31	1.75	0.21	1.17
STAKE 235	2086510.54		0.22	1.25	0.11	0.62
STAKE 236	2086490.24		0.27	1.52	0.16	0.91
STAKE 237	2086547.64	748465.17	0.23	1.30	0.12	0.67
STAKE 238	2086525.82		0.23	1.29	0.12	0.66
STAKE 239	2086583.99		0.25	1.40	0.14	0.79
STAKE 240		748434.87	0.21	1.21	0.10	0.57
STAKE 241	2086325.85		0.25	1.44	0.15	0.83
STAKE 242	2086305.90		0.23	1.29	0.12	0.66
STAKE 243	2086362.36		0.23	1.30	0.12	0.67
STAKE 244	2086339.62		0.21	1.21	0.10	0.57
STAKE 245	2086395.59		0.23	1.32	0.12	0.70
STAKE 246	2086372.84		0.24	1.38	0.14	0.77
STAKE 247	2086321.04		0.17	0.96	0.05	0.27
STAKE 248	2086289.16		0.40	2.26	0.31	1.73
STAKE 249	2086328.12		0.35	2.00	0.26	1.45
STAKE 250	2086298.73		0.18	0.99	0.05	0.31
STAKE 251	2086310.07		0.18	1.05	0.07	0.38
STAKE 252	2086278.63		0.32	1.81	0.22	1.24
STAKE 253	2086266.92		0.35	1.97	0.25	1.42
STAKE 254	2086244.80		0.37	2.07	0.27	1.53
STAKE 255	2086286.39		0.17	0.96	0.05	0.27
STAKE 256	2086255.54		0.32	1.84	0.22	1.27
STAKE 257	2086296.31		0.18	1.03	0.06	0.35
STAKE 258	2086262.86		0.22	1.26	0.11	0.62
STAKE 260	2086616.82		0.18	1.02	0.06	0.34
STAKE 261	2086636.56		0.18	1.00	0.06	0.31
STAKE 262	2086650.05	749240.27	0.23	1.32	0.12	0.69
STAKE 263	2086671.01	749214.02	0.50	2.82	0.41	2.31
STAKE 264	2086682.78	749244.98	0.21	1.20	0.10	0.55
STAKE 265	2086703.63	749219.19	0.58	3.27	0.49	2.76

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 266	2086716.98	749249.52	0.25	1.40	0.14	0.79
STAKE 267	2086739.55	749225.96	0.35	1.99	0.25	1.44
STAKE 268	2086752.96	749254.54	0.37	2.11	0.28	1.57
STAKE 269	2086772.11	749230.15	0.48	2.70	0.39	2.19
STAKE 270	2086786.46	749258.83	0.40	2.25	0.30	1.72
STAKE 271	2086806.05	749233.85	0.55	3.11	0.46	2.60
STAKE 272	2086822.59	749264.51	0.35	1.97	0.25	1.42
STAKE 273	2086839.84	749239.81	0.49	2.76	0.40	2.25
STAKE 274	2086853.65	749268.88	0.43	2.42	0.34	1.90
STAKE 275	2086872.48	749243.17	0.45	2.56	0.36	2.05
STAKE 276	2086887.80	749272.81	0.35	1.99	0.26	1.45
STAKE 277	2086908.24	749248.77	0.38	2.15	0.28	1.61
STAKE 278	2086922.89	749277.76	0.32	1.81	0.22	1.24
STAKE 279	2086941.51	749252.38	0.31	1.76	0.21	1.19
STAKE 280	2086954.61	749282.82	0.31	1.76	0.21	1.19
STAKE 281	2086976.58	749257.58	0.28	1.61	0.18	1.02
STAKE 282	2086989.36	749289.10	0.27	1.53	0.16	0.93
STAKE 283	2087008.94	749260.27	0.30	1.68	0.19	1.10
STAKE 284	2087022.76	749291.23	0.31	1.77	0.21	1.20
STAKE 285	2087043.96	749264.07	0.29	1.64	0.19	1.06
STAKE 286	2087058.62	749295.66	0.30	1.68	0.19	1.10
STAKE 287	2087077.41	749269.69	0.29	1.66	0.19	1.07
STAKE 288	2087090.31	749300.35	0.25	1.41	0.14	0.79
STAKE 289	2087111.64	749272.84	0.25	1.41	0.14	0.80
STAKE 290	2087124.34	749303.89	0.26	1.47	0.15	0.87
STAKE 291	2087144.98	749278.13	0.31	1.77	0.21	1.20
STAKE 292	2087156.34	749308.92	0.25	1.42	0.14	0.81
STAKE 293	2087177.74	749282.13	0.33	1.88	0.23	1.32
STAKE 294	2087191.72	749312.83	0.22	1.27	0.11	0.64
STAKE 295	2087212.11	749286.56	0.29	1.66	0.19	1.08
STAKE 296	2087226.93	749317.71	0.21	1.18	0.09	0.53
STAKE 297	2087246.98	749292.78	0.28	1.60	0.18	1.01
STAKE 298	2087260.25	749323.23	0.25	1.43	0.14	0.82
STAKE 299	2087281.16	749298.05	0.23	1.33	0.12	0.70
STAKE 300	2087292.82	749328.93	0.24	1.36	0.13	0.74
STAKE 301	2087313.94	749301.66	0.27	1.50	0.16	0.90
STAKE 302	2087327.23	749332.53	0.23	1.29	0.12	0.66
STAKE 303	2087349.06	749307.91	0.24	1.33	0.13	0.71
STAKE 304	2087361.60	749336.45	0.19	1.10	0.08	0.44
STAKE 305	2087381.29	749310.79	0.21	1.19	0.10	0.54
STAKE 306	2086871.94	749301.75	0.21	1.22	0.10	0.57
STAKE 307	2086904.82	749304.60	0.24	1.34	0.13	0.72
STAKE 308	2086937.35	749310.77	0.35	1.98	0.25	1.43
STAKE 309	2086967.22	749312.84	0.31	1.76	0.21	1.19
STAKE 310	2087002.35	749320.48	0.35	1.99	0.25	1.44
STAKE 311	2087015.26	749350.62	0.22	1.25	0.11	0.61
STAKE 312	2087036.39	749322.69	0.37	2.07	0.27	1.53

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STAKE 313	2087050.73		0.35	2.00	0.26	1.45
STAKE 314	2087070.90		0.35	1.99	0.25	1.44
STAKE 315	2087084.44	749359.64	0.35	2.01	0.26	1.46
STAKE 316	2087103.84	749331.47	0.36	2.02	0.26	1.47
STAKE 317	2087119.41		0.32	1.83	0.22	1.27
STAKE 318	2087139.28		0.31	1.77	0.21	1.20
STAKE 319	2087153.02		0.30	1.71	0.20	1.13
STAKE 320	2087174.37	749341.53	0.31	1.77	0.21	1.20
STAKE 321	2087186.85	749369.91	0.29	1.64	0.19	1.06
STAKE 322	2087207.75	749343.63	0.27	1.52	0.16	0.92
STAKE 323	2087222.20		0.28	1.61	0.18	1.02
STAKE 324	2087241.84	749348.23	0.25	1.44	0.15	0.83
STAKE 325	2087255.60	749380.57	0.26	1.48	0.15	0.88
STAKE 326	2087276.03	749351.42	0.24	1.34	0.13	0.71
STAKE 327	2087288.33		0.26	1.46	0.15	0.85
STAKE 328	2087306.95	749360.37	0.25	1.42	0.14	0.81
STAKE 329	2087322.50	749387.48	0.22	1.27	0.11	0.63
STAKE 330	2087343.36	749364.78	0.23	1.30	0.12	0.67
STAKE 331	2087355.24	749392.28	0.23	1.31	0.12	0.69
STAKE 332	2087375.95	749368.06	0.24	1.38	0.13	0.76
STAKE 333	2087098.21	749391.03	0.26	1.48	0.15	0.87
STAKE 334	2087131.39	749394.00	0.36	2.05	0.27	1.51
STAKE 335	2087146.37	749423.75	0.28	1.61	0.18	1.02
STAKE 336	2087165.63	749396.16	0.41	2.35	0.32	1.82
STAKE 337	2087178.95	749431.41	0.18	1.04	0.07	0.37
STAKE 338	2087200.57	749403.70	0.41	2.32	0.32	1.80
STAKE 339	2087211.98	749434.17	0.29	1.66	0.19	1.08
STAKE 340	2087233.43	749410.44	0.36	2.02	0.26	1.47
STAKE 341	2087245.78	749439.84	0.24	1.36	0.13	0.74
STAKE 342	2087268.09	749414.00	0.29	1.66	0.19	1.07
STAKE 343	2087281.01	749443.36	0.24	1.38	0.13	0.76
STAKE 344	2087303.02	749419.38	0.23	1.31	0.12	0.68
STAKE 345	2087313.98	749449.12	0.24	1.38	0.13	0.76
STAKE 346	2087335.75	749422.10	0.24	1.34	0.13	0.71
STAKE 347	2087225.35	749466.89	0.22	1.22	0.10	0.58
STAKE 348	2087259.13	749473.38	0.24	1.35	0.13	0.73
STAKE 349	2087294.07	749478.27	0.23	1.31	0.12	0.68
STAKE 350	2087303.33	749508.86	0.17	0.94	0.05	0.26
STAKE 351	2087327.79	749483.35	0.25	1.44	0.15	0.83
STAKE 352	2087339.48	749514.49	0.18	1.02	0.06	0.35
STAKE 353	2086620.34	749178.63	0.25	1.40	0.14	0.78
STAKE 354	2086657.99	749183.21	0.31	1.74	0.21	1.17
STAKE 355	2086644.79	749153.59	0.22	1.25	0.11	0.61
STAKE 356	2086678.24	749157.14	0.49	2.77	0.40	2.26
STAKE 357	2086691.89	749188.03	0.16	0.93	0.04	0.24
STAKE 358	2086712.49	749159.10	0.49	2.75	0.40	2.24
STAKE 359	2086725.67	749190.70	0.48	2.74	0.39	2.23

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STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 360	2086746.55	749162.69	0.18	0.99	0.05	0.31
STAKE 361	2086759.54	749195.18	0.48	2.72	0.39	2.21
STAKE 362	2086780.07	749167.64	0.70	3.95	0.60	3.41
STAKE 363	2086792.71	749200.16	0.40	2.27	0.31	1.74
STAKE 364	2086816.37	749174.26	0.54	3.05	0.45	2.54
STAKE 365	2086828.92	749207.42	0.36	2.05	0.27	1.50
STAKE 366	2086849.63	749179.53	0.44	2.51	0.35	1.99
STAKE 367	2086862.74	749212.25	0.37	2.12	0.28	1.58
STAKE 368	2086883.87	749184.50	0.35	2.01	0.26	1.46
STAKE 369	2086896.25	749216.55	0.29	1.63	0.19	1.05
STAKE 370	2086916.59	749188.97	0.31	1.77	0.21	1.20
STAKE 371	2086929.36	749221.07	0.27	1.55	0.17	0.96
STAKE 372	2086950.73	749193.71	0.29	1.64	0.19	1.05
STAKE 373	2086963.65	749226.04	0.24	1.36	0.13	0.74
STAKE 374	2086984.28	749198.30	0.32	1.80	0.22	1.23
STAKE 375	2086996.28	749230.50	0.29	1.67	0.19	1.09
STAKE 376	2087017.46	749202.92	0.24	1.34	0.13	0.72
STAKE 377	2087032.08	749233.34	0.28	1.60	0.18	1.01
STAKE 378	2087052.05	749206.28	0.26	1.50	0.16	0.89
STAKE 379	2087065.66	749238.40	0.32	1.83	0.22	1.27
STAKE 380	2087085.80	749210.49	0.28	1.57	0.17	0.97
STAKE 381	2087099.82	749242.51	0.30	1.72	0.20	1.14
STAKE 382	2087119.53	749216.52	0.22	1.24	0.11	0.60
STAKE 383	2087133.04	749248.88	0.25	1.41	0.14	0.80
STAKE 384	2087152.11	749220.83	0.22	1.27	0.11	0.63
STAKE 385	2087166.35	749252.72	0.24	1.36	0.13	0.74
STAKE 386	2087186.71	749225.64	0.25	1.43	0.14	0.82
STAKE 387	2087200.74	749257.70	0.29	1.64	0.19	1.06
STAKE 388	2087220.90	749229.56	0.26	1.47	0.15	0.86
STAKE 389	2087234.84		0.21	1.20	0.10	0.56
STAKE 390	2087255.11	749233.63	0.33	1.89	0.23	1.33
STAKE 391	2087268.34	749265.73	0.22	1.25	0.11	0.62
STAKE 392	2087288.32	749237.25	0.33	1.86	0.23	1.30
STAKE 393	2087300.21		0.24	1.34	0.13	0.72
STAKE 394	2087321.02		0.29	1.62	0.18	1.03
STAKE 395	2087335.44		0.19	1.09	0.08	0.43
STAKE 396	2087355.99	749246.16	0.26	1.46	0.15	0.85
STAKE 397	2087368.75		0.23	1.29	0.12	0.66
STAKE 398	2087389.74		0.31	1.77	0.21	1.20
STAKE 399	2087401.04		0.23	1.33	0.12	0.71
STAKE 400	2087422.58		0.27	1.50	0.16	0.90
STAKE 401	2087437.14		0.18	1.04	0.07	0.37
STAKE 402	2087456.61		0.22	1.27	0.11	0.64
STAKE 403	2087470.61		0.21	1.19	0.10	0.55
STAKE 404	2087490.86		0.25	1.39	0.14	0.78
STAKE 405	2086561.74		0.46	2.63	0.37	2.11
STAKE 406	2086548.21	749086.09	0.96	5.46	0.84	4.76

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 407	2086596.76	749119.98	0.19	1.10	0.08	0.44
STAKE 408	2086580.90	749087.83	0.91	5.13	0.79	4.48
STAKE 409	2086629.92	749120.68	0.58	3.29	0.49	2.78
STAKE 410	2086615.78	749089.37	0.68	3.85	0.59	3.32
STAKE 411	2086664.45	749123.49	0.63	3.59	0.54	3.07
STAKE 412	2086649.33	749095.49	0.67	3.81	0.58	3.28
STAKE 413	2086695.21	749127.25	0.51	2.91	0.42	2.40
STAKE 414	2086683.90	749098.34	0.61	3.44	0.52	2.93
STAKE 415	2086731.42	749133.57	0.44	2.48	0.35	1.96
STAKE 416	2086717.19	749102.08	0.34	1.91	0.24	1.35
STAKE 417	2086766.20	749134.92	0.31	1.77	0.21	1.20
STAKE 418	2086752.50	749103.85	0.27	1.53	0.16	0.93
STAKE 419	2086802.23	749139.66	0.22	1.26	0.11	0.63
STAKE 420	2086790.86	749108.21	0.18	0.99	0.05	0.31
STAKE 421	2086837.67	749145.99	0.23	1.29	0.12	0.66
STAKE 422	2086824.02	749116.62	0.17	0.97	0.05	0.28
STAKE 423	2086871.87	749152.52	0.20	1.13	0.08	0.47
STAKE 424	2086857.56	749122.14	0.17	0.97	0.05	0.28
STAKE 425	2086905.62	749156.77	0.20	1.12	0.08	0.46
STAKE 426	2086893.22	749127.12	0.17	0.97	0.05	0.28
STAKE 427	2086938.27	749161.39	0.17	0.94	0.04	0.24
STAKE 428	2086927.00	749132.33	0.17	0.96	0.05	0.27
STAKE 429	2086973.43	749165.57	0.17	0.94	0.04	0.25
STAKE 430	2086960.45	749137.22	0.23	1.28	0.11	0.64
STAKE 431	2087006.42	749171.20	0.17	0.99	0.05	0.31
STAKE 432	2086993.76	749143.30	0.61	3.47	0.52	2.96
STAKE 433	2087038.27	749179.60	0.22	1.25	0.11	0.62
STAKE 434	2087027.49	749142.33	0.42	2.40	0.33	1.87
STAKE 435	2087074.17	749181.40	0.27	1.52	0.16	0.92
STAKE 436	2087061.22		0.41	2.35	0.32	1.82
STAKE 437	2087102.24	749193.92	0.31	1.78	0.21	1.21
STAKE 438	2087090.92	749164.16	0.39	2.21	0.30	1.67
STAKE 439	2087136.49		0.27	1.54	0.17	0.94
STAKE 440	2087123.98	749171.55	0.36	2.04	0.26	1.49
STAKE 441	2087170.11	749205.49	0.25	1.39	0.14	0.78
STAKE 442	2087157.33	749176.13	0.39	2.22	0.30	1.69
STAKE 443	2087204.83	749213.60	0.19	1.08	0.07	0.41
STAKE 444	2087192.17	749183.35	0.35	1.96	0.25	1.40
STAKE 445	2087243.12	749200.36	0.17	0.96	0.05	0.27
STAKE 446	2087227.71	749169.87	0.32	1.83	0.22	1.27
STAKE 447	2087277.86	749202.69	0.17	0.96	0.05	0.27
STAKE 448	2087262.48		0.29	1.64	0.19	1.05
STAKE 449	2087311.20		0.19	1.07	0.07	0.40
STAKE 450	2087296.44		0.29	1.63	0.18	1.04
STAKE 451	2087343.92		0.25	1.41	0.14	0.79
STAKE 452	2087331.01		0.18	1.04	0.06	0.37
STAKE 453	2087378.30		0.26	1.49	0.16	0.89

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 454	2087361.87	749186.54	0.17	0.97	0.05	0.28
STAKE 455	2087408.06	749218.60	0.24	1.38	0.13	0.76
STAKE 456	2087384.85	749189.53	0.17	0.97	0.05	0.28
STAKE 457	2087435.39	749222.88	0.16	0.93	0.04	0.23
STAKE 458	2087420.11	749191.65	0.17	0.99	0.05	0.30
STAKE 459	2086536.75	749055.99	0.84	4.76	0.73	4.15
STAKE 460	2086554.05	749026.53	1.63	9.22	1.36	7.72
STAKE 461	2086562.19	749057.49	1.26	7.16	1.09	6.16
STAKE 462	2086580.08	749028.77	1.52	8.64	1.29	7.29
STAKE 463	2086597.03	749061.14	0.85	4.82	0.74	4.20
STAKE 464	2086615.60	749032.48	1.07	6.04	0.93	5.26
STAKE 465	2086627.58	749061.75	0.29	1.64	0.19	1.05
STAKE 466	2086645.56	749030.78	0.31	1.76	0.21	1.19
STAKE 467	2086671.10	749064.99	0.17	0.97	0.05	0.28
STAKE 468	2086690.82	749039.12	0.50	2.85	0.41	2.34
STAKE 469	2086702.92	749068.15	0.17	0.95	0.05	0.26
STAKE 470	2086723.98	749042.16	0.57	3.23	0.48	2.72
STAKE 471	2086737.79	749071.92	0.17	0.95	0.05	0.26
STAKE 472	2086757.51	749046.85	0.62	3.49	0.52	2.97
STAKE 473	2086770.08	749077.21	0.17	0.94	0.04	0.25
STAKE 474	2086791.88	749049.92	0.52	2.94	0.43	2.43
STAKE 475	2086803.39	749079.50	0.17	0.95	0.05	0.26
STAKE 476	2086823.61	749059.77	0.28	1.59	0.18	0.99
STAKE 477	2086834.88	749081.75	0.17	0.94	0.04	0.25
STAKE 478	2087213.84	749139.42	0.31	1.78	0.21	1.21
STAKE 479	2087347.84	749158.63	0.27	1.53	0.16	0.93
STAKE 480	2087373.10	749135.66	0.26	1.45	0.15	0.85
STAKE 481	2087315.78	749152.09	0.26	1.45	0.15	0.84
STAKE 482	2087330.92	749131.32	0.26	1.48	0.15	0.88
STAKE 483	2087281.90	749148.60	0.28	1.58	0.18	0.99
STAKE 484	2087292.09	749125.88	0.25	1.41	0.14	0.80
STAKE 485	2087249.08	749144.09	0.26	1.45	0.15	0.84
STAKE 486	2087268.30	749118.18	0.28	1.57	0.17	0.98
STAKE 487	2087234.92	749113.25	0.23	1.33	0.12	0.70
STAKE 488	2087183.23	749137.41	0.32	1.83	0.22	1.27
STAKE 489	2087202.34	749109.22	0.29	1.66	0.19	1.08
STAKE 490	2087150.06	749134.59	0.30	1.68	0.19	1.10
STAKE 491	2087170.10	749106.46	0.30	1.69	0.20	1.11
STAKE 492	2087117.40	749128.71	0.39	2.21	0.30	1.67
STAKE 493	2087136.49	749103.82	0.29	1.63	0.18	1.04
STAKE 494	2087086.32	749122.40	0.33	1.88	0.23	1.32
STAKE 495	2087106.16	749102.80	0.34	1.95	0.25	1.39
STAKE 496	2087042.70	749116.51	0.35	2.01	0.26	1.46
STAKE 497	2087063.21	749091.86	0.28	1.59	0.18	1.00
STAKE 498	2087014.17	749118.17	0.30	1.70	0.20	1.12
STAKE 499	2087035.57	749090.76	0.48	2.71	0.39	2.20
STAKE 500	2087571.06	749409.41	0.16	0.92	0.04	0.23

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 501	2087553.20	749380.89	0.16	0.93	0.04	0.24
STAKE 502	2087525.20	749498.25	0.16	0.93	0.04	0.24
STAKE 503	2087537.17	749468.98	0.17	0.98	0.05	0.29
STAKE 504	2087555.23	749497.93	0.16	0.93	0.04	0.23
STAKE 505	2087573.24	749469.75	0.17	0.95	0.05	0.26
STAKE 506	2087591.09	749500.34	0.23	1.29	0.12	0.66
STAKE 507	2087607.83	749469.11	0.22	1.22	0.10	0.58
STAKE 508	2087624.87	749497.91	0.21	1.18	0.09	0.54
STAKE 509	2087640.16	749469.11	0.20	1.16	0.09	0.50
STAKE 510	2087659.36	749498.39	0.21	1.19	0.10	0.55
STAKE 511	2087674.45	749467.34	0.21	1.18	0.09	0.53
STAKE 512	2087691.86	749495.97	0.21	1.17	0.09	0.52
STAKE 513	2087708.66	749467.61	0.22	1.22	0.10	0.58
STAKE 514	2087725.23	749494.39	0.20	1.14	0.09	0.48
STAKE 515	2087742.45	749467.79	0.20	1.15	0.09	0.49
STAKE 516	2087785.38	749330.54	0.20	1.12	0.08	0.46
STAKE 517	2087606.16	749535.07	0.18	1.05	0.07	0.38
STAKE 518	2087643.87	749529.14	0.21	1.20	0.10	0.55
STAKE 519	2086484.30	748886.63	0.53	3.00	0.44	2.49
STAKE 520	2086491.94	748850.95	0.20	1.13	0.08	0.47
STAKE 521	2086512.51	748881.39	0.51	2.89	0.42	2.39
STAKE 522	2086522.57	748850.67	0.20	1.12	0.08	0.46
STAKE 523	2086545.95	748874.42	0.54	3.06	0.45	2.55
STAKE 524	2086547.67	748846.12	0.23	1.30	0.12	0.67
STAKE 525	2086574.57	748876.25	0.44	2.51	0.35	1.99
STAKE 526	2086581.87	748844.37	0.21	1.17	0.09	0.52
STAKE 527	2086607.62	748872.63	0.45	2.53	0.36	2.01
STAKE 528	2086623.66	748840.23	0.20	1.14	0.08	0.48
STAKE 529	2086637.65	748872.07	0.29	1.63	0.19	1.05
STAKE 530	2086660.29	748840.91	0.21	1.18	0.09	0.53
STAKE 531	2086681.15	748863.58	0.32	1.81	0.22	1.24
STAKE 532	2086694.01	748833.69	0.19	1.09	0.08	0.42
STAKE 533	2086716.35	748861.12	0.34	1.92	0.24	1.37
STAKE 534	2086730.16	748827.73	0.24	1.37	0.13	0.74
STAKE 535	2086749.45	748856.63	0.41	2.33	0.32	1.81
STAKE 536	2086762.10	748824.92	0.26	1.49	0.16	0.88
STAKE 537	2086779.83	748853.83	0.33	1.88	0.23	1.32
STAKE 538	2086793.16	748821.46	0.29	1.62	0.18	1.03
STAKE 539	2086812.79	748849.34	0.24	1.35	0.13	0.72
STAKE 540	2086825.52	748820.94	0.17	0.98	0.05	0.29
STAKE 541	2086845.07		0.17	0.98	0.05	0.29
STAKE 542	2086857.50		0.20		0.09	0.50
STAKE 543	2086887.91	748810.85	0.20		0.09	0.49
STAKE 544	2086870.70		0.17	0.94	0.04	0.24
STAKE 545	2086903.96		0.24		0.13	0.74
STAKE 546	2086494.68		0.83		0.72	4.08
STAKE 547	2086530.65	748906.12	0.85	4.79	0.74	4.18

	1		95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 548	2086566.08	748907.05	0.36	2.02	0.26	1.47
STAKE 549	2086599.00	748897.28	0.44	2.52	0.35	2.00
STAKE 550	2086632.94	748903.43	0.42	2.38	0.33	1.85
STAKE 551	2086655.98	748894.29	0.34	1.91	0.24	1.36
STAKE 552	2086696.86	748886.37	0.35	1.96	0.25	1.41
STAKE 553	2086731.12	748883.14	0.37	2.07	0.27	1.53
STAKE 554	2086766.03	748879.40	0.35	1.97	0.25	1.41
STAKE 555	2086799.13	748875.56	0.36	2.02	0.26	1.47
STAKE 556	2086831.90	748875.36	0.32	1.82	0.22	1.26
STAKE 557	2086849.54	748903.14	0.31	1.74	0.21	1.17
STAKE 558	2086880.69	748902.99	0.28	1.56	0.17	0.96
STAKE 559	2086903.73	748926.72	0.37	2.10	0.27	1.56
STAKE 560	2086869.98	748933.45	0.32	1.83	0.22	1.27
STAKE 561	2086835.46	748934.55	0.33	1.89	0.23	1.33
STAKE 562	2086803.60	748943.34	0.30	1.71	0.20	1.13
STAKE 563	2086813.19	748908.14	0.35	1.98	0.25	1.43
STAKE 564	2086767.88	748939.43	0.37	2.12	0.28	1.58
STAKE 565	2086781.53	748911.68	0.40	2.25	0.30	1.72
STAKE 566	2086737.13	748938.51	0.40	2.29	0.31	1.76
STAKE 567	2086749.52	748911.98	0.40	2.26	0.30	1.72
STAKE 568	2086704.79	748938.07	0.40	2.25	0.30	1.71
STAKE 569	2086716.40	748910.57	0.45	2.57	0.36	2.05
STAKE 570	2086672.63	748949.47	0.42	2.40	0.33	1.88
STAKE 571	2086681.12	748918.65	0.40	2.29	0.31	1.76
STAKE 572	2086646.07	748953.23	0.46	2.59	0.37	2.07
STAKE 573	2086661.66	748926.46	0.47	2.68	0.38	2.17
STAKE 574	2086621.24	748938.85	0.56	3.14	0.47	2.64
STAKE 575	2086595.46	748927.78	0.54	3.08	0.45	2.57
STAKE 576	2086568.73	748943.90	0.39	2.24	0.30	1.70
STAKE 577	2086539.86	748927.10	0.58	3.29	0.49	2.77
STAKE 578	2086522.01	748932.11	0.49	2.76	0.40	2.25
STAKE 579	2086486.25	748943.04	0.20	1.12	0.08	0.46
STAKE 580	2086512.06	748967.76	0.62	3.49	0.53	2.98
STAKE 581	2086542.06	748960.04	0.38	2.16	0.29	1.62
STAKE 582	2086533.86	748992.58	1.06	5.99	0.92	5.21
STAKE 583	2086567.53	748981.36	0.52	2.92	0.43	2.41
STAKE 584	2086601.86	748986.36	0.59	3.37	0.50	2.85
STAKE 585	2086591.86	748960.67	0.45	2.54	0.36	2.02
STAKE 586	2086623.59	748960.18	0.36	2.02	0.26	1.47
STAKE 587	2086641.51	749006.22	0.51	2.91	0.42	2.40
STAKE 588	2086660.28	748983.74	0.35	2.00	0.26	1.45
STAKE 589	2086678.38	749008.83	0.28	1.59	0.18	1.00
STAKE 590	2086711.53	749014.95	0.32	1.82	0.22	1.25
STAKE 591	2086743.97	749017.04	0.34	1.91	0.24	1.35
STAKE 592	2086775.42	749021.57	0.37	2.10	0.27	1.56
STAKE 593	2086806.37	749023.88	0.30	1.70	0.20	1.12
STAKE 594	2086934.51	749073.88	0.26	1.47	0.15	0.87

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STAKE 595	2086950.10		0.53	3.01	0.44	2.50
STAKE 596	2086968.72		0.48	2.74	0.39	2.23
STAKE 597	2086956.93		0.41	2.33	0.32	1.80
STAKE 598	2086992.66		0.36	2.06	0.27	1.51
STAKE 599	2087024.57		0.45	2.55	0.36	2.03
STAKE 600	2087057.56		0.37	2.08	0.27	1.53
STAKE 601	2087092.94		0.35	2.00	0.26	1.46
STAKE 602	2087121.18		0.34	1.94	0.24	1.38
STAKE 603	2087156.64		0.31	1.76	0.21	1.18
STAKE 604	2087141.17	749046.03	0.39	2.21	0.30	1.68
STAKE 605	2087079.88		0.41	2.30	0.31	1.77
STAKE 606	2087118.78		0.44	2.49	0.35	1.97
STAKE 607	2087045.61		0.47	2.64	0.38	2.12
STAKE 608	2087014.69		0.37	2.10	0.28	1.56
STAKE 609	2086978.38		0.39	2.21	0.30	1.67
STAKE 610	2086945.92		0.50	2.84	0.41	2.33
STAKE 611	2086967.39		0.33	1.86	0.23	1.30
STAKE 612	2087002.99		0.54	3.05	0.45	2.54
STAKE 613	2087035.03		0.38	2.15	0.28	1.61
STAKE 614	2087057.46	749008.54	0.42	2.39	0.33	1.87
STAKE 615	2087058.28	749007.25	0.36	2.03	0.26	1.48
STAKE 616	2087019.02	748975.71	0.32	1.80	0.22	1.23
STAKE 617	2086920.60		0.46	2.63	0.37	2.12
STAKE 618	2086956.09		0.38	2.15	0.28	1.61
STAKE 619	2087095.06		0.38	2.13	0.28	1.59
STAKE 620	2086707.77	748990.80	0.34	1.92	0.24	1.37
STAKE 621	2086734.85		0.31	1.74	0.21	1.16
STAKE 622	2086763.17	748992.09	0.34	1.92	0.24	1.36
STAKE 623	2086800.69		0.33	1.85	0.23	1.29
STAKE 624	2086833.86		0.37	2.12	0.28	1.58
STAKE 625	2086979.56		0.35	1.99	0.25	1.44
STAKE 626	2087001.32		0.34	1.94	0.24	1.38
STAKE 627	2086011.99		0.23	1.29	0.12	0.66
STAKE 628	2085995.86		0.22	1.22	0.10	0.57
STAKE 629	2085979.91		0.25	1.42	0.14	0.81
STAKE 630	2085962.06		0.27	1.55	0.17	0.95
STAKE 631	2085949.01		0.38	2.15	0.28	1.61
STAKE 632	2085932.47		0.21	1.18	0.09	0.53
STAKE 633	2085898.79		0.24	1.35	0.13	0.72
STAKE 634	2085913.92		0.18	1.05	0.07	0.37
STAKE 635	2085927.94		0.52	2.93	0.43	2.42
STAKE 636	2085944.79		0.20	1.13	0.08	0.48
STAKE 637	2085961.68		0.19	1.09	0.07	0.42
STAKE 638	2085974.40		0.18	1.05	0.07	0.38
STAKE 639	2085994.53		0.18	1.02	0.06	0.34
STAKE 640	2086014.75		0.33	1.85	0.23	1.28
STAKE 641	2086028.44		0.62	3.51	0.53	2.99

HPGe\_SORs

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 642	2086044.66		0.89	5.04	0.78	4.40
STAKE 643	2086062.46	748694.69	1.33	7.53	1.14	6.45
STAKE 644	2086079.03		1.03	5.85	0.90	5.09
STAKE 645	2086094.58	748690.61	0.24	1.36	0.13	0.73
STAKE 646	2086112.18		0.20	1.14	0.08	0.48
STAKE 647	2086129.58		0.48	2.70	0.39	2.19
STAKE 648	2086144.72		0.17	0.97	0.05	0.28
STAKE 649	2086157.19		0.35	1.96	0.25	1.40
STAKE 650	2086171.71		0.17	0.95	0.04	0.25
STAKE 651	2086189.44		0.65	3.67	0.56	3.15
STAKE 652	2086205.15		0.82	4.62	0.71	4.02
STAKE 653	2086228.59		0.51	2.87	0.42	2.36
STAKE 654	2086245.35		0.69	3.90	0.59	3.36
STAKE 655	2086212.71	748661.41	0.44	2.50	0.35	1.98
STAKE 656	2086179.36	748662.26	0.45	2.53	0.36	2.02
STAKE 657	2086148.29	748663.53	0.65	3.70	0.56	3.17
STAKE 658	2086132.71	748634.60	0.39	2.22	0.30	1.69
STAKE 659	2086120.16	748663.25	0.69	3.89	0.59	3.35
STAKE 660	2086102.76		0.37	2.07	0.27	1.53
STAKE 661	2086083.14	748663.60	0.58	3.30	0.49	2.79
STAKE 662	2086059.76		0.68	3.84	0.58	3.31
STAKE 663	2086043.93	748662.55	0.36	2.01	0.26	1.46
STAKE 664	2086028.25	748635.37	0.20	1.12	0.08	0.46
STAKE 665	2086013.85		0.20	1.14	0.09	0.49
STAKE 666	2085991.96		0.18	1.03	0.06	0.35
STAKE 667	2085977.51		0.18	1.02	0.06	0.34
STAKE 668	2085961.03	748634.76	0.35	1.97	0.25	1.42
STAKE 669	2085947.08	748667.47	0.53	3.00	0.44	2.49
STAKE 670	2085932.35	748639.73	0.30	1.70	0.20	1.12
STAKE 671	2085917.40	748667.30	0.33	1.90	0.24	1.34
STAKE 672	2085893.31	748639.67	0.16	0.92	0.04	0.23
STAKE 673	2085883.50	748672.23	0.18	1.01	0.06	0.34
STAKE 674	2085866.02	748643.46	0.18	1.00	0.06	0.32
STAKE 675	2085848.43	748670.27	0.17	0.98	0.05	0.29
STAKE 676	2085828.19	748649.88	0.18	1.02	0.06	0.35
STAKE 677	2085846.28	748620.32	0.17	0.96	0.05	0.27
STAKE 678	2085831.10	748589.20	0.17	0.97	0.05	0.28
STAKE 679	2085876.43	748610.24	0.17	0.94	0.04	0.25
STAKE 680	2085863.30	748583.01	0.18	1.00	0.06	0.32
STAKE 681	2085912.89	748612.55	0.23	1.32	0.12	0.70
STAKE 682	2085893.01	748583.89	0.21	1.20	0.10	0.55
STAKE 683	2085941.98	748608.45	0.32	1.82	0.22	1.25
STAKE 684	2085925.42	748579.35	0.28	1.57	0.17	0.98
STAKE 685	2085975.03		0.25	1.43	0.14	0.82
STAKE 686	2085957.79		0.23	1.29	0.12	0.66
STAKE 687	2086008.41		0.18	1.02	0.06	0.34
STAKE 688	2085994.62		0.23	1.30	0.12	0.67

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 689	2086041.99		0.33	1.89	0.24	1.33
STAKE 690	2086023.10		0.25	1.43	0.14	0.82
STAKE 691	2086080.34		0.32	1.82	0.22	1.25
STAKE 692	2086061.84		0.64	3.60	0.54	3.08
STAKE 693	2086105.02	748601.89	0.37	2.11	0.28	1.57
STAKE 694	2086087.02		0.29	1.63	0.18	1.04
STAKE 695	2086009.74	748542.43	0.26	1.48	0.15	0.88
STAKE 696	2086044.92		0.32	1.83	0.22	1.26
STAKE 697	2085977.40		0.24	1.38	0.13	0.76
STAKE 698	2085956.35	748516.63	0.23	1.32	0.12	0.70
STAKE 699	2085943.40		0.23	1.32	0.12	0.69
STAKE 700	2085924.09	748520.71	0.23	1.30	0.12	0.67
STAKE 701	2085914.95	748549.29	0.21	1.21	0.10	0.56
STAKE 702	2085894.42	748525.27	0.25	1.39	0.14	0.77
STAKE 703	2085883.17	748551.38	0.24	1.36	0.13	0.74
STAKE 704	2085862.87	748523.97	0.24	1.36	0.13	0.74
STAKE 705	2085849.54	748554.39	0.23	1.33	0.12	0.71
STAKE 706	2085827.99	748528.91	0.23	1.30	0.12	0.66
STAKE 707	2085817.34	748560.04	0.17	0.95	0.05	0.26
STAKE 708	2085793.39	748532.06	0.22	1.23	0.10	0.58
STAKE 709	2085782.28	748563.58	0.18	1.04	0.07	0.37
STAKE 710	2085762.97	748534.89	0.19	1.09	0.08	0.43
STAKE 711	2085776.37	748505.71	0.18	1.05	0.07	0.38
STAKE 712	2085756.39	748478.21	0.18	1.02	0.06	0.34
STAKE 713	2085808.65	748500.60	0.19	1.09	0.08	0.43
STAKE 714	2085792.16	748472.77	0.19	1.08	0.07	0.41
STAKE 715	2085843.90	748500.45	0.21	1.19	0.10	0.55
STAKE 716	2085823.40	748469.70	0.19	1.09	0.08	0.43
STAKE 717	2085875.75	748493.34	0.22	1.22	0.10	0.58
STAKE 718	2085854.49	748466.61	0.20	1.15	0.09	0.49
STAKE 719	2085803.34	748446.64	0.18	1.03	0.06	0.35
STAKE 720	2085767.26	748447.73	0.17	0.95	0.05	0.26
STAKE 721	2085740.42	748447.43	0.18	1.00	0.06	0.32
STAKE 722	2085751.82	748421.89	0.17	0.97	0.05	0.29
STAKE 723	2085706.53	748453.24	0.17	0.97	0.05	0.29
STAKE 724	2085717.51	748426.02	0.17	0.98	0.05	0.30
STAKE 725	2086043.15	748778.43	0.25	1.43	0.15	0.83
STAKE 726	2086026.41	748753.49	0.27	1.53	0.17	0.94
STAKE 727	2086075.86	748777.22	0.31	1.76	0.21	1.19
STAKE 728	2086058.57	748750.69	0.33	1.88	0.23	1.32
STAKE 729	2086110.88	748777.78	0.58	3.27	0.49	2.76
STAKE 730	2086093.33	748749.38	0.42	2.39	0.33	1.86
STAKE 731	2086135.06	748779.41	0.37	2.11	0.28	1.57
STAKE 732	2086125.78	748766.95	0.21	1.20	0.10	0.54
STAKE 733	2086178.62	748774.94	0.29	1.66	0.19	1.08
STAKE 734	2086159.48	748749.21	0.27	1.50	0.16	0.90
STAKE 735	2086215.26	748770.30	0.90	5.08	0.78	4.44

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 736	2086197.34		0.21	1.20	0.10	0.54
STAKE 737	2086245.82		0.34	1.90	0.24	1.34
STAKE 738	2086227.65		0.68	3.86	0.59	3.33
STAKE 739	2086279.41		0.37	2.10	0.27	1.56
STAKE 740	2086263.68		0.85	4.82	0.74	4.21
STAKE 741	2086315.84		0.32	1.79	0.21	1.22
STAKE 742	2086295.69		0.40	2.29	0.31	1.76
STAKE 743	2086329.29		0.44	2.48	0.35	1.96
STAKE 744	2086344.24		0.65	3.71	0.56	3.18
STAKE 745	2086298.38		0.61	3.43	0.52	2.92
STAKE 746	2086317.38		0.65	3.66	0.55	3.13
STAKE 747	2086264.28		0.50	2.84	0.41	2.33
STAKE 748	2086286.36		0.90	5.11	0.79	4.46
STAKE 749	2086829.73	748714.60	0.25	1.44	0.15	0.83
STAKE 750	2086846.94	748687.20	0.31	1.77	0.21	1.20
STAKE 751	2086872.12	748715.85	0.22	1.27	0.11	0.63
STAKE 752	2086880.98	748680.06	0.30	1.72	0.20	1.15
STAKE 753	2086912.17	748674.81	0.29	1.63	0.18	1.05
STAKE 754	2086947.93	748667.24	0.20	1.16	0.09	0.51
STAKE 755	2086892.78	748652.47	0.27	1.52	0.16	0.92
STAKE 756	2086928.32	748645.46	0.21	1.21	0.10	0.57
STAKE 757	2086980.50	748664.24	0.17	0.95	0.05	0.26
STAKE 758	2086960.81	748641.32	0.22	1.27	0.11	0.64
STAKE 759	2086906.52	748618.83	0.23	1.31	0.12	0.69
STAKE 760	2086870.77	748622.77	0.25	1.39	0.14	0.78
STAKE 761	2086780.10	748609.29	0.29	1.63	0.18	1.05
STAKE 762	2086818.54	748602.94	0.27	1.51	0.16	0.91
STAKE 763	2086850.71	748597.39	0.24	1.39	0.14	0.77
STAKE 764	2086882.07	748593.49	0.25	1.40	0.14	0.79
STAKE 765	2086759.73	748581.78	0.27	1.51	0.16	0.91
STAKE 766	2086793.64		0.28	1.60	0.18	1.01
STAKE 767	2086826.98	748569.40	0.27	1.53	0.16	0.93
STAKE 768	2086862.16		0.21	1.19	0.10	0.54
STAKE 769	2086894.85		0.24	1.35	0.13	0.73
STAKE 770	2086926.89		0.21	1.18	0.09	0.54
STAKE 771	2087045.32		0.23	1.31	0.12	0.68
STAKE 772	2087049.01		0.19	1.08	0.07	0.41
STAKE 773	2087079.96	***************************************	0.21	1.19	0.09	0.54
STAKE 774	2087092.15		0.25	1.41	0.14	0.80
STAKE 775	2087066.43		0.25	1.41	0.14	0.80
STAKE 776	2087098.70		0.15	0.87	0.03	0.17
STAKE 777	2087075.88		0.26	1.49	0.16	0.89
STAKE 778	2087108.21		0.33	1.87	0.23	1.31
STAKE 779	2087144.13		0.20	1.11	0.08	0.45
STAKE 780	2087177.75		0.19	1.08	0.07	0.42
STAKE 781	2087131.60		0.35	1.99	0.25	1.44
STAKE 782	2087165.49	749025.96	0.17	0.97	0.05	0.28

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	1		95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 783	2087197.83		0.20	1.14	0.08	0.48
STAKE 784	2087176.15		0.20	1.16	0.09	0.50
STAKE 785	2087188.64		0.24	1.36	0.13	0.74
STAKE 786	2087208.33		0.39	2.23	0.30	1.70
STAKE 787	2087217.83		0.27	1.55	0.17	0.95
STAKE 788	2087240.70		0.26	1.47	0.15	0.86
STAKE 789	2087254.79	749080.19	0.30	1.68	0.19	1.10
STAKE 790	2087279.28		0.25	1.42	0.14	0.81
STAKE 791	2087288.41	749085.84	0.27	1.52	0.16	0.92
STAKE 792	2087310.76		0.38	2.18	0.29	1.64
STAKE 793	2087321.04		0.28	1.57	0.17	0.98
STAKE 794	2087346.04		0.27	1.52	0.16	0.92
STAKE 795	2087356.00		0.27	1.53	0.16	0.93
STAKE 796	2087374.81	749063.66	0.25	1.41	0.14	0.80
STAKE 797	2087390.24		0.26	1.49	0.16	0.89
STAKE 798	2087415.33		0.25	1.44	0.15	0.83
STAKE 799	2087423.31		0.26	1.50	0.16	0.90
STAKE 800	2087452.90		0.27	1.53	0.17	0.94
STAKE 801	2087488.34		0.21	1.17	0.09	0.52
STAKE 802	2087526.79		0.17	0.95	0.05	0.26
STAKE 803	2087512.39		0.18	1.00	0.06	0.32
STAKE 804	2087480.31		0.23	1.31	0.12	0.69
STAKE 805	2087444.67		0.26	1.46	0.15	0.86
STAKE 806	2087469.09		0.27	1.54	0.17	0.94
STAKE 807	2087433.13		0.27	1.55	0.17	0.95
STAKE 808	2087398.61		0.28	1.58	0.18	0.99
STAKE 809	2087502.61		0.22	1.27	0.11	0.64
STAKE 810	2087494.31		0.27	1.54	0.17	0.94
STAKE 811	2087475.04		0.28	1.59	0.18	1.00
STAKE 812	2087455.58	749029.38	0.30	1.68	0.20	1.11
STAKE 813	2086428.55	748423.71	0.22	1.23	0.10	0.59
STAKE 814	2086408.52	748400.77	0.23	1.31	0.12	0.68
STAKE 815	2086463.90		0.22	1.23	0.10	0.59
STAKE 816	2086437.59	748390.24	0.22	1.27	0.11	0.63
STAKE 817	2086494.02		0.20	1.13	0.08	0.47
STAKE 818	2086475.34		0.23	1.28	0.11	0.64
STAKE 819	2086623.56		0.22	1.24	0.11	0.60
STAKE 820	2086657.69		0.24	1.36	0.13	0.73
STAKE 821	2086233.33		0.26	1.50	0.16	0.90
STAKE 822	2086222.98		0.29	1.65	0.19	1.07
STAKE 823	2086210.21		0.24	1.36	0.13	0.74
STAKE 824	2086200.39		0.28	1.60	0.18	1.01
STAKE 825	2086187.64		0.21	1.17	0.09	0.52
STAKE 826	2086178.19		0.24	1.38	0.13	0.76
STAKE 827	2086162.91		0.20	1.14	0.09	0.48
STAKE 828	2086153.45		0.22	1.25	0.11	0.61
STAKE 829	2086142.55		0.20	1.14	0.09	0.48

HPGe\_SORs

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 830	2086130.91	748448.19	0.21	1.21	0.10	0.57
STAKE 831	2086108.08	748422.01	0.21	1.21	0.10	0.56
STAKE 832	2086167.27	748530.05	0.26	1.46	0.15	0.86
STAKE 833	2086145.29	748499.13	0.24	1.34	0.13	0.71
STAKE 834	2086123.51	748480.84	0.23	1.30	0.12	0.66
STAKE 835	2086092.14	748491.43	0.23	1.30	0.12	0.67
STAKE 836	2086097.67	748458.18	0.21	1.19	0.10	0.55
STAKE 837	2086066.37	748467.49	0.22	1.22	0.10	0.58
STAKE 838	2086216.92	748458.65	0.22	1.25	0.11	0.61
STAKE 839	2086226.87	748425.94	0.21	1.19	0.10	0.54
STAKE 840	2086241.07	748481.07	0.28	1.57	0.17	0.98
STAKE 841	2086252.04	748450.08	0.17	0.98	0.05	0.29
STAKE 842	2086271.80	748470.16	0.17	0.97	0.05	0.28
STAKE 843	2086264.39	748419.04	0.17	0.98	0.05	0.30
STAKE 844	2086267.80	748507.44	0.20	1.11	0.08	0.45
STAKE 845	2086297.41	748499.72	0.26	1.48	0.15	0.88
STAKE 846	2087229.89	749027.16	0.31	1.75	0.21	1.18
STAKE 847	2087252.05	749001.05	0.27	1.54	0.17	0.94
STAKE 848	2087263.38	749032.05	0.29	1.63	0.18	1.04
STAKE 849	2087286.58	749005.57	0.31	1.75	0.21	1.18
STAKE 850	2087271.88	748975.19	0.30	1.69	0.20	1.11
STAKE 851	2087289.27	748944.12	0.18	1.00	0.06	0.32
STAKE 852	2087305.13	748974.31	0.31	1.73	0.20	1.16
STAKE 853	2087326.47	748946.99	0.29	1.67	0.19	1.09
STAKE 854	2087316.06	748914.81	0.26	1.46	0.15	0.86
STAKE 855	2087342.67	748920.75	0.28	1.60	0.18	1.01
STAKE 856	2087331.44		0.24	1.34	0.13	0.72
STAKE 857	2087365.81		0.25	1.44	0.15	0.83
STAKE 858	2087351.58		0.22	1.23	0.10	0.59
STAKE 859	2087385.54		0.23	1.33	0.12	0.70
STAKE 860	2087301.62		0.31	1.75	0.21	1.18
STAKE 861	2087333.58	749026.84	0.25	1.43	0.15	0.82
STAKE 862	2087307.04		0.28	1.60	0.18	1.01
STAKE 863	2087349.08		0.28	1.60	0.18	1.01
STAKE 864	2087338.44		0.31	1.76	0.21	1.19
STAKE 865	2087372.70		0.27	1.50	0.16	0.90
STAKE 866	2087357.50		0.29	1.62	0.18	1.04
STAKE 867	2087389.91		0.26	1.49	0.16	0.89
STAKE 868	2087373.33		0.29	1.65	0.19	1.07
STAKE 869	2087405.28		0.25	1.42	0.14	0.81
STAKE 870	2087389.98		0.28	1.59	0.18	1.00
STAKE 871	2087425.04		0.25	1.42	0.14	0.81
STAKE 872	2087406.36		0.28	1.56	0.17	0.97
STAKE 873	2087445.17		0.22	1.25	0.11	0.61
STAKE 874	2087427.73		0.25	1.41	0.14	0.79
STAKE 875	2087403.22		0.29	1.62	0.18	1.04
STAKE 876	2087368.01	749028.85	0.34	1.93	0.24	1.37

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 877	2087417.28		0.29	1.63	0.18	1.04
STAKE 878	2087386.65		0.29	1.62	0.18	1.04
STAKE 879	2087437.93		0.29	1.63	0.18	1.04
STAKE 880	2087406.08		0.24	1.37	0.13	0.75
STAKE 881	2087456.10		0.22	1.25	0.13	0.61
STAKE 882	2087418.62		0.26	1.49	0.16	0.89
STAKE 883	2087440.46		0.24	1.33	0.13	0.71
STAKE 884	2087473.65		0.27	1.53	0.16	0.93
STAKE 885	2087455.07	748878.02	0.23	1.29	0.12	0.66
STAKE 886	2087475.83		0.24	1.38	0.12	0.76
STAKE 887	2087446.50		0.29	1.66	0.19	1.08
STAKE 888	2087460.75		0.30	1.67	0.19	1.09
STAKE 889	2087484.59		0.25	1.39	0.14	0.78
STAKE 890	2087498.45		0.32	1.80	0.22	1.23
STAKE 891	2087506.99		0.24	1.36	0.13	0.74
STAKE 892	2087517.86		0.27	1.51	0.16	0.91
STAKE 893	2087560.06		0.21	1.17	0.09	0.52
STAKE 894	2087540.07		0.27	1.50	0.16	0.90
STAKE 895	2087530.40		0.25	1.44	0.15	0.83
STAKE 896	2087510.80		0.32	1.79	0.22	1.22
STAKE 897	2087383.28		0.26	1.48	0.15	0.87
STAKE 898	2087402.38	TA	0.27	1.51	0.16	0.91
STAKE 899	2087416.79		0.17	0.94	0.04	0.25
STAKE 900	2087436.97	749144.05	0.26	1.45	0.15	0.84
STAKE 901	2087443.92	749172.92	0.17	0.94	0.04	0.25
STAKE 902	2087462.75	749150.11	0.17	0.97	0.05	0.29
STAKE 903	2087493.41		0.16	0.91	0.04	0.21
STAKE 904		748558.15	0.23	1.31	0.12	0.68
STAKE 905	2086808.19		0.26	1.49	0.16	0.89
STAKE 906	2086842.92	748540.42	0.26	1.50	0.16	0.89
STAKE 907	2086881.06		0.21	1.17	0.09	0.52
STAKE 908	2086887.73		0.21	1.21	0.10	0.57
STAKE 909	2086905.52		0.21	1.19	0.10	0.55
STAKE 910	2086862.97		0.24	1.34	0.13	0.71
STAKE 911	2086850.42		0.23	1.32	0.12	0.69
STAKE 912	2086831.65	748485.08	0.25	1.44	0.15	0.83
STAKE 913	2086818.67	748518.23	0.26	1.49	0.16	0.89
STAKE 914	2086848.01	748456.12	0.23	1.33	0.12	0.70
STAKE 915	2086814.44	748457.22	0.23	1.32	0.12	0.69
STAKE 916	2086930.83	748613.85	0.24	1.35	0.13	0.72
STAKE 917	2086535.55		0.21	1.19	0.10	0.55
STAKE 918	2086940.94	748701.01	0.25	1.43	0.14	0.81
STAKE 919	2086927.62	748733.16	0.20	1.11	0.08	0.45
STAKE 920	2086972.19		0.17	0.98	0.05	0.29
STAKE 921	2086961.39		0.17	0.96	0.05	0.27
STAKE 922	2086901.45		0.26	1.45	0.15	0.84
STAKE 923	2087197.25		0.17	0.96	0.05	0.27

HPGe\_SORs 22

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 924	2087161.31		0.19	1.08	0.07	0.41
STAKE 925	2087203.08	748943.92	0.17	0.96	0.05	0.27
STAKE 926	2087180.11		0.20	1.11	0.08	0.45
STAKE 927	2087181.59		0.18	1.02	0.06	0.34
STAKE 928	2087209.96		0.22	1.26	0.11	0.63
STAKE 929	2087194.59		0.17	0.97	0.05	0.28
STAKE 930	2087227.36		0.16	0.92	0.04	0.22
STAKE 931	2087208.74		0.18	1.00	0.06	0.31
STAKE 932	2087238.68		0.20	1.11	0.08	0.44
STAKE 933	2087222.92		0.17	0.95	0.05	0.27
STAKE 934	2087248.82		0.19	1.08	0.07	0.41
STAKE 935	2087269.97		0.18	1.00	0.06	0.32
STAKE 936	2087235.70		0.17	0.98	0.05	0.29
STAKE 937	2087307.99		0.17	0.94	0.04	0.25
STAKE 938	2087300.55		0.21	1.20	0.10	0.56
STAKE 939	2087334.92		0.17	0.94	0.04	0.24
STAKE 940	2087332.18		0.20	1.15	0.09	0.49
STAKE 941	2087312.61		0.18	1.00	0.06	0.32
STAKE 942	2087341.68		0.19	1.08	0.07	0.41
STAKE 943	2087313.90		0.21	1.21	0.10	0.57
STAKE 944	2087295.72		0.23	1.29	0.12	0.66
STAKE 945	2087287.17		0.22	1.25	0.11	0.62
STAKE 946	2087258.35		0.20	1.15	0.09	0.49
STAKE 947	2087247.70		0.21	1.18	0.09	0.54
STAKE 948	2087224.31		0.27	1.53	0.16	0.93
STAKE 949	2087034.40		0.17	0.95	0.05	0.26
STAKE 950	2087071.95		0.19	1.06	0.07	0.38
STAKE 951	2087061.23		0.18	1.00	0.06	0.32
STAKE 952	2087036.65		0.18	1.01	0.06	0.33
STAKE 953	2087525.75		0.19	1.10	0.08	0.44
STAKE 954	2087533.72		0.17	0.95	0.05	0.26
STAKE 955	2087537.36		0.20	1.15	0.09	0.50
STAKE 956	2087555.10		0.17	0.96	0.05	0.27
STAKE 957	2087575.95		0.16	0.93	0.04	0.24
STAKE 958	2087586.41		0.17	0.96	0.05	0.27
STAKE 959	2087610.07		0.16	0.93	0.04	0.24
STAKE 960	2087575.78		0.17	0.95	0.05	0.26
STAKE 961	2087587.03		0.16	0.93	0.04	0.24
STAKE 962	2087554.79		0.25	1.42	0.14	0.81
STAKE 963	2086065.24		0.22	1.23	0.10	0.59
STAKE 964	2086032.84		0.39	2.22	0.30	1.69
STAKE 965	2086052.18		0.41	2.33	0.32	1.80
STAKE 966	2086017.66		0.49	2.77	0.40	2.26
STAKE 967	2086035.79		0.19	1.07	0.07	0.41
STAKE 968	2085999.94		0.20	1.12	0.08	0.46
STAKE 969	2086094.54		0.27	1.50	0.00	0.90
STAKE 970	2086061.05		0.23	1.31	0.10	0.90

HPGe\_SORs

			95% UCL	95% UCL	Best Fit	Best Fit
STAKE NUMBER	Easting	Northing	Tier I SOR (Fstat)	Tier II SOR (Fstat)	Tier I SOR	Tier II SOR
STAKE 971	2086108.80	748833.60	0.51	2.91	0.42	2.40
STAKE 972	2086076.46	748833.56	0.37	2.10	0.28	1.56
STAKE 973	2086125.64	748805.14	0.54	3.08	0.45	2.57
STAKE 974	2086094.17	748804.70	0.29	1.62	0.18	1.03
STAKE 975	2086197.51	748811.66	0.30	1.71	0.20	1.14
STAKE 976	2086159.10	748806.93	0.40	2.24	0.30	1.71
STAKE 977	2087577.45	748929.07	0.17	0.95	0.05	0.26
STAKE 978	2087606.93	748930.54	0.17	0.95	0.05	0.27
STAKE 979	2087533.36	748892.60	0.26	1.45	0.15	0.84
STAKE 980	2087586.64	748873.10	0.17	0.96	0.05	0.27
STAKE 981	2087523.00	748859.19	0.22	1.24	0.11	0.60
STAKE 982	2087562.50	748984.15	0.17	0.98	0.05	0.30
STAKE 983	2085961.45	748811.19	0.19	1.08	0.07	0.41
STAKE 984	2085993.20	748810.57	0.33	1.87	0.23	1.31
STAKE 985	2086149.45	748839.14	0.38	2.14	0.28	1.60
STAKE 986	2086172.77	748836.52	0.36	2.07	0.27	1.52
STAKE 987	2086219.88	748837.21	0.41	2.31	0.31	1.78
STAKE 988	2086249.69	748838.01	0.50	2.84	0.41	2.33
STAKE 989	2086235.08	748808.23	0.23	1.33	0.12	0.70
STAKE 990	2086367.63	748853.39	0.57	3.20	0.48	2.69
STAKE 991	2086391.09	748876.46	0.32	1.81	0.22	1.25
STAKE 992	2086335.75	748865.94	0.63	3.56	0.54	3.04
STAKE 993	2086348.72	748882.55	0.68	3.87	0.59	3.34
STAKE 994	2086302.93	748870.92	0.25	1.42	0.14	0.81
STAKE 995	2086325.51	748894.28	0.23	1.28	0.12	0.65
STAKE 996	2085771.64	748593.02	0.17	0.97	0.05	0.28
STAKE 997	2085797.29	748592.93	0.16	0.93	0.04	0.24
STAKE 998	2085736.48	748595.27	0.18	1.03	0.06	0.35
STAKE 999	2085748.47	748566.43	0.17	0.94	0.04	0.25

l			:			U-233/234	U-235	U-238	Pu 239/240	Am-24
Borehole		NORTHING		Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g
90098	2085611	*****************************	asphalt	0.0-0.6	PCI/G	0.909	0.034	0.888	0.042	0.0
90198	2085686	(Mary 111 11 11 11 11 11 11 11 11 11 11 11 1	asphalt	0.0-0.5	PCI/G	0.842	0.039	0.919	0.029	0.0
90398	2085835	PROTOCOLOGIC CONTRACTOR CONTRACTO	asphalt	0.0-0.4	PCI/G	0.746	0.041	0.791	0.097	0.0
90698	2085685	*******************************	asphalt	0.0-0.5	PCI/G	0.672	0.038	0.607	0.001	0.0
90798	2085760		asphalt	0.0-0.4	PCI/G	0.859	0.035	0.851	0.01	0.0
91198	2085685		asphalt	0.0-0.4	PCI/G	0.782	0.012	0.736	0.047	0.
91298	2085760		asphalt	0.0-0.5	PCI/G	0.665	0.04	0.596	-0.002	0.0
91898	2085834		asphait	0.0-0.6	PCI/G	1.13	0.133	0.75	1.22	0.3
91998	2085909	harmon and articles and articles and articles and articles are also and articles are also are	asphalt	0.0-0.5	PCI/G	0.663	0.049	0.598	0.034	0.0
96098	2085612	749211	bedrock	15.8-16.0	PCI/G	0.185	-0.006	0.215	0.042	-0.0
96198	2085687	749213	bedrock	15.5-15.8	PCI/G	0.412	0.047	0.707	0.25	0.0
96298	2085611		bedrock	15,9-16.1	PCI/G	0.515	0.064	0.795	0.008	0.0
96398	2085610	749061	bedrock	16.0-16.2	PCI/G	0.731	0.073	0.69	0.041	0.0
96498	2085910	749141	bedrock	21.4-22.0	PCI/G	0.538	0.009	0.782	0.186	0,0
96598	2085867	749147	bedrock	22.7-22.9	PCI/G	0.904	0.063	0.842	0.044	0.0
96698	2085846	749128	bedrock	22.8-23.0	PCI/G	0.603	0.113	0.43	0.048	
96898	2085713	749095	bedrock	16.2-16.4	PCI/G	0.402	0.048	0.388	0.357	0.2
96998	2085711	749038	bedrock	17.5-17.6	PCI/G	0.337	0.01	0.693	0.008	0.0
97098	2085611	748986	bedrock	16.2-16.5	PCI/G	0.444	0.017	0.618	0.032	0.0
97198	2085611	748911	bedrock	24.2-24.4	PCI/G	0.404	0.015	0.526	0.038	
97298	2085930	manager of the commence of the	bedrock	17.9-18.1	PCI/G	0.358	0.054	0.748	0.019	0.0
90098	2085611	749212	fill	0.6-1.0	PCI/G	0.837	0.077	1.09	2.93	0.6
90198	2085686	749214	fill	0.5-0.9	PCI/G	0.913	0.033	0.857	2,62	0.5
90298	2085761	749211	fill	0.5-0.8	PCI/G	1.06	0.051	1.24	20.5	5
90398	2085835	749215	fill	0.4-0.8	PCI/G	0.837	0.029	0.939	1.37	0.3
90698	2085685	749139	fill	0.5-0.8	PCI/G	0.956	0.035	1.21	0.686	0.1
90798	2085760	749137	fill	0.4-0.8	PCI/G	1.08	0.079	1.08	8.13	va committee va altitude committee va commit
91198	2085685	749064	fill	0.4-0.9	PCI/G	0.728	0.042	0.844	4.6	0.9
91298	2085760	749062	fill	0.5-1.0	PCI/G	1.12	0.066	1.24	7,45	1
91798	2085759	748989	fill	0.5-1.1	PCI/G	1.22	0.055	1.16	4.36	0.8
91898	2085834	748990	***************************************	0.6-1.1	PCI/G	2.02	0.487	2.77	558	1
91998	2085909	748990	fill	0.5-0.9	PCI/G	0.907	0.058	0.174	0.41	0.0
92298	2085760	748914	fill	0.5-0.9	PCI/G	0.997	0.066	1.2	34	6
91198	2085685	749064	native	11.1-11.6	PCI/G	0.412	0	0.613	0.01	0.
91198	2085685	749064	native	15.1-15.5	PCI/G	0.467	0.04	0.574	0.073	0.0
91198	2085685	749064	native	18,6-19.1	PCI/G	0.48	0.031	0.603	0.009	0.0
91198	2085685	749064	native	19.8-20.2	PCI/G	0.578	0.037	0.698	0.047	0.0
91198	2085685	749064	Yananannan	7.4-7.7	PCI/G	0.315	0.009	0.341	0.009	0.0
92598	2085560	749064	native	12.0-12.5	PCI/G	0.379	0.027	0.4	0.056	0.0
92598	2085560	749064	Page	16.0-16.75	PCI/G	0.353	0.027	0.437	0.033	-0.0
92598	2085560	749064	auny management and a second	3,5-4,0	PCI/G	0.491	0.017	0.532	0.609	0.0
92598	2085560	749064		7.5-8.0	PCI/G	0.433	0.024	0.455	0.021	0.0
95998	2085893	749140		12.2-12.4	PCI/G	0.475	0.137	0.61	0.027	0.0
95998	2085893	749140		15.2-15.4	PCI/G	0.572	0.118	0.773	0.004	
95998	2085893	749140		17.5-17.9	PCI/G	0.6	0.106	0.483	0.023	***************
95998	2085893	inamentary parameter and the contract parameter in the contract of the contrac		20.2-20.6	PCI/G	0.455	0.21	1.08	-0.019	0.0
95998	2085893	749140		4.8-5.0	PCI/G	0.315	0.194	0.657	-0.003	····
95998	2085893	,	CONTRACTOR OF THE PROPERTY OF	8.2-8.4	PCI/G	0.636	0.147	0.692	-0,000	0.0
96098	2085612			12.3-12.5	PCI/G	0.743	0.015	1.35	0.602	0.0
96098	2085612	Marin 1999 Marin 1999 Marin 1999 Marin 1999		4.3-4.5	PCI/G	0.312	0.033	0.705	0.047	0.0
96098	2085612	749211		8.2-8.5	PCI/G	0.386	0.000	0.583	0.067	0.0
96198	2085687	749213	and the second second second second second	11.8-12.0	PCI/G	0.606	0.025	0.688	0.231	0.0
96198	2085687	749213		4.2-4.4	PCI/G	0.505	0.017	0.677	0.021	0.0
96198	2085687	749213		7.7-8.1	PCI/G	0.539	0.017	0.484	0.021	0.0
96298	2085611	749213		11.9-12.25	PCI/G	0.539	0.016	0.752	0.068	0.0
96298	2085611	749135		4.0-4.3	PCI/G	0.546	0.003	0.752	2.84	0.0
96298	2085611	749135 749135	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	7.0-8.0	PCI/G	0.656	0.003	1.06	1.63	
96398	2085610	000-17712000-1777000000-17712000-1771	anarore rananarare e ananaror e torre	12.2-12.4	PCI/G	0.588	0.113	0.715	1.83	*******
96398	2085610			4.0-4.3	PCI/G	0.588	0.046	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
····	*************************		THE STATE OF THE S	Street and the second s	ri Baran erregionera memberaria a compressoria.	francourse and a commence of the	a conversa conservada e e e e e e e e e e e e e e e e e e	0.563	1.99	*********
96398	2085610			8.2-8.4	PCI/G	0.309	0.05	0.442	0.522	0.7
96498	2085910			12.2-13.0	PCI/G	0.382	0.012	0.562	0.077	0.0
96498	2085910			15.3-16.0	PCI/G	0.45	0.033	0.544	0,504	0.
96498	2085910	******************************	\$****************************	17.7-18.0	PCI/G	0.366	0.01	0.468	0.361	0.
96498	2085910			4.4-4.8	PCI/G	0.349	0.027	0.296	1.11	0.
96498	2085910	THE PROPERTY OF THE PROPERTY O		9.0-9.5	PCI/G	0.398	0.031	0.533	0.528	*********
96598	******************			11.4-11.6	PCI/G	0.422	0.04	0,55	0,032	0.0
96598	2085867	749147	native	15.6-15.8	PCI/G	0.589	0.019	0.654	0.031	C

_						U-233/234	U-235	U-238	Pu 239/240	Am-24
Borehole	EASTING			Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g
96598	2085867	749147	native	18.4-18.6	PCI/G	0.43	0	0.449	0.027	
96598	2085867	749147	native	4.0-4.2	PCI/G	0.417	0.033	0.389	0.071	
96598	2085867	749147	native	8.2-8.4	PCI/G	0.413	0.016	0.398	-0.006	0.0
96698	2085846	749128	native	12.2-12.4	PCI/G	0.403	0.003	0.542	0.009	0.0
96698	2085846	Barrers and the commence of th	concrete contraction of the cont	17.5-17.7	PCI/G	0.629	0.069	0.678	0.01	0.0
96698	2085846	749128	native	20.0-20.2	PCI/G	0.383	0.163	0.364	0.448	0.
96698	2085846	749128	native	4.0-4.2	PCI/G	0.669	0.034	0.584	0.008	
96698	2085846	749128	native	8.2-8.4	PCI/G	0.504	0.009	0.597	0.025	0.0
96798	2085866	749108	native	12.2-12.5	PCI/G	0.647	0.071	0.788	0.017	0.0
96798	2085866	749108	native	16.6-16.8	PCI/G	0.506	0.026	0.796	-0.008	0.0
96798	2085866	749108	native	20.0-20.4	PCI/G	0.578	0.055	0.52	0	0.0
96798	2085866	749108	native	4.2-4.4	PCI/G	1.4	0.097	1.46	0.017	
96798	2085866	749108	native	8.2-8.4	PCI/G	0.281	0.019	0.693	0.047	0.0
96898	2085713	749095	native	12.1-12.3	PCI/G	0.389	0.016	0.325	0.121	0.2
96898	2085713	749095	native	4.2-4.4	PCI/G	0.479	0.003	0.54	0.348	0.0
96898	2085713	Contraction of the Contraction o		8.2-8.4	PCI/G	0.435	0,009	0.495	0.459	0.0
96998	2085711	£		12.2-12.4	PCI/G	0.614	0.032	0.69	0.013	-0.0
96998	2085711	749038		4.2-4.4	PCI/G	0.502	0.03	0.652	0.052	0.0
96998	2085711	749038		8.2-8.4	PCI/G	0.523	0.017	0.566	-0.006	0.0
97098	2085611	748986		12.2-12.4	PCI/G	0.82	0.009	0.783	0.198	0.0
97098	2085611	748986 748986		4.0-4.2	PCI/G	0.62	-0.012	0.763	1.33	0.6
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	******************************			.S		,	~~~~~~ <del>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</del>	***************************************	£	common community as
97098	2085611	748986		8.2-8.4	PCI/G	0.564	0.002	0.657	1.24	0.1
97198	2085611	748911		12.2-12.4	PCI/G	0.776	0.035	0.967	0.049	0.
97198	2085611	748911		15.4-15.5	PCI/G	0.406	0	0.451	0.013	0.1
97198	2085611	748911		20.2-20.4	PCI/G	0.367	0.047	0.531	0.163	0.0
97198	2085611	748911		4.2-4.4	PCI/G	0.613	0.063	0.697	0.118	0.0
97198	2085611	748911	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	7.0-7.3	PCI/G	0.573	0.014	0.557	0.482	0.1
97298	2085930	748844	native	12.2-12.4	PCI/G	0.592	0.053	0.512	0.098	0.0
97298	2085930	748844	native	16.2-16.4	PCI/G	0.387	0.058	0.423	0.157	0.0
97298	2085930	748844	native	4.4-4.6	PCI/G	0.441	0.012	0.779	0.023	0.0
97298	2085930	748844	native	8.2-8.4	PCI/G	0.673	0.031	0.617	0.009	0.0
97698	2085880	749135	native	11.6-11.8	PCI/G	0.511	0.042	0.695	0.019	
97698	2085880	&+++++++++++++++++++++++++++++++++++++		13.9-14.1	PCI/G	0.38	0.021	0.62	0	
97698	2085880		processor de monte de constante de la procesa de la	16.1-16.3	PCI/G	0.442	0.122	0.687	0.018	0.0
97698	2085880	&		18.0-18.2	PCI/G	0.527	0.144	0.977	0.048	0.0
97698	2085880			19.8-20.0	PCI/G	0.473	-0.01	0.486	0	
97698	2085880	\$		4.2-4.6	PCI/G	0.519	0.122	0.400	0.06	0.0
97698	2085880	33333333333333333333333333333333333333	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	8.6-8.8	PCI/G	0.318	0.122	0.538	0.021	0.0
		\$		· &	, E				~ <del></del>	0.0
90098	2085611		native 1	1.0-1.5	PCI/G	1.14	0.071	1.68	4.85	U.3
90198	2085686		native 1	0.9-1.4	PCI/G	1.58	0.384	1.9	711	
90298	2085761		native 1	0.8-1.1	PCI/G	3.11	0,213	8.5	9110	18
90398	2085835	\$ <b>.</b>	native 1	0.8-1.3	PCI/G	0.748	0.026	0.894	3.01	0.5
90498	2085910		native 1	0.7-1.2	PCI/G	1.37	0.158	2.68	284	5
90598	2085610	}	native 1	1.1-1.6	PCI/G	0.842	0.038	1.59	142	3
90698	2085685		native 1	0.8-1.5	PCI/G	5.14	0.577	7.92	10670	18
90798	2085760	§	native 1	0.8-1.5	PCI/G	0.973	0.134	1.91	260	6
90898	2085835	749140	native 1	0.9-1.4	PCI/G	3.56	0.169	5.21	685	
90998	2085910	749141	native 1	0.8-1.3	PCI/G	10.8	0.566	26.8	1210	
91098	2085610	749062	native 1	1.4-1.9	PCI/G	0.749	0.091	1.23	2500	
91198	2085685	749064	native 1	0.9-1.3	PCI/G	0.848	0.032	1.54	125	2
91298	2085760	749062	native 1	1.0-1.5	PCI/G	0.798	0.066	1.51	242	3
91398	2085834	}	native 1	0.8-1.3	PCI/G	178	16.9	780	6600	1:
91498	2085909	\$	native 1	0.8-1.3	PCI/G	6.18	1.74	15.2	768	
91598	2085610	***************************************	native 1	1.5-2.0	PCI/G	19.8	7.2	28.2	152260	310
91698	2085684	\$.v	native 1	0.9-1.4	PCI/G	1.83	-0.913	0.913	389	3:
91798	2085759	{	native 1	1.1-1.6	PCI/G	0,838	0.045	1.72	7960	
91898	2085834	<b>&amp;</b>	native 1	1.1-1.6	PCI/G	10.7	2.52	13.2	2420	
91998	2085909	\$	native 1	0.9-1.4	PCI/G	2.53	0.961	2.69	2420 581	
		&		.3			····			
92098	2085609	Zanga namang pangang managan kananan kananan kananan kananan kananan kananan kananan kananan kananan kananan k	native 1	0.9-1.4	PCI/G	1.3	0.038	1.03	0.969	1
92298	2085760	\$a	native 1	0.9-1.6	PCI/G	0.764	0.029	0.866	18	3
92198	2085684		native 1	0.7-1.2	PCI/G	1.37	0.048	0.62	104	1
92398		§	native 1	1.3-1.8	PCI/G	0.797	0.073	0.656	10	1
92498	***************	ผู้สามารถการการการการการการครายการสามารถการการการการการการการการการการการการการก	native 1	1.1-1.6	PCI/G	0.758	0.092	1.1	474	5
92598	2085560	749064	native 1	0.0-0.2	PCI/G	0.966	0.18	1.15	93.6	1
92698	2085551	748977	native 1	0.0-0.4	PCI/G	0.788	0.062	0.789	5.83	C
92798	2085553	748827	native 1	0.0-0.4	PCI/G	1.05	0.045	0.852	3.49	0.
92898		\$	native 1	0.5-1.0	PCI/G	1	0.038	0.994	0.817	0.

Danahala	FAOTINO	NODTUNO		1.1.1450		U-233/234	U-235	U-238	Pu 239/240	Am-241
Borehole	EASTING	NORTHING		Interval(ft)	unit_code	pCi/g	pCi/g	pCi/g	pCi/g	pCi/g
92998	2085853	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	native 1	0.0-0.5	PCI/G	0.418	0.016	0.494	90.2	15.6
93098	2086005	b	native 1	0.0-0.5	PCI/G	0,866	0.017	0.863	37.6	7.86
93198	2086167	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	native 1	0.0-0.5	PCI/G	1.29	-0.196	2.53	808	128
93298	2085755		native 1	0.0-0.5	PCI/G	0.963	0.051	1.42	45.9	9.3
93398 93498	2085857 2086198	CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF	native 1 native 1	0.0-0.5	PCI/G	1.34	0.033	1.33	19.1	3.39
93598		\$		0.0-0.5	PCI/G	1.05	0.066	1.56	326	56.1
93698	2085978 2086153	******************************	native 1 native 1	0.0-0.4	PCI/G PCI/G	0.893 1.13	0.169	1.82	417	80.5 225
93798	2086300		native 1	0.0-0.5 0.0-0.45	PCI/G	1.13	0.086 0.123	3.78 0.538	1170 472	75.6
93898	2086406		native 1	0.0-0.43	PCI/G	0.803	0.123	1.16	196	35.9
93998	2086000	b-1	native 1	0.0-0.5	PCI/G	0.003	0.017	1.15	39.3	30.8
94098	2086128	***************************************	native 1	0.0-0.4	PCI/G	35.8	4.17	75.7	14950	3140
94198	2086298	\$	native 1	0.0-0.4	PCI/G	1.13	0.051	1.66	229	35.7
94298	2086438	*******************************	native 1	0.0-0.5	PCI/G	0.859	0.033	1.03	56.3	10
94398	2085550		native 1	0.0-0.3	PCI/G	1.06	0.032	1.06	2.32	0.497
94498	2085552		native 1	0.0-0.3	PCI/G	0.949	0.096	0.949	4.9	0.839
94598	2085703		native 1	0.0-0.5	PCI/G	0.801	0.014	0.995	19.2	2.91
94698	2085852	***************************************	native 1	0.0-0.45	PCI/G	0.822	0,034	0.905	9.32	2.14
94798	2086000		native 1	0.0-0.5	PCI/G	0.587	0.064	0.795	30.6	5.08
94898	2086149	***************************************	native 1	0.0-0.4	PCI/G	0.798	0.056	1.32	362	80.8
94998	2086298		native 1	0.0-0.5	PCI/G	0.997	0.085	1.31	162	36.7
95098	2086447	***************************************	native 1	0.0-0.5	PCI/G	1	-0.012	0.993	18.8	3.34
95198	2086149	749188	native 1	0.0-0.5	PCI/G	3.28	0.122	8,66	3300	880
95298	2086066		native 1	0.0-0.5	PCI/G	0.78	0.062	0.827	10.6	1.96
95398	2086211	749120	native 1	0.0-0.5	PCI/G	1.94	0.188	6.34	978	182
95498	2086078	748987	native 1	0.0-0.45	PCI/G	0.772	0.022	1.01	49.8	8.51
95598	2086229	748984	native 1	0.0-0.5	PCI/G	1.14	0.055	2.74	858	176
95698	2086077	749248	native 1	0.0-0.5	PCI/G	0.765	0.046	1.54	135	26.9
95798	2086148	749268	native 1	0.0-0.5	PCI/G	0.911	0.049	0.962	40.3	6.69
95898	2086219	749244	native 1	0.0-0.5	PCI/G	0.94	0.056	1.3	27.3	5.03
97398	2086096	748827	native 1	0.0-0.5	PCI/G	0.884	0.116	0.917	278	45
97498	2086182	748770	native 1	0.0-0.45	PCI/G	0.762	0.004	1.14	82.7	11.6
97598	2086247	748845	native 1	0.0-0.5	PCI/G	1.2	0.018	1.47	75.7	15.7
90098	2085611	749212	native 2	1.5-2.0	PCI/G	0.587	0.027	0.598	0.135	0.031
90198	2085686	***************************************	native 2	1.4-1.9	PCI/G	0.491	0.022	0.651	0.656	0.122
90298	2085761	749211	native 2	1.1-1.7	PCI/G	1.63	0.105	3,5	25	6.26
90398	2085835		native 2	1.3-1.8	PCI/G	0.565	0.011	0.594	0.403	0.306
90498	2085910		native 2	1.2-1.7	PCI/G	0.721	0.034	0.87	50.1	9.35
90598	2085610	**************	native 2	1.6-2.1	PCI/G	0.502	0.029	0.58	0.224	0.05
90698	2085685		native 2	1.5-2.1	PCI/G	0.383	0.018	0.394	12.3	1.89
90798	2085760	**************	native 2	1.5-2.0	PCI/G	0.36	0.02	0.397	6.22	0.917
90898	2085835		native 2	1.4-1.9	PCI/G	0.324	0.032	0.379	0.848	0.296
90998	2085910	***************************************	native 2	1.3-1.8	PCI/G	2.85	0.227	15.7	13.6	2.4
91098	2085610		native 2	1.9-2.4	PCI/G	0.914	0.056	0.967	21.7	3.93
91198	2085685	····	native 2	1.3-1.9	PCI/G	0.39	0.012	0.304	5.52	0.744
91298	2085760	\$11017 PRO COLUMN TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE TO THE T	native 2	1.5-2.0	PCI/G	0.284	0.007	0.319	1.49	0.229
91398	2085834	***************************************	native 2 native 2	1.3-1.8	PCI/G	0.436	0.065	0.721	201	10.3
91498	2085909			1.3-1.8	PCI/G	0.723	0.045	2.35	9.1 167	1.69
91598 91698	2085610 2085684	******************************	native 2 native 2	2.0-2.5	PCI/G PCI/G	0.977 1.45	0.137 0.252	1.12 1.89	167 0.937	33.2 7.05
91698			native 2	1.4-1.9 1.6-2.0	PCI/G PCI/G	0.537	0.252 0.046	0.771	0.937 5.98	7.0t 1.0t
91798	2085759		native 2	1.6-2.1	PCI/G PCI/G	1.65	0.046	1.38	212	29.2
91998	2085909	b	native 2	1.4-1.9	PCI/G	1.65	6.57	8.51	1480	29.2 256
92098	2085609		native 2	1.4-1.9	PCI/G	0.904	0.022	0.72	0.381	0.172
92198	2085684		native 2	1.2-1.7	PCI/G	0.904	0.022	0.824	0.16	0.172
92298	2085760	*******************	native 2	1.6-2.0	PCI/G	0.963	0.043	0.996	1.79	0.18
92398	2085834	\$	native 2	1.8-2.3	PCI/G	0.652	0.039	0.69	2.93	0.59
92498	2085909	}~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	native 2	1.6-2.1	PCI/G	0.56	0.045	0.54	0.408	0.05
92598	2085560	}	native 2	0.2-1.0	PCI/G	0.726	0.03	0.832		2.64
92698	2085551	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	native 2	0.4-0.9	PCI/G	0.442	0.022	0.516	1.22	0.34
92798	2085553		native 2	0.4-0.9	PCI/G	0.621	0.011	0.694		0.049
92898	2085703	***************************************	native 2	1.0-1.5	PCI/G	0.926	0.051	0.972	0.932	0.17
92998	2085853	\$	native 2	0.5-1.0	PCI/G	0.607	0.014	0.551	5.76	1.
93098		······	native 2	0.5-1.0	PCI/G	0.961	0.066	0.877	6.1	1.3
93198		»	native 2	0.5-1.0	PCI/G	0.941	0.028	1.29	62.8	9.88
93298	Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction of the Contraction o		native 2	0.5-1.0	PCI/G	0.825	-0.007	0.854	~~~~~~~~~~~~ <u>~~~~~~~~~~~~~~~~~~~~~~~~~</u>	0.114
93398	***************************************	§	native 2	0.5-1.0	PCI/G	1.27	0.046	1.25		0.45

						11 223/234	11 225	11 220	Pu 220/240	Am 24:
Borehole	FASTING	NORTHING	Material	Interval(ft)	unit code	U-233/234 pCi/g	U-235 pCi/g	U-238 pCi/g	239/240 pCi/g	Am-24
93498	2086198		native 2	0.5-1.0	PCI/G	0.694	0.066	рсид 1.09	<del> ,</del>	pCi/g
93598	2085978	£	native 2	0.4-0.8	PCI/G		~~~	ommercian accessis and a second	9.01	1.0
93698	2086153	\$	native 2			0.499	0.015	0.522	9.34	1.
93798	2086300	***********	native 2	0.5-1.0	PCI/G PCI/G	0.511	0.032	0.764	49.5	9.
93898	2086406	§	******************************	0.45-0.9		0.413	0.033	0.369	4.12	0.9
on a commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence	************		native 2	0.5-1.0	PCI/G	0.915	0.035	1.15	34.6	5.
93998	2086000	j	native 2	0.5-1.0	PCI/G	0.492	0.029	0.541	4.64	0.6
94098	2086128		native 2	0.4-0.8	PCI/G	0.679	0.051	0.988	28.6	4.
94198	2086298	b	native 2	0.4-0.8	PCI/G	0.569	0.028	0.545	13.9	2.
94298	2086438		native 2	0.5-1.0	PCI/G	0.862	0.049	0.911	25.4	2.
94398	2085550		native 2	0.3-0.7	PCI/G	0.74	0.014	0.565	0.149	0.0
94498	2085552		native 2	0.3-0.8	PCI/G	0.876	0.061	0.729	1.26	0.3
94598	2085703	749265	native 2	0.5-1.0	PCI/G	0.918	0.038	1.03	11.4	2.
94698	2085852	749265	native 2	0.45-0.9	PCI/G	0.662	0.072	0.811	23.3	3
94798	2086000	749266	native 2	0.5-1.0	PCI/G	0.725	0.066	0.883	27	4.
94898	2086149	749243	native 2	0.4-0.8	PCI/G	1.07	0.074	2.3	785	2
94998	2086298	749244	native 2	0.5-1.0	PCI/G	1.19	0.023	1.5	192	4,
95098	2086447	749243	native 2	0.5-1.0	PCI/G	0.725	0.002	0.875	0.814	0.0
95198	2086149	749188	native 2	0.5-1.0	PCI/G	2.05	0.153	6.79	1820	4
95298	2086066		native 2	0.5-1.0	PCI/G	0.855	0.077	1.06	37.6	8
95398	2086211	***************************************	native 2	0.5-1.0	PCI/G	1.63	0.087	5.07	683	1
95498	2086078		native 2	0.45-0.9	PCI/G	1.2	0.047	2.97	669	1
95598	2086229		native 2	0.5-1.0	PCI/G	0.905	0.047	1.24	412	8
95698	2086077	[	native 2	0.5-1.0	PCI/G PCI/G	0.905	0.029	0.397	1.9	0.3
		· · · · · · · · · · · · · · · · · · ·	***************************************	****************	~{~~~~~~~~~			~~~~~~~~~ <del>~~~</del>	***************************************	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
95798	2086148		native 2	0.5-1.0	PCI/G	1.18	0.108	1.2	3.98	0.7
95898	2086219	· · · · · · · · · · · · · · · · · · ·	native 2	0.5-1.0	PCI/G	0.905	0.049	0.896	15.8	3
97398	2086096		native 2	0.5-1.0	PCI/G	0.933	0.063	1.06	4.5	0
97498	2086182		native 2	0.45-0.9	PCI/G	1.09	0.127	1.01	0.489	0.0
97598	2086247		native 2	0.5-1.0	PCI/G	0.9	0.118	1.87	389	7
90098	2085611	749212	native 3	2.0-2.5	PCI/G	0.746	0.026	0.853	0.006	-0.0
90198	2085686	749214	native 3	1.9-2.4	PCI/G	0.444	0.05	0.567	0.081	0.0
90298	2085761	749211	native 3	1.7-2.4	PCI/G	1.68	0.1	4	3.23	0.5
90398	2085835	749215	native 3	1.8-2.3	PCI/G	0.393	0.026	0.456	0.044	0.0
90498	2085910	749216	native 3	1.7-2.2	PCI/G	0.38	0.017	0.373	0.482	0.1
90598	2085610	749137	native 3	2.1-2.6	PCI/G	0.485	0.008	0.557	0.379	0.0
90698	2085685	749139	native 3	2.1-2.8	PCI/G	0.507	0.029	0.526	0.227	0
90798	2085760	749137	native 3	2.0-2.5	PCI/G	0.364	0.021	0.456	0.202	0.1
90898	2085835		native 3	1.9-2.4	PCI/G	0.501	0.028	0.492	0.032	0.0
90998	2085910		native 3	1.8-2.3	PCI/G	3.12	0.274	9.1	48.4	9
91098	2085610	\$	native 3	2.4-2.9	PCI/G	1.15	0.059	1.32	14.4	2
91198	2085685	······	native 3	1.9-2.5	PCI/G	0.263	0.022	0.368	0.934	0.0
91298	2085760		native 3	2.0-2.6	PCI/G	0.495	0.022	0.524	0.067	0.3
91398	2085834		native 3	. 20 00 00 00 00 00 00 00 00 00 00 00 00	~\$~~~~~~~~~	0.493	aaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa	0.324	0.007	0.2
				1.8-2.3	PCI/G		0.013			~~~~~~~
91498	2085909	***************************************	native 3	1.8-2.3	PCI/G	0.31	0.007	0.367	0.327	0.
91598	2085610		native 3	2.5-3.0	PCI/G	0.472	0.028	0.546	12.2	1
91698	2085684		native 3	1.9-2.4	PCI/G	0.645	0.031	0.745	0.292	0.0
91798	2085759		native 3	2.0-2.4	PCI/G	0.38	0.023	0.516	5.13	contractor con
91898	2085834		native 3	2.1-2.6	PCI/G	0.554	0.076	0.577	29.9	······································
91998	2085909		native 3	1.9-2.4	PCI/G	0.659	0.066	0.625	3.39	0.6
92098	2085609	*************	native 3	1.9-2.4	PCI/G	0.352	0.358	0.358	0.206	0.
92198	2085684	§	native 3	1.7-2.2	PCI/G	0.01	0.017	0.1	0.15	0.0
92298	2085760	b	native 3	2.0-2.3	PCI/G	1.06	0.043	1.22	0.023	0.0
92398	2085834	748915	native 3	2.3-2.8	PCI/G	0,489	0.033	0.396	0.433	0
92498	2085909	748915	native 3	2.1-2.6	PCI/G	0.27	0.05	0.29	0.059	0.1
92598	2085560	749064	native 3	1.0-1.5	PCI/G	0.806	0.038	0.888	0.936	0.1
92698	2085551		native 3	0.9-1.4	PCI/G	0.946	0.041	0.786	0.071	0.
92798	2085553	***************************************	native 3	0.9-1.4	PCI/G	0.354	0.013	0.458	0.09	C
92898	2085703	<u> </u>	native 3	1.5-2.0	PCI/G	0.769	0.039	0.77	0.137	0.0
92998	2085853		native 3	1.0-1.5	PCI/G	0.766	0.023	0.896	1.75	0.2
93098	2086005		native 3	1.0-1.5	PCI/G	1.02	0.020	0.76	11.8	2
93198	2086167	L	native 3	1.0-1.5	PCI/G	0.934	0.055	0.70	28	4
	····			&	·d·····				~~~~~~ <u>~</u>	
93298	2085755		native 3	1.0-1.5	PCI/G	0.706	0.018	0.776	0.322	-0.0
93398	2085857	\$	native 3	1.0-1.5	PCI/G	1.2	0.07	1.14	5.46	0.1
93498	2086198	\$	native 3	1.0-1.5	PCI/G	0.823	0.064	1.15	5.55	
93598	2085978		native 3	0.8-1.2	PCI/G	0.556	0.003	0.632	3.64	0.4
93698	2086153		native 3	1.0-1.5	PCI/G	0.372	0.012	0.401	54.1	8
93798	2086300	748976	native 3	0.9-1.35	PCI/G	0,367	0.04	0,308	0.154	0.0
93898	2086406	749003	native 3	1.0-1.5	PCI/G	0.761	0.049	0.776	17.4	3

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Borehole	EASTING	NORTHING	Material	Interval/ft)	unit_code	U-233/234 pCi/g	U-235	U-238	239/240	Am-241
93998	2086000		native 3	Interval(ft) 1.0-1.5	PCI/G	0.544	pCi/g 0.042	pCi/g 0.655	pCi/g 0.058	pCi/g 0.0
94098	2086128	\$	native 3	0.8-1.2	PCI/G	0.671	0.042	0.769	19.2	2.
94198	2086298	\$	native 3	0.8-1.2	PCI/G	0.316	0.030	0.703	0.346	0.0
94298	2086438	}a	native 3	1.0-1.5	PCI/G	0.696	0.05	0.738	0.278	0.1
94398	2085550	\	native 3	0.7-1.1	PCI/G	0.677	0.042	0.713	0.257	0.0
94498	2085552		native 3	0.8-1.3	PCI/G	0.423	0.025	0.468	0.058	0.0
94598	2085703		native 3	1.0-1.5	PCI/G	0.636	0.025	0.567	1.04	0.1
94698	2085852		native 3	0.9-1.35	PCI/G	0.568	0.04	0.617	2.1	0.4
94798	2086000	749266	native 3	1.0-1.5	PCI/G	0.588	0.037	0.512	0.521	0.2
94898	2086149	749243	native 3	0.8-1.2	PCI/G	1.48	0.124	3.12	247	54
94998	2086298		native 3	1.0-1.5	PCI/G	0.843	0.017	1.22	26.6	4.
95098	2086447	·	native 3	1.0-1.5	PCI/G	0.426	0.023	0.618	1.52	0.3
95198	2086149		native 3	1.0-1.5	PCI/G	1.29	0.138	2.71	115	2
95298	2086066		native 3	1.0-1.5	PCI/G	0.956	0.037	0.944	45.1	8.
95398	2086211	*************	native 3	1.0-1.5	PCI/G	0.841	0.062	1.19	46.5	8.
95498	2086078		native 3	0.9-1.35	PCI/G	0.827	0.063	1.76	156	29
95598	2086229	****************************	native 3	1.0-1.5	PCI/G	0.489	0.015	0.572	38.1	5.
95698	2086077		native 3	1.0-1.5	PCI/G	0.544	0.009	0.622	10.7	2.
95798 95898	2086148		native 3	1.0-1.5	PCI/G	0.562	-0.013	1.02	1.34	0.2
95898 97398	2086219 2086096		native 3 native 3	1.0-1.5	PCI/G	0.805	0.003	0.751	11.4	2.
	*****	***************************************	}	1.0-1.5	PCI/G	0.818	0.063	0.892	0.423	0.1
97498 97598	2086182		native 3	0.9-1.35 1.0-1.5	PCI/G PCI/G	0.905 1.01	0.082	1.21	0.265	0.0
90098	2086247 2085611	************	native 3 native 4	\$~~~~~~~~~	··· · · · · · · · · · · · · · · · · ·		-0.007	1.23	33.2 0.016	
90198	2085686		****	2.5-3.0 2.4-2.9	PCI/G PCI/G	0.592 0.76	0.041 0.051	0.515 0.841	0.016	-0.0
90298	2085761	************	native 4 native 4	S	PCI/G PCI/G	0.76		0.633	0.747	0.0 .0
90398	2085835		native 4	2.4-3.0 2.3-2.8	PCI/G	0.629	0.048 0.042	0.604	0.085	0.
90498	2085910	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	native 4	2.2-2.7	PCI/G	0.829	0.042	0.804	0.046	******************
90598	2085610		native 4	<b>6</b>	PCI/G				0.784	0.
90798	2085760	**********	· · · · · · · · · · · · · · · · · · ·	2.6-3.1	PCI/G	0.408 0.311	0.026 0.014	0.486 0.334	2.65	0.0
90898	2085835		native 4 native 4	2.5-3.1	PCI/G		0.014		0.029	0.0
90998	2085910	***************************************	native 4	2.4-2.9 2.3-2.8	PCI/G	0.499	0.082	0.459 1.24	3.7	0.0
91098	2085610		native 4	ģ	PCI/G	0.815 0.462	0.082	0.439	5.5	0. <i>7</i> 1.
91198	2085685		native 4	2.9-3.4 2.5-3.1	PCI/G	0.462	0.012	0.403	0.659	0.1
91398	2085834		native 4	2.3-2.8	PCI/G	0.408	0.014	0.403	0.56	0.1
91498	2085909	******************************	native 4	2.3-2.8	PCI/G	0.403	0.023	0.52	0.09	0.0
91598	2085610		native 4	3.0-3.5	PCI/G	0.27	0.022	0.187	17.6	3.
91698	2085684	**********	native 4	2.4-2.9	PCI/G	0.908	0.039	0.791	0.697	0.1
91898	2085834		native 4	2.6-3.1	PCI/G	0.357	0.035	0.39	1.08	0.2
91998	2085909		native 4	2.4-2.9	PCI/G	0.34	0.021	0.411	1.9	0.
92098	2085609		native 4	2.4-2.9	PCI/G	0.362	0.018	0.493	0.087	0.2
92198	2085684		native 4	2.2-2.7	PCI/G	0.558	0.012	0.58	0.036	0.0
92398	2085834		native 4	2.8-3.3	PCI/G	0.455	0.016	0.452	0.119	0.0
92498	2085909	harmon and the second second	native 4	2.6-3.1	PCI/G	0.422	0.042	0.502	0.034	0.0
92598	2085560		native 4	1,5-2.0	PCI/G	0.586	0.023	0.543	0.84	0.1
92698	2085551	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	native 4	1.4-1.9	PCI/G	0.895	0.014	0.857	0.17	0.
92798	2085553		native 4	1.4-1.9	PCI/G	0.355	0.016	0.393	0.058	0.0
92898	2085703		native 4	2.0-2.4	PCI/G	0.642	0.051	0.626	0.071	0.0
92998	2085853		native 4	1.5-2.0	PCI/G	0.684	0.027	0.647	4.33	0.8
93098	2086005	748817	native 4	1.5-2.0	PCI/G	0.773	0	0.645	2.33	0.3
93198	2086167	748839	native 4	1.5-2.0	PCI/G	0,826	0.032	1.06	35.6	5.
93298	2085755	748671	native 4	1.5-2.0	PCI/G	0,595	0.034	0.626	0.135	-0.0
93398	2085857	***************************************	native 4	1.5-2.0	PCI/G	1.32	0.102	1.13	0.073	-0.0
93498	2086198	\$	native 4	1.5-2.0	PCI/G	0.943	0.003	1.08	1.24	0.0
93598	2085978	Anna ann ann ann ann ann an ann ann ann	native 4	1.2-1.4	PCI/G	0.456	0.029	0.477	2.83	0.3
93698	2086153		native 4	1.5-2.0	PCI/G	0,334	0.015	0.343	1.72	0.3
93798	2086300		native 4	1.35-1.8	PCI/G	0.371	0.025	0.311	1.03	0.3
93898	2086406	<b></b>	native 4	1.5-2.0	PCI/G	0.385	0.033	0.576	14.3	2
93998	2086000		native 4	1.5-2.0	PCI/G	0.637	0.014	0,548	0.037	0.3
94098	2086128	\$	native 4	1.2-1.5	PCI/G	0.522	-0.047	1.11	54	5
94198	2086298		native 4	1.2-1.6	PCI/G	0.464	0.017	0.36	2.86	0.2
94298	2086438	\$	native 4	1.5-2.0	PCI/G	0,686	0.034	0.773	0.471	0.0
94398	2085550		native 4	1.1-1.4	PCI/G	0.668	0.032	0.702	0.267	0.0
94498	2085552	\$ 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to 100 to	native 4	1.3-1.8	PCI/G	0.37	0.047	0.449	0.014	0.0
94598	2085703	Barrer Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Commence Comme	native 4	1.5-2.0	PCI/G	0.802	0.043	0.813	0.081	0.0
94698	2085852	749265	native 4	1.35-1.8	PCI/G	0.651	0.055	0.878	5.62	1.
94798	2086000	749266	native 4	1.5-2.0	PCI/G	0.483	0.016	0.611	0.121	0.0

Borehole	EASTING	NORTHING	Material	Interval(ft)	unit code	U-233/234 pCi/g	U-235 pCi/q	U-238 pCi/q	Pu 239/240 pCi/a	Am-241 pCi/g
94898	2086149		native 4	1.2-1.7	PCI/G	0.946	0.079	ρο#g 1.97	34.5	7.63
94998	***************************************		native 4	1.5-2.0	PCI/G	0.491	0.079	***************************************	34.5 6.95	1.33
95098	2086447	749243	native 4	1.5-2.0	PCI/G	0.652	0.062	0.664	0.57	0.152
95198	2086149	749188	native 4	1.5-2.0	PCI/G	0.523	0.031	0.716	5.32	0.969
95298	2086066	749123	native 4	1.5-2.0	PCI/G	0.562	0.023	0.595	1.31	0.238
95398	2086211	749120	native 4	1.5-2.0	PCI/G	0.713	0.032	0.813	34.5	6.66
95498	2086078	748987	native 4	1.35-1.75	PCI/G	0.52	0.034	0.593	12.3	2.26
95598	2086229	748984	native 4	1.5-2.0	PCI/G	0.359	-0.011	0.265	1.37	0.272
95698	2086077	749248	native 4	1.5-2.0	PCI/G	0.477	0.017	0.505	4.49	1.06
95798	2086148	749268	native 4	1.5-2.0	PCI/G	0.654	0.017	0.792	0.816	0.13
95898	2086219	749244	native 4	1.5-2.0	PCI/G	0.538	0.041	0.552	20,1	4.46
97398	2086096	748827	native 4	1.5-2.0	PCI/G	0.76	0.044	0.917	0.549	0.169
97498	2086182	748770	native 4	1.35-1.8	PCI/G	0.617	0.04	0.559	0	0.032
97598	2086247	748845	native 4	1.5-2.0	PCI/G	0.978	0.077	0.89	0.913	0.194

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Sample	···		lab_result_ qualifier	1,1,1,2- TETRACHLOROETHANE	1,1,1- TRICHLOROETHANE	1,1,2,2- TETRACHLOROETHANE	1,1,2- TRICHLOROETHAN E	1,1,2- Trichlorotrifluoroethane
Borehole Interval	Material	RIN/Event/Bottle	sapoo	(ug/kg)	(ug/kg)	(ug/kg)	(ng/kg)	(ug/kg)
90998 3.8-4.0	native	98A2015-001.010		15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				
91198 11.6-11.9	native	98A1091-001.035						
91198 15.5-15.8	native	98A1091-001.036						
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96898 8.4-8.7	Material	FIN/Event/Bottle 99A6307-002.002	Spoo	(Sy/Sn)	(Sy/Sp)	(By/Bn)	(ng/kg)	(ug/kg)
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Sample Interval	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	1,1,1,2- TETRACHLOROETHANE (ua/ka)	1.1.1- TRICHLOROETHANE (ug/kg)	1,1,2,2- TETRACHLOROETHANE (ua/kg)	1,1,2- TRICHLOROETHAN E (ua/ka)	1.1.2- Trichlorotrifluoroethane (uofka)
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97698 16.3-16.7	native	99A8275-005.002	Щ		in direction accountant and the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the		OO COO COO COO COO COO COO COO COO COO	TO THE THE THE THE THE THE THE THE THE THE
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95998 12.4-12.8	native	99A7799-003.002	J	**************************************	ACCUSTO AND AND AND AND AND AND AND AND AND AND			
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1,1,1,2- TETRACHLOROETHANE (ug/kg)							-		***************************************	TO THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF TH	SCS TOCOGOGO C. 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RIN/Event/Bottle			98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	99A6817-006.002	99A6649-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	99A6307-001.002	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-004.003		T	99A8275-009.002	98A2015-001.010	98A1091-001.035	98A1091-001.036	98A1091-001.037	98A1091-001.038	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	98A1092-001.033	98A1092-001.034	99A7799-003.002	99A7799-004.002	99A7799-005.002	99A7799-006.002	99A7799-001.002
Material	native	native	native	native	native	bedrock	bedrock	native	native	native	native	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	bedrock	native	bedrock	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native
Sample Interval	91198 11.6-11.9	91198 15.5-15.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 16.5-17.0	97298 16.4-17.0	97298 17.7-18.2	97698 19.4-19.8	90998 3.8-4.0	91198 11.6-11.9	91198 15.5-15.8	91198 19.1-19.5	91198 19.5-19.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	92598 3.5-4.0	92598 7.5-8.0	95998 12.4-12.8	95998 14.8-15.2	95998 17.7-18.2	95998 24.6-25.0	95998 5.0-5.6
Borehole	91198	91198	91198	91198	92298	92598	96598	86996	86996	86996	96798	96798	96798	96798	96798	96896	96898	96898	96898	86696	86696	96698	86696	95026	97298	97298	97698	86606	91198	91198	91198	91198	91198	91198	92598	92598	92598	92598	95998	95998	95998	96656	95998

ETHAN 1,1,2- Trichlorotrifluoroethane	5.2	002	700	730	00.2	060	ng/	, , ,	200	670	750	720	700	670	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
1,1,2- TRICHLOROETHAN E		PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF THE PRINCE OF 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1,1,2,2- TETRACHLOROETHANE (unka)	(B) (B)	200	002	08.7	COS	092	00/	700	700	670	750	720	7007	670	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
1,1,1- TRICHLOROETHANE (110/kg)		002	002	730	000	080	ρο,	200	700	670	750	720	200	670	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	2.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
1,1,1,2- TETRACHLOROETHANE (uo/ka)	(8),8)		002	730	009	080	00/	, 700	700	670	750	720	700	670	710	730	2007	710	MATERIAL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTROL CONTR		A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O				5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	2.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
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1,1,2,2- TETRACHLOROETHANE (uofka)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,1,1- TRICHLOROETHANE (uolks)	5.2	5.6	5.7	5.3	5.2		5.7					670	700	002	920	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,1,1,2- TETRACHLOROETHANE, (norko)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
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RIN/Event/Roffle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
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Sample Brownle Interval	8.4	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0		97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8		97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6		97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6

Sample			lab_result_ qualifier_	1,1- DICHLOROETHANE	DICHL	1,1- DICHLOROPROPEN E	ENZENE	1,2,3- TRICHLOROPROPANE
Borehole Interval	Material	RIN/Event/Bottle	codes	(ug/kg)	(ng/kg)	(ug/kg)	(ug/kg	(ng/kg)
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91198 15.5-15.8	native	98A1091-001.036						
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96798 12.5-12.9	native	99A6650-003.002	***************************************	· · · · · · · · · · · · · · · · · · ·				***************************************
96798 16.0-16.4	native	99A6650-004.002	SOMEON AND PROPERTY OF STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET,				agenerate (Associate and associate  (), (**********************************	
96798 20.4-20.8	native	99A6650-005.002						***************************************
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Sample Borehole Interval	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	1,1- DICHLOROETHANE (ug/kg)	1,1- DICHLOROETHANE DICHLOROETHENE (ug/kg) (ug/kg)	DICHLOROPROPEN E (ug/kg)	1,2,3- TRICHLOROBENZENE (ug/kg	1,2,3- TRICHLOROPROPANE (ug/kg)
96898 8.4-8.7	native	99A6307-002.002						
96998 4.4-4.8	native	99A6824-001.002				The second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the second statement of the se	A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O	TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TANKA TA
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97198 20.4-20.8	native	99A4102-002.015			**************************************			
97198 24.4-24.8	bedrock	99A4102-002.018			***************************************			
97298 12.4-12.8	native	99A6825-003.002			-			AMERICAN AND AND AND AND AND AND AND AND AND A
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97298 4.0-4.4		99A6825-001.002			A. C. C. C. C. C. C. C. C. C. C. C. C. C.	***************************************		WWW.WWW.WWW.WW.WW.WW.WW.WW.WW.WW.WW.WW.
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Sample			lab_result_ qualifier_	1,1- DICHLOROETHANE	1,1- DICHLOROETHENE	1,1- DICHLOROPROPEN E	1,2,3- TRICHLOROBENZENE	1,2,3- TRICHLOROPROPANE
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96098 16.0-16.2	bedrock	99A3210-002.016	n	700	700	700		700
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96398 12.4-12.7	native	99A4102-001.009	n	710	710	710	710	710
96398 16.2-16.4	bedrock	99A4102-001.012	n	730	730	730	730	730
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96598 18.6-18.9	native	99A6817-005.002	n	5.3				5.3
96598 22.3-22.7	bedrock	99A6817-006.002	Ω	6.2		6.2	6.2	6.2
96598 4.2-4.6	native	99A6817-001.002	n	5.7				5.7
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96698 17.7-18.3	native	99A7930-001.002	Ω	5.6		5.6	5.6	5.6
96698 20.2-20.6	native	99A7930-002.002	Ω	5.4				5.4
96698 22.4-22.8	bedrock	99A7930-003.002	Ω	6.4			***************************************	6.4
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96698 8.2-8.6	native	99A6649-002.002	n	5.6		5.6	5.6	5.6
96798 12.5-12.9	native	99A6650-003.002	Ω	6.2			######################################	6.2
96798 16.0-16.4	native	99A6650-004.002	n	7.2		7.2	THE THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPER	7.2
96798 20.4-20.8	native	99A6650-005.002	n	7.4		7.4	7.4	7.4
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96798 8.4-8.8	native	99A6650-002.002	n	6.3				6.3
96898 12.3-12.6	native	99A6307-003.002	n	6.4	***************************************	6.4	0.000000000000000000000000000000000000	6.4
96898 17.1-17.4	bedrock	99A6307-004.002	n	5.3		5.3	5.3	5.3
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1,2,3- TRICHLOROBENZENE (ug/kg	5.2	5.6	5.7	5.3	5.2	5.1	. 5.7	5.5	5.8	650	740	670	002	200	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,1- DICHLOROPROPEN E (ug/kg)	5.2	vite (Alvalana valana vana vapapana vana manamanta (Altalania) (Vite (Al	5.7		5.2	5.1		***************************************				670						6.1	5.4		5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,1- DICHLOROETHANE DICHLOROETHENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1						670		200		5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,1- DICHLOROETHANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	920	740	670	200	200	029	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
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RIN/Event/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native		native	native	_	native	native	native		bedrock		native							
Sample	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	86896	86696	86696	86696	86696	97098	97098	86026	95026	97198	97198	97198	97198	97198	97198	97298	97298	97298	97298	97298	97698	97698	97698	97698	97698	97698	97698

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Sample			lab_result_ qualifier_	1,2,4- TRICHLOROBENZENE	TRIMETHYLBENZEN	1,2-CIS- DICHLOROETHYLENE	1,2-DIBROMO-3- CHLOROPROPANE	1,2- DIBROMOETHAN E	1,2- Dichlorobenzene
Borehole Interval	Material	RIN/Event/Bottle	səpoo	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ng/kg)
90998 3.8-4.0	native	98AZ015-001.010			7.0				
91198 11.6-11.9	native	98A1091-001.035							
91198 15.5-15.8	native	98A1091-001.036	24200000						
91198 19.1-19.5	native	98A1091-001.037						O TATALON CONTROL OF THE PARTY AND AND AND AND AND AND AND AND AND AND	000000000000000000000000000000000000000
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Interview   9946275-004.002   E		$\dashv$	RIN/Event/Bottle	səpoo	(ug/kg)	(ng/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
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1,2- DIBROMOETHAN E (ua/ka)		002						7007	erico de como como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de como de		720	\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$		II desegrato que encono ses estados ses estados en estados en estados en estados en estados en estados en esta	730	700	710		-		10000000000000000000000000000000000000			5.4	9					5.9	ponomono contrata contrata de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de la ferial de l		***************************************	***************************************		***************************************	***************************************	5.3	6.3	6.4	5.3	5.2
1,2-DIBROMO-3- CHLOROPROPANE (ua/ka)		002	700	730	069	092	700	007	670	750	720	700	670	710	730	700	710	THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O	**************************************			A A A A A A A A A A A A A A A A A A A	\$0000000000000000000000000000000000000	5.4	9	5.3	6.2	5.7	5.3	5.9	0.0	4.0	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
1,2-CIS- DICHLOROETHYLENE (ua/ka)	5.2				\$2000 P. C. C. C. C. C. C. C. C. C. C. C. C. C.		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s		\$0000000000000000000000000000000000000		**************************************					70. Lippe participation (1) 200 (200 (200 (200 (200 (200 (200 (200							***************************************	5.4	9	5.3	6.2	5.7	5.3	5.9	0.0	5.4 6.4	5.7	5.6			Polonomonomonomonomonomonomonomonomonomon	5.3	6.3	6.4	5.3	5.2
1,2,4- TRIMETHYLBENZEN E (ua/ka)		700	2007	730	069	092	, 700	007	929	750	720	700	029	710	730	200	710							5.4	9	5.3	6.2	5.7	5.3	5.9	0.5	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
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Material	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	nauvo	native	native	native	native	native	native	native	native	native	bedrock	native
Sample	8	96098 12.5-13.0	96098 16.0-16.2	96098 4.5-4.8	96098 8 5-8 8	96198 12.0-12.5		96198 4.4-4.7	96198 8,1-8.5	96298 12.25-12.75 native	96298 16.1-16.5	96298 4.3-4.7	96298 8.0-9.0	96398 12.4-12.7	96398 16.2-16.4	96398 4.3-4.8	96398 8.4-8.9	96498 13-13.5	96498 16.0-16.5	96498 18.0-18.6	96498 22.0-22.5	96498 4.8-5.2	96498 9.5-10.0	96598 11.6-12.0	96598 15.2-15.6	96598 18.6-18.9	96598 22.3-22.7	96598 4.2-4.6	96598 8.4-8.8	96698 12.4-12.8	0000000	96696 20.2-20.6 96698 22 4-22 8	96698 4 2-4 6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4 4-4 7
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1,2- Dichlorobenzene (ug/kg)			**************************************	NAMES AND ASSOCIATION OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE 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1,2- DIBROMOETHAN E (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	7.5					670	700	2007	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,2-DIBROMO-3- CHLOROPROPANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,2-CIS- DICHLOROETHYLENE CHLOROPROPANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8					THE RELEASE AND A THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY		5.3	5.4	6.1	5.4	2.7						5.3	Contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction of the contraction o
1,2,4- TRIMETHYLBENZEN E (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	029	200	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
1,2,4- TRICHLOROBENZENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	700	650	5.3	5.4	6.1	5.4	2.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
lab_result_ qualifier_ codes	<u></u>	n	D	n	n	n	n	n	<b>D</b>	D	D	n	⊃	n	ח		n	D	D	D	n	D	n	Ω	n	n	D
RIN/Event/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	native
Sample	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	96896	696	8696	8696	8696	8026	026	026	160∠6	9719	9719≀	9719	9719	9719≀	9719≀	9729	9729	9729	9729	8226	∂926	8926	89∠6	8926	9769	9769	9769

BeANTSE-ON 100   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120   120	Sample Borehole Interval	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	1,2- DICHLOROETHANE (ug/kg)	1,2-Dichloroethane- d4 (ug/kg)	1,2- DICHLOROETHEN E(TOTAL) (ug/kg)	1,2- DICHLOROPROPANE (ug/kg)	1,2-TRANS- DICHLOROETHYLENE (ug/kg)	1,3,5- TRIMETHYLBENZENE (ug/kg)
native 98A1091-001 035  native 98A1091-001 036  bedrock 98A1091-001 038  native 98A1091-001 038  native 98A1091-001 038  native 98A1092-001 036  native 98A1092-001 036  native 98A1092-001 034  native 98A7799-006 002  native 98A7799-006 002  native 98A7799-006 002  native 98A7799-006 002  native 98A7799-001 018  native 98A3210-001 016  native 98A3210-001 018  native 98A3210-001 018  native 98A3210-001 018  native 98A3210-001 018  native 98A3210-001 018  native 98A3210-001 012  native 98A6817-005 002  bedrock 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6817-002 002  native 98A6810-001 002  native 98A6810-002 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002  native 98A680000 002	90998 3.8-4.0	native	98A2015-001.010							
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15.5-15.8		98A1091-001.036			118			\$\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarrow\rightarro	TO 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native   98A1091-001.033   native   98A1092-001.034   native   98A1092-001.035   native   98A1092-001.035   native   98A1092-001.035   native   98A1092-001.033   native   98A7092-001.033   native   99A7199-002.001   99A7799-006.002   native   99A7799-006.002   native   99A7799-006.002   native   99A7799-006.002   native   99A3210-001.015   native   99A3210-001.015   native   99A3210-001.015   native   99A3210-001.015   native   99A3210-001.015   native   99A3210-001.016   native   99A6817-002.002   native   99A6817-002.002   native   99A6817-002.002   native   99A6817-002.002   native   99A6849-003.002   native   99A6849-003.002   native   99A6849-003.002   native   99A6849-003.002   native   99A6849-003.002   native   99A6869-003.002   native   99A68907-003.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-004.002   native   99A68307-00	91198 19.5-19.8	**********	98A1091-001.038					**************************************	**************************************	0.000000000000000000000000000000000000
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native   9948824-001 002     native   9948824-002 002     native   9948824-002 002 015     native   9948625-003 002     native   9948625-003 002     native   9948625-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9841091-001 038     native   9841092-001 038     native   9841092-001 038     native   9841092-001 036     native   984275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   9948275-003 002     native   99	96898 8.4-8.7	native	99A6307-002.002			Verrore				
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Sample Borehole Interval	e Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	1,2- DICHLOROETHANE (ug/kg)	1,2-Dichloroethane- DICHLOROETHEN d4 E(TOTAL) (ug/kg) (ug/kg)	1,2- DICHLOROETHEN E(TOTAL) (ug/kg)	1,2- DICHLOROPROPANE (ug/kg)	1,2-TRANS- DICHLOROETHYLENE TRIMETHYLBENZENE (ug/kg) (ug/kg)	1,3,5- TRIMETHYLBENZENE (ug/kg)
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1,3,5- TRIMETHYLBENZENE (ug/kg)		AND THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPER	***************************************		***************************************		***************************************	elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektristik eta oleh elektrist	***************************************		***************************************	01.01.04.01.01.01.01.01.01.01.01.01.01.01.01.01.		2000 000 mm m m m m m m m m m m m m m m	***************************************																						***************************************						
1,2-TRANS- DICHLOROETHYLENE (ug/kg)	5.2			The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s					9,000,000,000,000,000,000,000,000,000,0		\$0000000000000000000000000000000000000					A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O								5.4	g	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	2.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
1,2- DICHLOROPROPANE (ug/kg)	5.2	700	2007	730	069	760	2007	200	029	750	720	700	670	710	730	200	710	2000 CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRA					1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
1,2- DICHLOROETHEN E(TOTAL) (ug/kg)			**************************************		***************************************	STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE	**************************************											1300	1300	1300	1500	1500	1300																				
1,2-Dichloroethane- d4 (ug/kg)			***************************************		***************************************	······································	\$5.000.000.000.000.000.000.000.000.000.0							Vanasa anninga e de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de cerce de c																													
1,2- DICHLOROETHANE (ug/kg)	5.2	700	700	730	069	760	. 700	200	670	750	720	200	029	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
lab_result_ qualifier_ codes	<b>-</b>	n	n	n	n	n	n	n	n	n	n	n	Π	n	n	n	n	n	n	n	n	n	n	n	n n	n	n	n	ם	n	n	n	n	n	n	n	n	n	<b>-</b>	n	n	⊃	D
RIN/Event/Bottle	99A7799-002.002	99A3210-002.015	99A3210-002.016	99A3210-002.013	99A3210-002.014	99A3210-003.015	99A3210-003.016	99A3210-003.013	99A3210-003.014	99A3210-004.016	99A3210-004.017	99A3210-004.013	99A3210-004.014	99A4102-001.009	99A4102-001.012	99A4102-001.003	99A4102-001.006	99A3210-001.015	99A3210-001.016	99A3210-001.017	99A3210-001.018	99A3210-001.013	99A3210-001.014	99A6817-003.002	99A6817-004.002	99A6817-005.002	99A6817-006.002	99A6817-001.002	99A6817-002.002	99A6649-003.002	99A7930-001.002	99A7930-002.002	99A7930-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	99A6307-001.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	natíve	bedrock	native	native	native	native	native	native	native	native	bedrock	native
Sample Interval	8.4-8.8	96098 12.5-13.0	96098 16.0-16.2	96098 4.5-4.8	96098 8.5-8.8	96198 12.0-12.5	96198 15.8-16.2	96198 4.4-4.7	96198 8.1-8.5	96298 12.25-12.75	96298 16.1-16.5	96298 4.3-4.7	96298 8.0-9.0	96398 12.4-12.7	96398 16.2-16.4	96398 4.3-4.8	96398 8.4-8.9	96498 13-13.5	96498 16.0-16.5	96498 18.0-18.6	96498 22.0-22.5	96498 4.8-5.2	96498 9.5-10.0	96598 11.6-12.0	96598 15.2-15.6	96598 18.6-18.9	96598 22.3-22.7	96598 4.2-4.6	96598 8.4-8.8	96698 12.4-12.8	96698 17.7-18.3	96698 20.2-20.6	96698 22.4-22.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7
Borehole	92998	96098	96098	96098	96098	96198	96198	96198	96198	96298	96298	96298	96298	96398	96398	96398	96398	96498	96498	96498	96498	96498	96498	96598	96298	96298	96598	96598	96598	96998	86996	96998	86996	96998	96998	96798	96798	96798	96798	96798	96898	96898	96898

					1,3,5- IMETHYLBENZENE
ab_result_ qualifier DIC	1,2-DI DICHLOROETHANE	1,2-Dichloroethane- DICHLOROETHEN 64 E(TOTAL)	1,2- DICHLOROPROPANE	1,2- DICHLOROPROPANE DICHLOROETHYLENE TRIMETHYLBENZENE	
	(ug/kg)	(ug/kg) (ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
	5.2	Ø Salaron	5.2	5.2	5.2
	5.6		5.6	5.6	5.6
	5.7		5.7	5.7	5.7
	5.3		5.3	5.3	5.3
*********	5.2		5.2	5.2	5.2
	5.1		5.1	5.1	5.1
	5.7		5.7	5.7	5.7
	5.5		5.5	5.5	5.5
	5.8		5.8	5.8	5.8
	650		650		650
	740		740		740
	670		670		670
	700		700		002
	700		700		700
	650		650		650
	5.3		5.3	5.3	5.3
•	5.4		5.4	5.4	5.4
	6.1		6.1	6.1	6.1
	5.4		5,4	5.4	5.4
	5.7		5.7	5.7	5.7
	5.2		5.2	5.2	5.2
	5.4		5.4	5.4	5.4
	C L		5.3	5.3	5.3
	5.3		5.6	5.6	5.6
	5.6		5.7	5.7	5.7
	5.6 5.6 5.7			5.3	5.3
	5.3 5.3		ů. W.	;	CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR

		i,	lab_result_ qualifier_	1,3- DICHLOROBENZENE	1,3- DICHLOROPROPANE	1,4- DICHLOROBENZENE	2,2- DICHLOROPROPANE	2-BUTANONE
90998 3 8-4 0	Material	98A2015-001.010	cones	(By/Bn)	(Ry/Rn)	(dg/kg)	(ng/kg)	(ug/kg)
91198 11.6-11.9	native	98A1091-001.035						111 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST - 110 CAST -
91198 15.5-15.8	native	98A1091-001.036	***************************************		***************************************	***************************************		
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96498 4.8-5.2	native	99A3210-001.013						
96498 9.5-10.0	native	99A3210-001.014						
96598 11.6-12.0	native	99A6817-003.002						
96598 15.2-15.6	native	99A6817-004.002						
96598 18.6-18.9	native	99A6817-005.002						
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96698 12.4-12.8	native	99A6649-003.002						
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Borehole         Interval         Material           96898         8.4.8.7         native         96           96998         8.4.8.8         native         96           96998         8.4.8.8         native         96           97198         20.4-20.8         native         96           97298         12.4-12.8         native         96           97298         17.7-18.2         bedrock         96           97298         17.7-18.2         bedrock         96           97298         17.7-18.2         bedrock         96           97298         17.7-18.2         bedrock         96           97698         13.5-13.9         native         96           97698         13.5-13.9         native         96           97698         12.4-18.8         native         96           97698         12.5-18.         native         96           97698         1.6-5.8         native         98           91198         1.6-15.5         native         98           91198         1.5-19.5         native         98           91198         1.7-19.5         native         98           92598	RIN/Event/Bottle 99A6307-002.002 99A6324-001.002 99A6224-002.002 99A6102-002.018 99A6825-003.002 99A6825-001.002 99A6825-001.002 99A8275-004.002 99A8275-004.002 99A8275-003.002	Sopoo	(ug/kg)	DICTION OF A CHARLE		DICT CROPROPANE	z-BUTANONE (ug/kg)
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Sample			lab_result_	1,3- DICHLOROBENZENE	1,3- DICHLOROPROPANE	1,4- DICHLOROBENZENE	2,2- DICHLOROPROPANE	2-BUTANONE
Borehole Interval	Material	RIN/Event/Bottle	sapoo	(ug/kg)	(ug/kg)	(ng/kg)	(ug/kg)	(ug/kg)
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96098 12.5-13.0	native	99A3210-002.015	) )	002	200	002	700	700
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96498 22.0-22.5	bedrock	99A3210-001.018	<b>_</b>					1500
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96598 15.2-15.6	native	99A6817-004.002	<b>)</b>		9		9	120
96598 18.6-18.9	native	99A6817-005.002	D		5.3		5.3	106
96598 22.3-22.7	bedrock	99A6817-006.002	<b>-</b>		6.2		6.2	125
96598 4.2-4.6	native	99A6817-001.002	D		5.7		5.7	114
96598 8.4-8.8	native	99A6817-002.002	⊃		5.3		5.3	105
96698 12.4-12.8	native	99A6649-003.002	D		5.9		5.9	118
96698 17.7-18.3	native	99A7930-001.002	)		5.6		5.6	111
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96798 16.0-16.4	native	99A6650-004.002	D		7.2		7.2	144
96798 20.4-20.8	native	99A6650-005.002	D		7.4		7.4	149
96798 4.4-4.8	native	99A6650-001.002	n		5.3		5.3	106
96798 8.4-8.8	native	99A6650-002.002	n		6.3		6.3	126
96898 12.3-12.6	native	99A6307-003.002	<b>-</b>		6.4		6.4	128
96898 17.1-17.4	bedrock	99A6307-004.002	ם		5.3		5.3	105
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2-BUTANONE (ug/kg)			114			Account to the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	. 114		***************************************	650		670	***************************************	700		106			109	114	104		105	11	11	and an an an an an an an an an an an an an	105
2.2- DICHLOROPROPANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	920	740	670	700	200	950	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	53
1,4- DICHLOROBENZENE (ug/kg)		**************************************	NAMES OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE 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1,3- DICHLOROPROPANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	920	740	670	700	200	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	53
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Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	שליִלְבּר
Sample	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4,4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7		97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	æ.		97198 7.3-7.6	97298 12.4-12.8		97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8		97698 8 2-8 6
Borehole	96898	96998	96998	96698	86696	95026	95026	95026	95026	97198	97198	97198	97198	97198	97198	97298	97298	97298	97298	97298	97698	97698	97698	97698	97698	97698	97898

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Borehole Interval	Material	RIN/Event/Bottle	codes	(ng/kg)	(ug/kg)		(ug/kg)		(ug/kg)
90998 3.8-4.0	native	98A2015-001.010							
91198 11.6-11.9	native	98A1091-001.035							CCCCC Transportation of the Cocco
91198 15.5-15.8	native	98A1091-001.036		**************************************	***************************************	Quarter and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the second and the secon	ATT OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PRO		
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RIN/Event/Bottle	99A8275-004.002	99A8275-005.002	99A8275-008.002	98A2015-001.010	99A7799-003.002	-	99A7799-006.002		99A3210-003.013	99A4102-001.009	99A4102-001.012	99A4102-001.003	99A4102-001.006	99A3210-001.013	99A6817-003.002	99A6817-006.002	99A6817-002.002	99A6649-003.002	99A7930-001.002	99A7930-002.002	99A7930-003.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-002.002	99A6307-004.002	99Abo24-001.002	99A6824-002.002	99A6308-001.003	99A4102-002.009	99A4102-002.012	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-002.002
Material	native	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	bedrock	nalive	native	native	native	native	native	native	native	native	native	native	native	native	native	native	native
Sample Borehole Interval	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	90998 3.8-4.0	95998 12.4-12.8	95998 17.7-18.2	. 95998 24.6-25.0	95998 5.0-5.6	961984.4-4.7	96398 12.4-12.7	96398 16.2-16.4	96398 4.3-4.8	96398 8.4-8.9	96498 4.8-5.2	96598 11.6-12.0	96598 22.3-22.7	96598 8.4-8.8	96698 12.4-12.8	96698 17.7-18.3	96698 20.2-20.6	96698 22.4-22.8	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 8.4-8.8	96898 17.1-17.4	90990 4.4-4.0	96998 8.4-8.8	97090 4.2-4.1 07008 8 4.8 8	97198 12.4-12.8	97198 15.5-16.1	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 8.2-8.6

ACETONE (ug/kg)	440	009	1200	810		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	29.8	2.5	3.5	3.2	3	2.9	6.3	11	3.2	***************************************	***************************************	000000000000000000000000000000000000000		11.8	11.8	2.5	1.8		3.2	4.3		1600	***************************************		1300	1200			1400	1400	1300	1200	116	106	111	126	111
4-METHYL-2-PENTANONE (ug/kg)			***************************************				***************************************	000,000,000,000,000,000,000,000,000,00	Maria de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition de la composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della		***************************************	0.0000000000000000000000000000000000000																1600	1400	1400	1300	1200	1400	1400	1400	1400	1300	1200	58.1	53.2	55.6	63.3	55.6
4-ISOPROPYLTOLUENE (ug/kg)									***************************************	*	alemannen en en en en en en en en en en en en	. Octobro de production de la companie de la companie de la companie de la companie de la companie de la compa		A CONTRACTOR AND AND AND AND AND AND AND AND AND AND		region in the department of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of th									77			790	069	089	630	620	01/	680	700	720	650	610	5.8	5.3	5.6	6.3	5.6
4-CHLOROTOLUENE (ug/kg)				***************************************	***************************************		wommen and the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the contro	PO JATESTO DE LES CALLES CALLES CALLES AND AND AND AND AND AND AND AND AND AND	***************************************	***************************************	**************************************																	790	069	980	630	620	OL.	089	700	720	650	610	5.8	5.3	5.6		5.6
2-HEXANONE (ug/kg)					•				-																••••			1600	1400	1400	1300	1200	1400	1400	1400	1400	1300	1200	58.1	53.2	55.6	63.3	55.6
2-CHLOROTOLUENE (ug/kg)		Adjanuary Mathemate Handdom market and a site of a state of the state of the special property of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the 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lab_result_ qualifier_ codes	JB	JB	æ	ЭВ	JB	ЭВ	ac B	B	JB	JB	JB	JB	JB	9	ЭВ	JВ	JB	JB	ЭВ	JB	JB	д В	JB	ЭВ	ЭВ	JB	JB	_	n	o ii	n	o :	0	n	n	n	ם	n	D	<b>-</b>	<b>-</b>	⊃	_
RIN/Event/Bottle	98A1091-001.035	98A1091-001.036	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	99A6817-006.002	99A6649-003.002		99A6649-002.002	T		·			ľ																	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	98A1092-001.033	98A1092-001.034	99A7799-003.002	99A7799-004.002			99A7799-001.002
Material	native	native	native	native	native	bedrock	bedrock	native	native	native	native	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	bedrock	native	bedrock	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native
Sample	91198 11.6-11.9	91198 15.5-15.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 16.5-17.0	97298 16.4-17.0	97298 17.7-18.2	97698 19.4-19.8	90998 3.8-4.0	91198 11.6-11.9	91198 15.5-15.8	91198 19.1-19.5	91198 19.5-19.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	92598 3.5-4.0	92598 7.5-8.0	95998 12.4-12.8	95998 14.8-15.2	95998 17.7-18.2	95998 24.6-25.0	95998 5.0-5.6
Borehole	91198	91196	91196	91198	92596	92596	96598	36996	36996	96996	96798	96798	96798	96798	96798	96898	96898	96896	96896	96998	36696	36696	96998	97098	97298	97298	97698	B6606	91198	91198	91198	91198	91198	91198	92598	92598	92598	92598	96656	95998	95998	95998	95998

ACETONE (ug/kg)	103				**************************************	760	. 700	700	670	750	720	200	670			of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of th		1300	1300	1300	1500	1500	1300	108	120	106		114	105		111	108	128	government continues			***************************************				128	105	103
	51.5	700	2007	730	069	760	200	700	029	750	720	002	029	710	730	700	710	1300	1300	1300	1500	1500	1300	53.8	60.2	53.2	62.5	56.8	52.6	59.3	55.6	53.8	64.1	56.9	55.6	61.8	71.9	74.5	52.8	63.2	64.1	52.6	51.5
4-ISOPROPYLTOLUENE (ug/kg)	5.2	200	200	730	069	260	200	2007	0.29	750	720	200	929	710	730	200	710	Web 2000 100 100 100 100 100 100 100 100 10			**************************************			5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6,3	6.4	5.3	5.2
4-CHLOROTOLUENE (ug/kg)	5.2	700	200	730	069	760	002	200	929	750	720	200	920	710	730	700	710							5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	52
2-HEXANONE (ug/kg)	51.5	700	200	730	069	200	. 700	700	670	750	720	700	029	710	730	200	710	1300	1300	1300	1500	1500	1300	53.8	60.2	53.2	62.5	56.8		59.3	55.6	53.8	64.1	6.99	9.55	61.8	71.9	74.5	52.8	63.2	64.1	52.6	515
2-CHLOROTOLUENE (ug/kg)	5.2	700	700	730	069	760	700	700	929	<u>750</u>	720	700	670	710	730	200	710							5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
lab_result_ qualifier_ codes	<b>-</b>	n	n	Ω	n	0	n N	n	n	n	n	n	n	Ω	n	Ω	n	n	n	Ω	n	n	n	n	Ω	n	n	n	n	Ω	n	n	n	n	n	n	n	n	Ω	n	D.	<b>-</b>	_
RIN/Event/Bottle	99A7799-002.002	99A3210-002.015	99A3210-002.016	99A3210-002.013	99A3210-002.014	99A3210-003.015	99A3210-003.016	99A3210-003.013	99A3210-003.014	99A3210-004.016	99A3210-004.017	99A3210-004.013	99A3210-004.014	99A4102-001.009	99A4102-001.012	99A4102-001.003	99A4102-001,006	99A3210-001.015	99A3210-001.016	99A3210-001.017	99A3210-001.018	99A3210-001.013	99A3210-001.014	99A6817-003.002	99A6817-004.002	99A6817-005.002	99A6817-006.002	99A6817-001.002	99A6817-002.002	99A6649-003.002	99A7930-001.002	99A7930-002.002	99A7930-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	9946307-001 002
Material	native	native	bedrock	native	native	native	bedrock .	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	bedrock	Safiyo
Sample	95998 8.4-8.8	96098 12.5-13.0	96098 16.0-16.2	96098 4.5-4.8	96098 8.5-8.8	96198 12.0-12.5	96198 15.8-16.2	96198 4.4-4.7	96198 8.1-8.5	96298 12.25-12.75 native	96298 16.1-16.5	96298 4.3-4.7	96298 8.0-9.0	96398 12.4-12.7	96398 16.2-16.4	96398 4.3-4.8	96398 8.4-8.9	96498 13-13.5	96498 16.0-16.5	96498 18.0-18.6	96498 22.0-22.5	96498 4.8-5.2	96498 9.5-10.0	96598 11.6-12.0	96598 15.2-15.6	96598 18.6-18.9	96598 22.3-22.7	96598 4.2-4.6	96598 8.4-8.8	96698 12.4-12.8	96698 17.7-18.3	96698 20.2-20.6	96698 22.4-22.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	06808 / / / 7
Borehole	95998	36096	36096	36096	36096	96198	. 96198	96198	96198	96298	96298	96298	96298	36338	96398	96398	96398	96498	96498	96498	96498	96498	96498	96596	96598	96598	36296	36296	36296	36996	36996	36996	36996	36996	36996	96798	96798	96798	96798	36796	36896	36896	20890

ACETONE (ug/kg)	103	A CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR				102	114		116		***************************************	84000	700	***************************************	***************************************	106			109	114	***************************************	ather contrates and a second			***************************************	106	105
4-METHYL-2-PENTANONE AC. (ug/kg)	51.5	56.6	57.1	53.1	52.5	51	, 56.8	54.9	58.1	920	740	0.29	007	700	650	53.2	53.5	611	54.3	56.8	52.1	54.3	52.6	55.6	57.2	53.2	52.6
4-ISOPROPYLTOLUENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	099	740	670	200	002	029	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
4-CHLOROTOLUENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7		5.8	650	740	029	200	200	920	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
2-HEXANONE (ug/kg)	51.5	56.6	57.1	53.1	52.5	51	56.8	54.9	58.1	650	740	670	700	700	650	53.2	53.5	61	54.3	56.8	52.1	54.3	52.6	55.6	57.2	53.2	52.6
2-CHLOROTOLUENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	. 5.7	5.5	5.8	920	740	670	700	7007	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5,3
lab_result_ qualifler_ codes	n	Ŋ	Ŋ	Ŋ	n	Ú	n	n	n	Ŋ	n	<u> </u>	n	Ŋ	n	n	Ŋ	n	n	Ŋ	n	Ŋ	Ŋ	Ω	n	n	U
RIN/Even/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	native
Sample	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	96898	96698	86696	96698	96698	95026	95026	95008	95008	97198	97198	97198	97198	97198	97198	97298	97298	97298	97298	97298	97698	97698	97698	97698	97698	97698	97698

Sample			lab_result_ qualifier_	BENZENE	BROMOBENZENE	BROMOBENZENE BROMOCHLOROMETHANE		BROMOFLUOROBENZEN
Borehole Interval	Material	RIN/Event/Bottle	sepoo	(ug/kg)	(ug/kg)	(ug/kg)	BROMODICHLOROMETHAN	(ug/kg)
90998 3.8-4.0	native	98AZU15-001.010		And the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s			86
91198 11.6-11.9	native	98A1091-001.035		***************************************	000000000000000000000000000000000000000			114
91198 15.5-15.8	native	98A1091-001.036						107
91198 19.1-19.5	native	98A1091-001.037						87
91198 19.5-19.8	bedrock	98A1091-001.038						68
91198 3.1-3.4	native	98A1091-001.033	,		**************************************		A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O	110
91198 7.7-8.0	native	98A1091-001.034	-	÷	*		10000000000000000000000000000000000000	108
92598 12.0-12.5	native	98A1092-001.035						96
92598 16.0-16.75	5 bedrock	98A1092-001.036						96
92598 3.5-4.0	native	98A1092-001.033						88
92598 7.5-8.0	native	98A1092-001.034					**************************************	95
95998 12.4-12.8	native	99A7799-003.002				The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s		56.6
95998 14.8-15.2	native	99A7799-004.002						51.1
95998 17.7-18.2	native	99A7799-005.002						54.7
95998 24.6-25.0	bedrock	99A7799-006.002		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	Source Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the		0	59.2
92998 5.0-5.6	native	99A7799-001.002					A TO THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF	54
95998 8.4-8.8	native	99A7799-002.002						47.7
96298 16.1-16.5	bedrock	99A3210-004.017						66
96498 13-13.5	native	99A3210-001.015					TO THE THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY O	100
96498 16.0-16.5	native	99A3210-001.016		000000000000000000000000000000000000000	000-0000000000000000000000000000000000			100
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96498 22.0-22.5	bedrock	99A3210-001.018					**************************************	103
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96698 17.7-18.3	native	99A7930-001.002	•					54.7
96698 20.2-20.6	native	99A7930-002.002						51.8
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96798 12.5-12.9	native	99A6650-003.002		***************************************	***************************************		**************************************	55.5
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96798 20.4-20.8	native	99A6650-005.002	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					72.8
96798 8.4-8.8	native	99A6650-002.002						57.3
96898 12.3-12.6	native	99A6307-003.002						09
96898 17.1-17.4	bedrock	99A6307-004.002						48
96898 4.4-4.7	native	99A6307-001.002						47.7

		lab_result_	BENZENE	RROMORENZENE	BROMOCHI OROMETHANE		BROMOFLUOROBENZEN
RIN/Event/Bottle	ttle	codes	(ug/kg)	(ug/kg)	(ug/kg)	BROMODICHLOROMETHAN	(ug/kg)
99A6307-002.002	2	*********					47.7
99A6824-001.002	7						45.9
99A6824-002.002	~						44.6
99A4102-002.015	ည						91.25
99A4102-002.018	_	·		***************************************	\$ 100 mm 1 mm 1 mm 1 mm 1 mm 1 mm 1 mm 1		100.4
99A6825-003.002	<u> </u>						49.3
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96098 8.5-8.8	native	99A3210-002.014	n	069	069		069	A THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF TAXABLE STATE OF THE TAXABLE STATE OF THE TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF TAXABLE STATE OF
96198 12.0-12.5	native	99A3210-003.015	D	760	760	**************************************	092	A COLOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE
96198 15.8-16.2	bedrock	99A3210-003.016	D	700	. 700		00L	THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O
96198 4.4-4.7	native	99A3210-003.013		700	700	9904999999 1 10991 1 10991 1 10991 1 10000 1 10000 1 10000 1 10000 1 10000 1 10000 1 10000 1 10000 1 10000 1 1	002	And the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of th
96198 8.1-8.5	native	99A3210-003.014	<b>1</b>	670	670		029	WWW.WWW.WWW.WWW.WW.WW.WW.WW.WW.WW.WW.WW
96298 12.25-12.75 native	5 native	99A3210-004.016	Ð	750	750		750	WWW.WWW.WWW.WW.WW.WW.WW.WW.WW.WW.WW.WW.
96298 16.1-16.5	bedrock	99A3210-004.017	n	720	720		720	
96298 4.3-4.7	native	99A3210-004.013	<b>-</b>	700	700		200	
96298 8.0-9.0	native	99A3210-004.014	<b>-</b>	670	670	207720000000000000000000000000000000000	670	
96398 12,4-12.7	native	99A4102-001.009	<b>-</b>	710	710		710	
96398 16.2-16.4	bedrock	99A4102-001.012		730	730		730	
96398 4.3-4.8	native	99A4102-001.003	Э	700	700	700	700	Control of the many and the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control
96398 8.4-8.9	native	99A4102-001.006	D	710	710	710	710	**************************************
96498 13-13.5	native	99A3210-001.015	ı,	1300			1300	
96498 16.0-16.5	native	99A3210-001.016	)	1300			1300	TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL
96498 18.0-18.6	native	99A3210-001.017	⊃	1300			1300	
96498 22.0-22.5	bedrock	99A3210-001.018	D	1500			1500	***************************************
96498 4.8-5.2	native	99A3210-001.013	)	1500			1500	
96498 9.5-10.0	native	99A3210-001.014	⊃	1300			1300	
96598 11.6-12.0	native	99A6817-003.002	n	5.4	5.4	5.		
96598 15.2-15.6	native	99A6817-004.002	⊃	9	9			
96598 18.6-18.9	native	99A6817-005.002	'n	5.3	5.3			White the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the comm
96598 22.3-22.7	bedrock	99A6817-006.002	J	6.2	6.2			
96598 4.2-4.6	native	99A6817-001.002	n	5.7	5.7			202020202020 S AVB
96598 8.4-8.8	native	99A6817-002.002	n	5.3	5.3	***************************************		
96698 12.4-12.8	native	99A6649-003.002	Ω	5.9	5.9	***************************************		
96698 17.7-18.3	native	99A7930-001.002	n	5.6	5.6			
96698 20.2-20.6	native	99A7930-002.002	) )	5.4	5.4			
96698 22.4-22.8	bedrock	99A7930-003.002	n	6.4	6.4			
96698 4.2-4.6	native	99A6649-001.002	n	5.7	5.7			
96698 8.2-8.6	native	99A6649-002.002	⊃	5.6	5.6			
96798 12.5-12.9	native	99A6650-003.002	<b>-</b>	6.2	6.2			
96798 16.0-16.4	native	99A6650-004.002	_	7.2	7.2			
96798 20.4-20.8	native	99A6650-005.002	⊃	7.4	7.4			
96798 4.4-4.8	native	99A6650-001.002	D	5.3	5.3			
96798 8.4-8.8	native	99A6650-002.002	<b></b>	6.3	6.3			
96898 12.3-12.6	native	99A6307-003.002	n	6.4	6.4			20000000000000000000000000000000000000
96898 17.1-17.4	bedrock	99A6307-004.002	n	5.3	5.3	6.0		
96898 4.4-4.7	native	99A6307-001.002	n	5.2	5.2			

Sample   Interval   Material   RINIVevent/Bottle   codes   Qualifier_   Codes   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/kg)   Cug/									
reative         99A6324-002.002         U         5.2         5.2         5.5           netive         99A6324-003.002         U         5.7         5.7         5.7           netive         99A6324-001.002         U         5.7         5.7         5.7           netive         99A6324-001.002         U         5.1         5.1         5.1           netive         99A6324-001.002         U         5.7         5.7         5.7           netive         99A6308-004.003         U         5.7         5.7         5.7           netive         99A6308-004.003         U         5.5         5.8         5.8           netive         99A6308-002.003         U         5.5         5.8         5.8           netive         99A4102-002.012         U         740         740         740           netive         99A4102-002.02         U         700         700         700           netive         99A4102-002.02         U         700         700         700           netive         99A4102-002.02         U         700         700         700           netive         99A6825-004.002         U         5.3         5.3         5.4	ample	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	BENZENE (ug/kg)	BROMOBENZENE (ug/kg)	BROMOCHLOROMETHANE (ug/kg)	BROMODICHLOROMETHAN	BROMOFLUOROBENZEN E (ug/kg)
native         99A6824-003.002         U         5.6         5.6           bedrock         99A6824-004.002         U         5.7         5.7           native         99A6824-004.002         U         5.3         5.3           native         99A6308-004.003         U         5.7         5.7           native         99A6308-004.003         U         5.8         5.8           native         99A4102-002.013         U         5.8         5.8           native         99A44102-002.013         U         5.8         5.8           native         99A44102-002.012         U         7.40         7.40           native         99A4102-002.013         U         650         650           native         99A4102-002.013         U         7.40         7.40           native         99A4102-002.013         U         6.70         6.70           native         99A4825-002.003         U         6.7         5.4         5.4           bedrock         99A6825-004.002         U         6.1         6.1         6.1           native         99A6825-003.002         U         6.1         6.7         5.4           native         99A6825-		native	99A6307-002.002	D		ļ			
bedrock         99A6824-004.002         U         5.7         5.7           native         99A6824-001.002         U         5.3         5.3           native         99A6308-002.003         U         5.1         5.1           bedrock         99A6308-002.003         U         5.8         5.8           native         99A6308-002.003         U         650         650           native         99A4102-002.003         U         650         650           native         99A4102-002.012         U         740         740           native         99A4102-002.013         U         670         670           native         99A4102-002.018         U         670         670           native         99A4102-002.018         U         670         670           native         99A4102-002.018         U         670         670           native         99A6825-003.002         U         5.3         5.3           native         99A6825-003.002         U         5.4         5.4           native         99A6825-003.002         U         5.4         5.4           native         99A6825-003.002         U         5.4         5.4 <td>1-12.7</td> <td>native</td> <td>99A6824-003.002</td> <td>n</td> <td>5.6</td> <td>5.6</td> <td>5.6</td> <td></td> <td></td>	1-12.7	native	99A6824-003.002	n	5.6	5.6	5.6		
native         99A6824-001.002         U         5.3         5.3           native         99A6824-002.002         U         5.2         5.2           native         99A6308-003.003         U         5.7         5.7           native         99A6308-001.003         U         5.5         5.5           native         99A4102-002.003         U         650         650           native         99A4102-002.018         U         700         700           native         99A4102-002.018         U         670         700           native         99A4102-002.018         U         670         700           native         99A4102-002.020         U         650         650           native         99A4102-002.03         U         670         700           native         99A4102-002.002         U         650         650           native         99A6825-002.002         U         650         650           native         99A6825-002.002         U         6.1         6.1           native         99A6825-002.002         U         6.1         6.1           native         99A68275-004.002         U         6.2         5.2	2-17.8	bedrock	99A6824-004.002	Ω	5.7	5.7	5.7		MMMMMM metalentering of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the property of the pr
native         99A6824-002.002         U         5.2         5.2           native         99A6308-003.003         U         5.1         5.1           bedrock         99A6308-004.003         U         5.7         5.7           native         99A6308-002.003         U         5.8         5.8           native         99A4102-002.003         U         670         740           native         99A4102-002.018         U         670         700           native         99A4102-002.018         U         650         650           native         99A4102-002.02         U         650         650           native         99A6825-002.02         U         650         650           native         99A6825-002.002         U         650         650           native         99A6825-002.002         U         6.1         6.1           native         99A68275-003.002         U         6.1         6.1	4.8	native	99A6824-001.002	D	5.3	5.3	additional control to the left for a restautive legal of the restautive transference are represented to 5.3		
native         99A6308-003.003         U         5.1         5.1           bedrock         99A6308-004.003         U         5.7         5.7           native         99A6308-004.003         U         5.5         5.5           native         99A6308-002.003         U         5.8         5.8           native         99A6308-002.003         U         650         650           native         99A4102-002.015         U         740         740           native         99A4102-002.018         U         670         670           native         99A4102-002.018         U         650         650           native         99A4102-002.003         U         650         650           native         99A4825-002.002         U         5.4         5.4           native         99A8825-004.002         U         5.7         5.7           native         99A8825-004.002         U         5.4         5.4           native         99A8825-004.002         U         5.3         5.3           native         99A8275-004.002         U         5.3         5.3           native         99A8275-004.002         U         5.3         5.3 <td></td> <td>native</td> <td>99A6824-002.002</td> <td>D</td> <td>5.2</td> <td>5.2</td> <td>5.2</td> <td>**************************************</td> <td>MANAMAN WAYAWAY WAYAWAY WAYAWAY WAYAWAYA WA WAYAWAYA</td>		native	99A6824-002.002	D	5.2	5.2	5.2	**************************************	MANAMAN WAYAWAY WAYAWAY WAYAWAY WAYAWAYA WA WAYAWAYA
bedrock         99A6308-004,003         U         5.7         5.7           native         99A6308-001,003         U         5.5         5.8           native         99A6308-002,003         U         650         650           native         99A4302-002,003         U         670         670           native         99A44102-002,015         U         740         740           native         99A44102-002,018         U         670         670           native         99A4102-002,018         U         650         650           native         99A6825-003,002         U         650         650           native         99A6825-004,002         U         6.1         6.1           native         99A6825-004,002         U         6.1         6.1           native         99A6825-004,002         U         6.1         5.4           native         99A6825-004,002         U         6.1         5.4           native         99A6825-004,002         U         6.1         5.4           native         99A8275-004,002         U         5.4         5.4           native         99A8275-004,002         U         5.3         5.3 </td <td></td> <td>native</td> <td>99A6308-003.003</td> <td>Ω</td> <td>5.1</td> <td>5.1</td> <td>5.1</td> <td></td> <td></td>		native	99A6308-003.003	Ω	5.1	5.1	5.1		
native         99A6308-001.003         U         5.5         5.5           native         99A6308-002.003         U         5.8         5.8           native         99A6308-002.003         U         650         650           native         99A4102-002.012         U         740         740           native         99A4102-002.018         U         670         670           native         99A4102-002.003         U         650         650           native         99A6825-003.002         U         6.3         5.3           native         99A6825-004.002         U         6.1         6.1           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.2         5.2           native         99A8275-004.002         U         5.3         5.3           native         99A8275-004.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3	Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of the Contract of 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native         99A6308-002.003         U         5.8         5.8           native         99A6308-002.009         U         650         650           native         99A4102-002.012         U         740         740           native         99A4102-002.018         U         670         670           native         99A4102-002.03         U         670         700           native         99A6825-003.002         U         6.3         6.1           native         99A6825-004.002         U         6.1         6.1           bedrock         99A6825-004.002         U         6.1         6.1           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.7         5.7           native         99A8275-004.002         U         5.2         5.2           native         99A8275-004.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3		native	99A6308-001.003	Э	5.5	5.5	5.5		\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$
native         99A4102-002.009         U         650         650           native         99A4102-002.012         U         740         740           native         99A4102-002.018         U         670         670           bedrock         99A4102-002.03         U         650         650           native         99A6825-003.002         U         6.3         6.4           native         99A6825-004.002         U         6.1         6.1           bedrock         99A6825-004.002         U         6.1         6.1           native         99A6825-004.002         U         6.1         6.1           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.7         5.7           native         99A8275-004.002         U         5.7         5.2           native         99A8275-004.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3           native         99A8275-001.002         U         5.3         5.3 <td></td> <td>native</td> <td>99A6308-002.003</td> <td>n</td> <td>5.8</td> <td>5.8</td> <td>5.8</td> <td></td> <td>The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the 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native         99A4102-002.012         U         740         740           native         99A4102-002.015         U         670         670           bedrock         99A4102-002.018         U         700         700           native         99A4102-002.003         U         650         650           native         99A6825-003.002         U         5.3         5.3           bedrock         99A6825-004.002         U         6.1         6.1           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.4         5.4           native         99A6825-004.002         U         5.7         5.7           native         99A8275-003.002         U         5.7         5.7           native         99A8275-004.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.3           native         99A8275-001.002         U         5.3         5.3 <td></td> <td>native</td> <td>99A4102-002.009</td> <td>n</td> <td>650</td> <td>920</td> <td>650</td> <td></td> <td>AMMINIA ATA ATA ATA ATA ATA ATA ATA ATA ATA A</td>		native	99A4102-002.009	n	650	920	650		AMMINIA ATA ATA ATA ATA ATA ATA ATA ATA ATA A
native         99A4102-002.015         U         670         670           bedrock         99A4102-002.018         U         700         700           native         99A4102-002.006         U         700         700           native         99A6825-003.002         U         6.3         6.3           native         99A6825-004.002         U         6.1         6.1           bedrock         99A6825-004.002         U         6.1         6.1           native         99A6825-001.002         U         6.7         6.1           native         99A6825-002.002         U         5.7         6.7           native         99A8275-003.002         U         5.7         5.2           native         99A8275-004.002         U         5.2         5.2           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.5           native         99A8275-009.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3 <td></td> <td>natíve</td> <td>99A4102-002.012</td> <td>n</td> <td>740</td> <td>740</td> <td>740</td> <td>***************************************</td> <td>000000000000000000000000000000000000000</td>		natíve	99A4102-002.012	n	740	740	740	***************************************	000000000000000000000000000000000000000
bedrock         99A4102-002.018         U         700         700           native         99A4102-002.006         U         700         700           native         99A6825-003.002         U         650         650           native         99A6825-004.002         U         6.1         6.1           bedrock         99A6825-004.002         U         6.1         6.1           native         99A6825-001.002         U         5.4         5.4           native         99A6825-001.002         U         5.7         5.7           native         99A68275-003.002         U         5.2         5.2           native         99A8275-004.002         U         5.2         5.2           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.3         5.5           native         99A8275-009.002         U         5.3         5.5           native         99A8275-001.002         U         5.3         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-001.002         U         5.3         5.3 </td <td></td> <td>native</td> <td>99A4102-002.015</td> <td>n</td> <td>670</td> <td>670</td> <td>670</td> <td>0.29</td> <td></td>		native	99A4102-002.015	n	670	670	670	0.29	
native         99A4102-002.006         U         700         700           native         99A4102-002.003         U         650         650           native         99A6825-003.002         U         5.4         5.4           native         99A6825-004.002         U         6.1         6.1           native         99A6825-001.002         U         5.4         5.4           native         99A6825-002.002         U         5.7         5.7           native         99A8275-003.002         U         5.2         5.2           native         99A8275-004.002         U         5.4         5.4           native         99A8275-004.002         U         5.2         5.2           native         99A8275-009.002         U         5.3         5.3           native         99A8275-009.002         U         5.6         5.6           native         99A8275-009.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.7           native         99A8275-002.002         U         5.3         5.7           native         99A82775-003.002         U         5.3         5.3 <td>1-24.8</td> <td>bedrock</td> <td>99A4102-002.018</td> <td>Э</td> <td>700</td> <td>700</td> <td>700</td> <td></td> <td>000000000000000000000000000000000000000</td>	1-24.8	bedrock	99A4102-002.018	Э	700	700	700		000000000000000000000000000000000000000
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native         99A6825-004.002         U         5.4         5.4           bedrock         99A6825-005.002         U         6.1         6.1           native         99A6825-001.002         U         5.4         5.7           native         99A6825-002.002         U         5.7         5.7           native         99A8275-003.002         U         5.2         5.2           native         99A8275-004.002         U         5.4         5.4           native         99A8275-008.002         U         5.3         5.5           native         99A8275-009.002         U         5.6         5.6           native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-001.002         U         5.3         5.3	-	native	99A6825-003.002	D	5.3	5.3	5.3		
bedrock         99A6825-005.002         U         6.1         6.1           native         99A6825-001.002         U         5.4         5.4           native         99A6825-002.002         U         5.7         5.7           native         99A8275-003.002         U         5.2         5.2           native         99A8275-004.002         U         5.4         5.4           native         99A8275-005.002         U         5.3         5.3           native         99A8275-009.002         U         5.6         5.6           native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-001.002         U         5.3         5.3		native	99A6825-004.002	D	5.4	5.4	5.4		NAMES OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY
native         99A6825-001.002         U         5.4         5.4           6         native         99A6825-002.002         U         5.7         5.7           6.         native         99A8275-003.002         U         5.2         5.2           1.9         native         99A8275-004.002         U         5.4         5.4           1.7         native         99A8275-005.002         U         5.3         5.3           1.8         native         99A8275-009.002         U         5.7         5.7           1.8         native         99A8275-001.002         U         5.3         5.3           1.8         native         99A8275-001.002         U         5.3         5.3           1.8         native         99A8275-001.002         U         5.3         5.3	7-18.2	bedrock	99A6825-005.002	D	6.1	6.1	6.1		
native         99A6825-002.002         U         5.7         5.7           .6         native         99A8275-003.002         U         5.2         5.2           .9         native         99A8275-004.002         U         5.4         5.4           .7         native         99A8275-005.002         U         5.3         5.3           .8         native         99A8275-009.002         U         5.6         5.7           .8         native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-001.002         U         5.3         5.3		native	99A6825-001.002	n	5.4	5.4	5.4		000000000000000000000000000000000000000
6         native         99A8275-003.002         U         5.2         5.2           1.9         native         99A8275-004.002         U         5.4         5.4           1.7         native         99A8275-005.002         U         5.3         5.3           1.8         native         99A8275-008.002         U         5.6         5.6           1.8         native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3		native	99A6825-002.002	Ω	5.7	5.7	5.7		Proposition of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the co
1.9         native         99A8275-004.002         U         5.4         5.4           1.7         native         99A8275-005.002         U         5.3         5.3           1.8         native         99A8275-008.002         U         5.6         5.6           1.8         native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3	2-11.6	native	99A8275-003.002	Ω	5.2	5.2	5.2		
1.7 native         99A8275-005.002         U         5.3         5.3           1.8 native         99A8275-008.002         U         5.6         5.6           1.8 native         99A8275-001.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3	6	native	99A8275-004.002	n	5.4	5.4	5.4		0.000000000000000000000000000000000000
(8)         native         99A8275-008.002         U         5.6         5.6           (8)         native         99A8275-009.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3		native	99A8275-005.002	n	5.3	5.3	5.3		COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR COLOR
1.8         native         99A8275-009.002         U         5.7         5.7           native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3		native	99A8275-008.002	Ω	5.6	5.6	5.6		**************************************
native         99A8275-001.002         U         5.3         5.3           native         99A8275-002.002         U         5.3         5.3		native	99A8275-009.002	D	5.7	5.7	5.7		
native 99A8275-002.002 U 5.3 5.3		native	99A8275-001.002	D	5.3	5.3	5.3		
×		native	99A8275-002.002	U	5.3	5.3	5.3		можения на применения на применения на применения на применения на применения на применения на применения на п

8 35.4.0 native 99x2015-001.010 8 115-158 native 99x2015-001.035 8 115-158 native 99x1091-001.035 8 115-158 native 99x1091-001.035 8 117-18 native 99x1091-001.034 8 117-18 native 99x1092-001.034 8 117-18 native 99x1092-001.035 8 117-18 native 99x1092-001.035 8 117-18 native 99x1092-001.035 8 117-18 native 99x1092-001.032 8 117-18 native 99x1092-001.032 8 117-18 native 99x1092-001.032 8 117-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.013 8 118-18 native 99x2010-001.002 8 118-18 native 99x2010-001.002 8 118-18 native 99x2010-001.002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-002 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003 8 118-18 native 99x2010-003	Sample Borehole Interval	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	BROMOFORM (ug/kg)	BROMOMETHANE (ug/kg)	CARBON DISULFIDE (ug/kg)	CARBON TETRACHLORIDE (ug/kg)	CHLOROBENZENE (ug/kg)	CHLORODIBROMOMETHANE (ug/kg)
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Sample Borehole Interval	ple Material		lab_result_ qualifier_ codes	BROMOFORM (ug/kg)	BROMOMETHANE (ug/kg)	CARBON DISULFIDE (ug/kg)	CARBON TETRACHLORIDE (ug/kg)	CHLOROBENZENE (ug/kg)	CHLORODIBROMOMETHANE (ug/kg)
96898 8.4-8.7	native	99A6307-002.002							
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CARBON DISULFIDE (ug/kg)												**************************************			300000000000000000000000000000000000000												000	OB/	089	630	620	710	089	200	720	920	610	5.8	5.3	5.6	6,3	5.6
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RIN/Event/Bottle	98A1091-001.035	98A1091-001.036	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	99A6817-006.002	99A6649-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	99A6307-001.002	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-004.003	99A6825-004.002	99A6825-005.002	99A8Z/5-009.00Z	98AZ015-001.010	98A1091-001 036	98A1091-001.037	98A1091-001.038	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	98A1092-001.033	98A1092-001.034	99A7799-003.002	99A7799-004.002	99A7799-005.002	99A7799-006.002	99A7799-001.002
Material	native	native	native	native	native	bedrock	bedrock	native	native	native	native	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	bedrock	native	bedrock	native	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native
Sample	91198 11.6-11.9	91198 15.5-15.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 16.5-17.0	97298 16.4-17.0	97298 17.7-18.2	9/698 19.4-19.8	90998 3.8-4.0	91190 11.0-11.3	91198 19.1-19.5	91198 19.5-19.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	92598 3.5-4.0	92598 7.5-8.0	95998 12.4-12.8	95998 14.8-15.2	95998 17.7-18.2	95998 24.6-25.0	95998 5.0-5.6
Borehole	91198	91198	91198	91198	92598	92298	96598	96698	96698	96698	96798	96798	96798	96798	96798	96898	96898	86896	96898	96998	96998	96998	96998	97098	97298	97298	9/698	90998	91198	91198	91198	91198	91198	92598	92598	92598	92598	95998	95998	95998	95998	95998

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CHLOROBENZENE (ug/kg)	5.2	700	7007	730	069	760	700	700	670	750	720	700	670	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
CARBON TETRACHLORIDE (ug/kg)	5.2	700	200	730	069	760	200	700	670	750	720	700	920	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4		5.7	5.6	6.2	7.2		5.3	6.3	6.4		5.2
CARBON DISULFIDE (ug/kg)	5.2	200	<u>700</u>	730	069	760	700	700	670	750	720	700	929	710	730		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
BROMOMETHANE (ug/kg)		700	700	730	9069	760	200	700	670	750	720	700	670	710	730	700	710	1300	1300	1300	1500	1500	1300			-																	
BROMOFORM (ug/kg)	5.2	700	200	730	069	760	700	700	670	750	720	2007	670	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	Cu
lab_result_ qualifier_ codes	n	n	n	<u> </u>	<u> </u>	n	n		n	<u> </u>	P	Ω	Ŋ	Ω	n	n	<u></u>	<u> </u>	n	)	n	n	Ω	n	Ω	n	Ω	<b>D</b>	n	ח	ລ		<b>-</b>	Ω	Ω	n	n	Ω	n	Ŋ	n	Ŋ	=
RIN/Event/Bottle	99A7799-002.002	99A3210-002.015	99A3210-002.016	99A3210-002.013	99A3210-002.014	99A3210-003.015	99A3210-003.016	1	99A3210-003.014	-	99A3210-004.017	99A3210-004.013	99A3210-004.014	99A4102-001.009	99A4102-001.012	99A4102-001.003	99A4102-001.006	·												*******		********				******	·····		99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	000 100 200
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	bedrock	Commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of th
Sample	8.4-8.8	96098 12.5-13.0	96098 16.0-16.2	96098 4.5-4.8	96098 8.5-8.8	96198 12.0-12.5	96198 15.8-16.2	96198 4.4-4.7	96198 8.1-8.5	96298 12.25-12.75	96298 16.1-16.5	96298 4.3-4.7	96298 8.0-9.0	96398 12.4-12.7	96398 16.2-16.4	96398 4.3-4.8	96398 8.4-8.9	96498 13-13.5	96498 16.0-16.5	96498 18.0-18.6	96498 22.0-22.5	96498 4.8-5.2	96498 9.5-10.0	96598 11.6-12.0	96598 15.2-15.6	96598 18.6-18.9	96598 22.3-22.7	96598 4.2-4.6	96598 8.4-8.8	96698 12.4-12.8	96698 17.7-18.3	96698 20.2-20.6	96698 22.4-22.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	
Borehole	92998	96098	96098	96098	96098	96198	96198	96198	96198	96298	96298	96298	96298	96398	96398	96398	96398	96498	96498	96498	96498	96498	96498	96598	96598	96598	96598	96598	96598	96998	96998	96998	96998	96998	. 96698	96798	96798	96798	96798	96798	96898	96898	

lab_result_ qualifier_	"It_   BROMOFORM		JLFIDE	CARBON TETRACHLORIDE	CHLOROBENZENE	CHLORODIBROMOMETHANE
codes	(ng/kg)	(ng/kg)	(ug/kg)	(ng/kg)	(ug/kg)	(ug/kg)
		5.2	5.2	5.2	5.2	5.2
		5.6	5.6	5.6	5.6	5.6
		5.7	5.7	5.7	5.7	5.7
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		5.2	5.2	5.2	5.2	5.2
		5.1	5.1	5.1	5.1	5.1
		5.7	. 5.7	5.7	5.7	7.5
		5.5	5.5	5.5	5.5	5.5
		5.8	5.8	5.8	5.8	5.8
	9			650	650	
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		5.3	5.3	5.3	5.3	5.3
		5.4	5.4	5.4	5.4	5.4
		6.1	6.1	6.1	6.1	6.1
		5.4	5.4	5.4	5.4	5.4
		5.7	5.7	5.7	5.7	7.5
		5.2	5.2	5.2	5.2	5.2
		5.4	5.4	5.4	5.4	5.4
		5.3	5.3	5.3	5.3	5.3
		5.6	5.6	5.6	5.6	5.6
		5.7	5.7	5.7	5.7	5.7
		5.3	5.3	5.3	5.3	5.3
		5.3	5.3	5.3	5.3	5.3

| CIS-1,3-<br>DICHLOROPROPYLEN<br>E<br>(ug/kg) |                 |                 | With the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the 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Sample	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	CHLOROETHANE (ug/kg)	CHLOROFORM (ug/kg)	Chloromethane (ug/kg)	CIS-1,2- DICHLOROETHENE (ug/kg)	CIS-1,3- DICHLOROPROPENE. (ug/kg)	CIS-1,3- DICHLOROPROPYLEN E (ug/kg)
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96998 4.4-4.8	native	99A6824-001.002				**************************************	CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR 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RIV/Event/Bottle	98A1091-001.035	98A1091-001.036	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	99A6817-006.002	99A6649-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	99A6307-001.002	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-004.003	99A6825-004.002	99A6825-005.002	99A8275-009.002	98A2015-001.010	98A1091-001.035	98A1091-001.036	98A1091-001.037	98A1091-001.038	98A1091-001.033	98A1091-001.034	98A1092-001.035	98A1092-001.036	98A1092-001.033	98A1092-001.034	99A7799-003.002	99A7799-004.002	99A7799-005.002	99A7799-006.002	99A7799-001.002
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Sample	91198 11.6-11.9	91198 15.5-15.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96/98 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 16.5-17.0	97298 16.4-17.0	97298 17.7-18.2	97698 19.4-19.8	90998 3.8-4.0	91198 11.6-11.9	91198 15.5-15.8	91198 19.1-19.5	91198 19.5-19.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	92598 3.5-4.0	92598 7.5-8.0	95998 12.4-12.8	95998 14.8-15.2	95998 17.7-18.2	95998 24.6-25.0	95998 5.0-5.6
Borehole	9119	9119	9119	9119	9259	9259	9659	16996	16996	9669	9679	6/96	9679	9679	9679	96896	96896	96898	96898	8696	8696	6696	6696	9208	9729	9729	9769	·6606	9119	9119	9119	9119	9119	9119	9259	9259	9259	9259	9599	9599	9599	9599	9599

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ORM	(ug/kg)	5.2	700	700	730	069	760	7007	2007	670	750	720	700	029	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3		5.7	5.3	5.9	5.6	5.4		5.7	5.6	6.2	7.2		5.3	6.3	6.4		
HANE	(ug/kg)	5.2	700	2007	730	069	760	200	700	920	750	720	700	670	710	730	700	710	1300	1300	1300	1500	1500	1300	5.4	9	5.3	6.2	5.7	5.3	6.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	
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	RIN/Event/Bottle	99A7799-002.002	99A3210-002.015	99A3210-002.016	99A3210-002.013	99A3210-002.014	99A3210-003.015	99A3210-003.016	99A3210-003.013	99A3210-003.014	99A3210-004.016	99A3210-004.017	99A3210-004.013	99A3210-004.014	99A4102-001.009	99A4102-001.012	99A4102-001.003	99A4102-001.006	99A3210-001.015	99A3210-001.016	99A3210-001.017	99A3210-001.018	99A3210-001.013	99A3210-001.014	99A6817-003.002	99A6817-004.002	99A6817-005.002	99A6817-006.002	99A6817-001.002	99A6817-002.002	99A6649-003.002	99A7930-001.002	99A7930-002.002	99A7930-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	000 4000
	Material	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	bedrock								
	ole Interval	95998 8.4-8.8	96098 12.5-13.0	96098 16.0-16.2	96098 4.5-4.8	96098 8.5-8.8	96198 12.0-12.5	96198 15.8-16.2	96198 4.4-4.7	96198 8.1-8.5	75	96298 16.1-16.5	96298 4.3-4.7	96298 8.0-9.0	96398 12.4-12.7	96398 16.2-16.4	96398 4.3-4.8	96398 8.4-8.9	96498 13-13.5		96498 18.0-18.6	96498 22.0-22.5			96598 11.6-12.0	96598 15.2-15.6	96598 18.6-18.9	96598 22.3-22.7	96598 4.2-4.6	96598 8.4-8.8	96698 12.4-12.8	96698 17.7-18.3	96698 20.2-20.6	96698 22.4-22.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	· · · · · · · · · · · · · · · · · · ·
	Borehole	<u>გ</u>	96	96	99	8	96	96	96	96	96	96	96	8	96	96	36	96	96	96	96	96	96	96	96	96	96	36	96	96	96	96	8	8	36	96	96	8	8	8	36	ቖ	8	· consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence of the consequence

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CIS-1,3- DICHLOROPROPYLEN E (ug/kg)					T		**************************************		1	AND THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF T		47700000000000000000000000000000000000		TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TO			4		4	Management of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the	4	Alemania de la companya de la companya de la companya de la companya de la companya de la companya de la compa			4)	1	4)
CIS-1,3- DICHLOROPROPENE (ug/kg)		AND THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPER	**************************************		######################################	00000000000000000000000000000000000000	WAS THE THE THE THE THE THE THE THE THE THE			650	740	670	700	700	650	CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR O				3000 000 000 000 000 000 000 000 000 00							
CHLOROETHANE CHLOROFORM Chloromethane DICHLOROETHENE (ug/kg) (ug/kg)		Octobros Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Company Compa		\$ VVVVVVVVVVVVVVVVVVVVVVVVVVVVVVVVVVVV	**************************************					920	740	670	700	200	650												
Chloromethane (ug/kg)				2007 P. 10 10 10 10 10 10 10 10 10 10 10 10 10						650			700		650												
CHLOROFORM (ug/kg)			5.7		5.2							670						6.1	5.4	- Carlo					5.7		
CHLOROETHANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	200	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
lab_result_ qualifier_ codes	n	Ŋ	D	Ω	D	n n	n	n	n	n	n	n	n D	n	n	D	Ω	n	n	D	n	Ω	n	⊃	n	Ω	n
RIN/Event/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	native
Sample	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8		97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	and and and and and and and and and and	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	86898	86696	86696	96998	96696	95026	95026	92008	92008	97198	97198	97198	97198	97198	97198	97298	97298	97298	97298	97298	97698	97698	97698	97698	97698	97698	97698

			lab_result_		-			DICHLOROBROMOME
Sample   Sample   Borehole   Interval	Material	RIN/Event/Bottle	codes	(ug/kg)	Upromocnioromementarie (ug/kg)	(ug/kg) (ug/kg)	UIBACINICINIE I DANE (ug/kg)	(ug/kg)
90998 3.8-4.0	native	98A2015-001.010						
91198 11.6-11.9	native	98A1091-001.035						AMORTO LO LO LO LO LO CONTRATO DE CONTRATO DE COLOTO DE LO CALIDADA DE LO CALIDADA ANTO ANTO ANTO ANTO ANTO ANTO ANTO ANT
91198 15.5-15.8	native	98A1091-001.036					CONTROL OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE	
91198 19.1-19.5	native	98A1091-001.037						
91198 19.5-19.8	bedrock	98A1091-001.038					***************************************	***************************************
91198 3.1-3.4	native	98A1091-001.033					Control of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	ANN THE THE THE THE THE THE THE THE THE THE
91198 7.7-8.0	native	98A1091-001.034			A CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR		**************************************	**************************************
92598 12.0-12.5	native	98A1092-001.035			AASSAANIA AA AA AA AA AA AA AA AA AA AA AA AA A			
92598 16.0-16.75	bedrock	98A1092-001.036			***************************************		division in the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of the contract of th	······································
92598 3.5-4.0	native	98A1092-001.033			VALUE AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PARTY AND THE PA			
92598 7.5-8.0	native	98A1092-001.034						
95998 12.4-12.8	native	99A7799-003.002				50.2		
95998 14.8-15.2	native	99A7799-004.002	***************************************			45.3		
95998 17.7-18.2	native	99A7799-005.002		AND THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF T	CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR	46.4		
95998 24.6-25.0	bedrock	99A7799-006.002				52.6		
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95998 8.4-8.8	native	99A7799-002.002				43.1		***************************************
96298 16.1-16.5	bedrock	99A3210-004.017				106	\$ 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 100 mm = 1	
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96598 11.6-12.0	native	99A6817-003.002				45.6		
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96698 17.7-18.3	native	99A7930-001.002				46.8		
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Material         RIN/Even/Bottle         codes         (ug/kg)           native         99A6307-002.002         (ug/kg)           native         99A6824-001.002         (ug/kg)           native         99A6824-001.002         (ug/kg)           native         99A6825-002.002         (ug/kg)           native         99A6825-002.002         (ug/kg)           native         99A6825-003.002         (ug/kg)           native         99A6825-001.002         (ug/kg)           native         99A6825-001.002         (ug/kg)           native         99A68275-001.002         (ug/kg)           native         99A68275-001.003         (ug/kg)           pedrock         98A1091-001.034         (ug/kg)           pedrock         98A1092-001.035         (ug/kg)           pedrock         98A1092-001.034         (ug/kg)           pedrock         98A1092-001.034         (ug/kg) <th>Cloroethane (ug/kg)         DIBROMOFLUOROMETHANE (ug/kg)         DIBROMOMETHANE (ug/kg)           (ug/kg)         45.7         (ug/kg)           (ug/kg)         45.7         (ug/kg)           49.9         49.9         (ug/kg)           49.9         49.9         (ug/kg)           49.9         49.9         (ug/kg)           49.9         49.9         (ug/kg)           85.56         85.56         (ug/kg)           85.67         47.4         (ug/kg)           85.67         50.1         (ug/kg)           85.7         48.4         (ug/kg)           85.7         50.7         (ug/kg)           85.7         60.7         (ug/kg)           85.7         60.7         (ug/kg)           85.7         60.7         (ug/kg)           85.7         0</th> <th>DICHLOROBROMOME THANE (ug/kg)</th>	Cloroethane (ug/kg)         DIBROMOFLUOROMETHANE (ug/kg)         DIBROMOMETHANE (ug/kg)           (ug/kg)         45.7         (ug/kg)           (ug/kg)         45.7         (ug/kg)           49.9         49.9         (ug/kg)           49.9         49.9         (ug/kg)           49.9         49.9         (ug/kg)           49.9         49.9         (ug/kg)           85.56         85.56         (ug/kg)           85.67         47.4         (ug/kg)           85.67         50.1         (ug/kg)           85.7         48.4         (ug/kg)           85.7         50.7         (ug/kg)           85.7         60.7         (ug/kg)           85.7         60.7         (ug/kg)           85.7         60.7         (ug/kg)           85.7         0	DICHLOROBROMOME THANE (ug/kg)
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Appendix E Real VOC Data

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RIWEvent/Bottle	98A1091-001.035	98A1091-001.036	98A1091-001.033	******	98A1092-001.035	1	99A6817-006.002	99A6649-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	T	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	99A6307-001.002	~~~	1		-	·		·····					*	***************************************		*******							99A7799-004.002	99A7799-005.002	99A7799-006.002	99A7799-001.002
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Sample	91198 11.6-11.9	91198 15.5-15.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	96698 4.2-4.6	96698 8.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	96798 4.4-4.8	96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 16.5-17.0	97298 16.4-17.0	97298 17.7-18.2	97698 19.4-19.8	90998 3.8-4.0	91198 11.6-11.9	91198 15.5-15.8	91198 19.1-19.5	91198 19.5-19.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	92598 3.5-4.0	92598 7.5-8.0	95998 12.4-12.8	95998 14.8-15.2	95998 17.7-18.2	95998 24.6-25.0	95998 5.0-5.6
Borehole	91198	91198	91198	91198	92598	92598	96598	96998	86996	86996	86298	96798	96798	86298	96798	96898	96898	96898	96898	86696	86696	86696	86696	95008	97298	97298	97698	86606	91198	91198	91198	91198	91198	91198	92598	92598	92598	92598	95638	95998	95998	95998	95998

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<u></u>	native	99A7799-002.002	Ъ				5.2	5.2
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96398 4.3-4.8	native	99A4102-001.003	n		700		700	
96398 8.4-8.9 n	native	99A4102-001.006			710		710	***************************************
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Sample Borehole Interval	   Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	Cloroethane (ug/kg)	Dibromochloromethane (ug/kg)	DIBROMOFLUOROMETHANE DIBROMOMETHANE (ug/kg)	DIBROMOMETHANE (ug/kg)	DICHLOROBROMOME THANE (ug/kg)
96898 8.4-8.7	native	99A6307-002.002	)				5.2	5.2
96998 12.4-12.7	native	99A6824-003.002	n	10.000	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		5.6	5.6
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96998 4.4-4.8	native	99A6824-001.002	n				5.3	5.3
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97098 12.4-12.6	native	99A6308-003.003	n				5.1	5.1
97098 16.5-17.0	bedrock	99A6308-004.003	n				5.7	5.7
97098 4.2-4.7	native	99A6308-001.003	n				5.5	5.5
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97198 4.4-4.8	native	99A4102-002.006	n		700		700	
97198 7.3-7.6	native	99A4102-002.003	Ω		029		650	WWW.
97298 12.4-12.8	native	99A6825-003.002	_				5.3	5.3
97298 16.4-17.0	native	99A6825-004.002	n				5.4	5.4
97298 17.7-18.2	bedrock	99A6825-005.002	<b>-</b>				6.1	6.1
97298 4.0-4.4	native	99A6825-001.002	n				5.4	5.4
97298 8.4-8.8	native	99A6825-002.002	n				5.7	5.7
97698 11.2-11.6	native	99A8275-003.002	ח	**********			5.2	5.2
97698 13.5-13.9	native	99A8275-004.002	D				5.4	5.4
97698 16.3-16.7	native	99A8275-005.002	n				5.3	5.3
97698 18.2-18.8	native	99A8275-008.002	n				5.6	5.6
97698 19.4-19.8	native	99A8275-009.002	_				5.7	5.7
97698 4.6-5.8	native	99A8275-001.002	D				5.3	5.3
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HEXACHLOROBUTADIENE ISOPROPY (ug/kg)	5.2	2007	2002	001	US./	069	760	700	00L	029	750	720	700 T	670	710	730	200	710	WWW. THE THE THE THE THE THE THE THE THE THE	WOODWOODS (TV-2000)					5.4	9	5.3	6.2	5.7	MONOTO DE SE PROPRIO DE LA CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CONTRACTORIO DE CON	5.9	9.6	5.4	6.4	5.7	5.6	6.2	7.2	4.7	5.3	6.3	6.4	5.3	
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DICHLORODIFLUORO METHANE (ug/kg)	5.2	002	22.	007	/ 30	069	760	, 700	700		750	720	700	670	710	730	200	710	THE STATE ASSESSMENT OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PR						5.4	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	4.7	5.3	6.3	6.4	5.3	
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ISOPROPYLBENZE (ug/kg)		***************************************	Sammer commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same commence of the same 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ISOPROPYL BENZENE ISOPROPYLBENZENE (ug/kg)	5.2	5.6		AND AND AND AND AND AND AND AND AND AND		5.1	5.7	5.5	5.8								5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6		MONOMORPHICAL CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACT	5.3
HEXACHLOROBUTADIENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
FREON 113 (ug/kg)							•			650	740	029	700	700	650												
ETHYLBENZENE FREON 113 (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	029	200	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
DICHLORODIFLUORO METHANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	200	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
lab_result_ qualifier_ codes	n	n	n	n.	Ω	Ω	Ω	n	D.	Ω	_	Ω	⊃	Ω	D	Ω	D.	<u> </u>	_	Ω	n	n	n	Ω	n	D	П
RIN/Event/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	native
Sample Interval	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	968	)696	696	696	3696	970	970	970	9706	971	971	971	9718	971	9716	972(	972	972	972	9729	926	976	926	926	976	976	976

Both-bile         Inflaterial         Britation         Britation         Britation         Cug/kg)         (ug/kg)         le</th> <th></th> <th></th> <th>lab_result_ qualifier_</th> <th>M- DICHLOROBENZENE</th> <th>METHYL BROMIDE</th> <th>METHYL CHLORIDE</th> <th>METHYLENE</th> <th>N-BUTYLBENZENE</th> <th>N-PROPYLBENZENE</th>	Sample			lab_result_ qualifier_	M- DICHLOROBENZENE	METHYL BROMIDE	METHYL CHLORIDE	METHYLENE	N-BUTYLBENZENE	N-PROPYLBENZENE
9         native         98A1091-001.035           1.8         native         98A1091-001.035           1.8         native         98A1091-001.035           1.8         native         98A1091-001.035           1.5         native         98A1091-001.035           1.75         bedrock         98A1092-001.035           1.75         bedrock         98A1092-001.035           1.75         bedrock         98A1092-001.035           1.8         native         99A7799-003.002           1.9         native         99A7799-004.002           1.0         bedrock         99A7799-002.002           1.0         bedrock         99A7799-001.002           1.0         bedrock         99A3210-001.015           1.0         native         99A3210-001.016           1.0         native         99A3210-001.016           1.0         native         99A3210-001.017           1.0         native         99A3210-001.016           1.0         native         99A3210-001.016           1.0         native         99A3210-001.016           1.0         native         99A6817-003.002           1.0         native         99A6817-003.002	83.2	Material	RIN/Event/Bottle 98A2015-001.010	səpoo	(ng/kg)	(ug/kg)	(ng/kg)	(ng/kg)	(ug/kg)	(ug/kg)
native         98A1091-001.036           native         98A1091-001.037           bedrock         98A1091-001.033           native         98A1092-001.035           native         98A1092-001.035           native         98A1092-001.033           native         98A71092-001.033           native         99A7799-005.002           native         99A7799-002.002           native         99A7799-001.002           native         99A3210-001.015           native         99A3210-001.015           native         99A3210-001.013           native         99A3210-001.013           native         99A3210-001.013           native         99A3210-001.012           pedrock         99A3210-001.013           native         99A6817-002.002           native         99A6817-003.002           pedrock         99A6817-003.002           native         99A6849-003.002           99A6681-002.002         99A6689-003.002           native         99A6689-003.002           99A6689-002.002         99A6689-003.002           native         99A6689-003.002           99A66890-003.002           native         99A66890-003.002	91198 11.6-11.9	native	98A1091-001.035		***************************************	***************************************	AN TO WALL THE REPORT TO THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY 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native         98A1091-001.037           bedrock         98A1091-001.038           native         98A1091-001.033           native         98A1092-001.035           bedrock         98A1092-001.035           native         98A1092-001.033           native         98A799-003.002           native         99A7799-006.002           native         99A7799-001.002           native         99A3210-001.015           native         99A3210-001.015           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.012           native         99A3210-001.012           pedrock         99A6817-003.002           pedrock         99A6817-003.002           native         99A6817-003.002           pedrock         99A6849-003.002           pedrock         99A6689-003.002           native         99A6689-003.002           pedrock         99A6689-003.002           native         99A6689-003.002           99A6689-003.002	91198 15.5-15.8	native	98A1091-001.036							CONTRACTOR OF THE CONTRACTOR AND THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR
bedrock         98A1091-001.038           native         98A1091-001.033           native         98A1092-001.035           bedrock         98A1092-001.036           native         98A1092-001.033           native         98A7092-001.033           native         99A7799-003.002           native         99A7799-006.002           native         99A7799-001.002           native         99A3210-001.017           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.018           native         99A3210-001.012           pedrock         99A3210-001.012           native         99A6817-003.002           native         99A6817-003.002           native         99A6849-003.002           pedrock         99A6849-003.002           pedrock         99A6689-003.002           native         99A6689-003.002           native         99A6689-003.002           native         99A66890-003.002           native         99A66890-003.002<	91198 19.1-19.5	native	98A1091-001.037							initial public - Viv. proprogramme more more more more more more more m
native         9841091-001.033           native         9841091-001.034           native         9841092-001.035           bedrock         9841092-001.033           native         9847092-001.033           native         9947799-002.002           pedrock         9947799-006.002           native         9947799-001.002           native         9943210-001.015           native         9943210-001.015           native         9943210-001.015           native         9943210-001.016           native         9943210-001.013           native         9943210-001.016           native         994817-002.002           pedrock         994817-003.002           native         9946817-003.002           pedrock         9946817-002.002           pedrock         9946849-003.002           pedrock         9946849-003.002           pedrock         9946869-003.002           native         9946869-003.002           9946869-003.002         native           9946869-003.002         native           9946869-003.002         native           9946869-003.002         native           99468690-003.002	91198 19.5-19.8	bedrock	98A1091-001.038			÷		Anni in the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same a	**************************************	
native         9841091-001.034           native         9841092-001.035           bedrock         9841092-001.035           native         9841092-001.033           native         9847799-003.002           native         9947799-006.002           bedrock         9947799-001.002           native         9947799-001.002           native         9943210-001.015           native         9943210-001.015           native         9943210-001.016           native         9943210-001.013           native         9943210-001.013           native         994817-002.002           pedrock         994817-003.002           native         994817-002.002           pedrock         9946817-003.002           native         9946817-002.002           pedrock         9946849-003.002           pedrock         9946849-003.002           pedrock         9946869-003.002           native         9946869-003.002           9946869-003.002         native           9946869-003.002         native           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Borehole	91198	91198	91198	91198	92598	92598	96598	96998	96698	96698	96798	96798	96798	96798	96798	96898	96898	96898	96898	96998	96998	96998	96998	94026	97298	97298	97698	90998	91198	91198	91198	91198	91198	91198	92598	92598	92598	92598	95998	95998	95998	95998	95998

	,	lab_result_	M- DICHLOROBENZENE	METHYL BROMIDE	METHYL CHLORIDE	METHYLENE	N-BUTYLBENZENE	N-PROPYLBENZENE
	RIN/Event/Bottle	codes	(ug/kg)		(ug/kg)	(ug/kg)	(ng/kg)	(ng/kg)
-	99A7799-002.002	<b>-</b>	5.2	5.2	5.2	5.2	5.2	5.2
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bedrock	99A3210-001.018	D				1500		
native	99A3210-001.013	)				1500		
native	99A3210-001.014	D				1300		***************************************
native	99A6817-003.002	<u>ר</u>	5.4	5.4	5.4	5.4	5.4	5.
native	99A6817-004.002	D	9	9	9		9	***************************************
native	99A6817-005.002	<b>D</b>	5.3	5.3	5.3	5.3		00000000000000000000000000000000000000
bedrock	99A6817-006.002	D	6.2	6.2	6.2		6.2	***************************************
native	99A6817-001.002	n	5.7	5.7	5.7			0000000
native	99A6817-002.002	<b>-</b>		5.3	5.3	5.		5.3
native	99A6649-003.002	<b>-</b>	5.9	5.9	5.9	5.9	5.9	
native	99A7930-001.002	⊃	5.6	5.6	5.6		5.6	5.6
native	99A7930-002.002	)	5.4	5.4	5.4		5.4	
bedrock	99A7930-003.002	<b>&gt;</b>	6,4	6.4	6.4			6.4
native	99A6649-001.002	⊃	2.7	5.7	5.7			
native	99A6649-002.002	<b>¬</b>	5.6	5.6	5.6	5.6		5.6
native	99A6650-003.002	2	6.2	6.2	6.2		6.2	
native	99A6650-004.002	D	7.2	7.2	7.2		7.2	7.2
native	99A6650-005.002	D	7.4	7.4	7.4		7.4	
native	99A6650-001.002	n	5.3	5.3	5.3	5.3	5.3	5.3
native	99A6650-002.002	n	6.3	6.3	6.3		6.3	
native	99A6307-003.002	<b>-</b>	6.4	6.4	6.4		6.4	
bedrock	99A6307-004.002	<b>-</b>	5.3	5.3	5.3		5.3	5.3
native	9946307-001 002		£ 3	. Э	C 3		THE RESIDENCE OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY	White the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the commence of the comm

			lab_result_	M-	METHYL	i i i	METHYLENE		
Sample Borehole Interval	Material	RIN/Event/Bottle	dnamer_	UCALOROBENZENE (ug/kg)		METATE CALORIDE (ug/kg)	CHLORIDE (ug/kg)	N-BOTTLBENZENE (ug/kg)	N-FROPTLBENZENE (ug/kg)
96898 8.4-8.7	native	99A6307-002.002	ח	5.2	5.2	5.2		5.2	5.2
96998 12.4-12.7	native	99A6824-003.002	n	5.6	5.6	5.6		5.6	5.6
96998 17.2-17.8	bedrock	99A6824-004.002	Ω	5.7	5.7	5.7	5.7	5.7	5.7
96998 4.4-4.8	native	99A6824-001.002	D	5.3	5.3	5.3		5.3	5.3
96998 8.4-8.8	native	99A6824-002.002	Ω	5.2	5.2	5.2		5.2	5.2
97098 12.4-12.6	native	99A6308-003.003	Ω	5.1	5.1	5.1	5.1	5.1	5.1
97098 16.5-17.0	bedrock	99A6308-004.003	n	, 5.7	5.7	5.7	***************************************		5.7
97098 4.2-4.7	native	99A6308-001.003	Ω	5.5	5.5	5.5	5.5		
97098 8.4-8.8	native	99A6308-002.003	Ω	5.8	5.8	5.8		5.8	**************************************
97198 12.4-12.8	native	99A4102-002.009	n	THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE 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97198 15.5-16.1	native	99A4102-002.012	Ω	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000			740	740	***************************************
97198 20.4-20.8	native	99A4102-002.015	Ω				670		929
97198 24.4-24.8	bedrock	99A4102-002.018	Ω					200	200
97198 4.4-4.8	native	99A4102-002.006	Ω					200	200
97198 7.3-7.6	native	99A4102-002.003	Ω					650	650
97298 12.4-12.8	native	99A6825-003.002	Ω	5.3	5.3	5.3		5.3	5.3
97298 16.4-17.0	native	99A6825-004.002	Ω	5.4	5.4	5.4	5.4	5.4	5.4
97298 17.7-18.2	bedrock	99A6825-005.002	Ω	6.1	6.1	6.1	6.1	6.1	6.1
97298 4.0-4.4	native	99A6825-001.002	Ω	5.4	5.4	5.4		5.4	5.4
97298 8.4-8.8	native	99A6825-002.002	Ω	5.7	5.7	5.7		5.7	5.7
97698 11.2-11.6	native	99A8275-003.002	D	5.2	5.2	5.2		5.2	5.2
97698 13.5-13.9	native	99A8275-004.002	Ω	5,4	5.4	5.4		5.4	5.4
97698 16.3-16.7	native	99A8275-005.002	Ω	5.3	5.3	5.3		5.3	5.3
97698 18.2-18.8	native	99A8275-008.002	Ω	5.6	5.6	5.6		5.6	5.6
97698 19.4-19.8	native	99A8275-009.002	Ω	2.7	5.7	2.7		5.7	5.7
97698 4.6-5.8	native	99A8275-001.002	Ω	5.3	5.3	5.3	5.3		5.3
97698 8.2-8.6	native	99A8275-002.002	<b>D</b>	5.3	5.3	5.3	5.3	5.3	5.3

	Material RIN/Event/Bottle		ab_result_ qualifier_ codes	NAPHTHALENE (ug/kg)	O-DICHLOROBENZENE (ug/kg)	P- DICHLOROBENZENE (ug/kg)	SEC-BUTYLBENZENE (ug/kg)	STYRENE (ug/kg)	TERT- BUTYLBENZENE (ug/kg)
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Sample Borehole Interval	Material	RIN/Event/Bottle	qualifier_ codes	NAPHTHALENE (ug/kg)	O-DICHLOROBENZENE (ug/kg)	DICHLOROBENZENE (ug/kg)	SEC-BUTYLBENZENE (ug/kg)	STYRENE (ug/kg)	BUTYLBENZENE (ug/kg)
96898 8.4-8.7	native	99A6307-002.002							
96998 4.4-4.8	native	99A6824-001.002				TO A TOTAL TO THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CONTROL OF THE CON	TO COLOR ON CONTRACTOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLOR ON COLO	ANNOTATION OF THE THE THE THE THE THE THE THE THE THE	
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97198 24.4-24.8	bedrock	99A4102-002.018		<b>4)</b>	***************************************	***************************************	Antiferrania manara manara manara manara manara manara manara manara manara manara manara manara manara manara	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	***************************************
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!					98A1091-001.034	98A1092-001.035	98A1092-001.036	99A6817-006.002	99A6649-003.002	1																				98A1091-001.035	98A1091-001.036	1	96A1091-001.036	9841091-001 034	*****	-	98A1092-001.033	98A1092-001.034	99A7799-003.002	99A7799-004.002	99A7799-005.002	9947799-006 002
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	Borehole Interval	91198 11.6-11.9	91198 15.5-15.8	91198 3.1-3.4	91198 7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	96698 4.2-4.6				96798 20.4-20.8		96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7			96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 16.5-17.0		97298 17.7-18.2	∞.			-	91198 19.1-19.5	91190 19.3-19.0	***************************************	5	ıc	92598 3.5-4.0		<b>∞</b>	95998 14.8-15.2	95998 17.7-18.2	05008 24 R-25 0

lab_result_qualifier_codes         NAPHTHALENE qualifier_codes         O-DICHLOROBENZENE (ug/kg)         P- codes         ult_codes         P-           qualifier_codes         (ug/kg)         P-           codes         5.2         (ug/kg)           700         700         (ug/kg)           730         760         (ug/kg)           760         760         (ug/kg)           760         760         (ug/kg)           760         760         (ug/kg)           770         710         (ug/kg)           730         710         (ug/kg)           730         710         (ug/kg)           710         710         (ug/kg)           710         710         (ug/kg)	lab_result_qualifier_ qualifier_ qualifier_ (ug/kg)	
ab_result_codes	lab_result_qualifier_	Material         RIN/Event/Bottle         codes         (ug/kg)         (ug/kg)         (ug/kg)           native         99A3710-002.015         U         5.2         (ug/kg)         5.2           native         99A3210-002.015         U         700         5.2           native         99A3210-002.014         U         700         5.2           native         99A3210-002.014         U         700         5.0           native         99A3210-003.015         U         700         5.0           native         99A3210-003.015         U         700         5.0           native         99A3210-004.017         U         700         5.0           native         99A3210-004.013         U         700         5.0           native         99A3210-004.014         U         700         710           bedrock         99A3210-004.013         U         710         710           bedrock         99A4102-001.012         U         730         10           native         99A3210-001.015         U         730         10           patrive         99A3210-001.015         U         730         10           native         99A3210-001.015<
qualifier_ (ug/kg)  codes (ug/kg)	lab_result qualifier   NAPHTHALEN     Codes   (ug/kg)     U	Material native         RIN/Event/Bottle codes         (ug/kg)           native         99A3210-002.002         U           bedrock         99A3210-002.015         U           native         99A3210-002.015         U           bedrock         99A3210-002.014         U           native         99A3210-003.015         U           bedrock         99A3210-003.015         U           native         99A3210-003.014         U           bedrock         99A3210-004.017         U           native         99A3210-004.017         U           bedrock         99A3210-004.017         U           native         99A4102-001.009         U           bedrock         99A4102-001.003         U           native         99A3210-001.015         U           native         99A3210-001.016         U           padrock         99A3210-001.016         U           native         99A3210-001.016         U           99A3210-001.016         U           native         99A3210-001.016         U           99A3210-001.017         U
lab_result_ qualifier_ codes_ U U U U U U U U U U U U U U U U U U U		Material         RIN/Event/Bottle           native         99A7799-002.002           bedrock         99A3210-002.015           bedrock         99A3210-002.014           native         99A3210-002.014           native         99A3210-003.015           bedrock         99A3210-003.016           native         99A3210-004.017           native         99A3210-004.017           native         99A3210-004.017           native         99A3210-004.017           native         99A3210-004.017           native         99A4102-001.009           pedrock         99A4102-001.009           native         99A3210-004.017           pattive         99A3210-001.003           native         99A3210-001.013           pattive         99A3210-001.013           pattive         99A3210-001.015           pattive         99A3210-001.015           pattive         99A3210-001.015           pattive         99A3210-001.015           pattive         99A3210-001.017           pattive         99A3210-001.017           pattive         99A3210-001.017           pattive         99A3210-001.017
		Material         RIN/Event/Bottle           native         99A7799-002.002           native         99A3210-002.015           bedrock         99A3210-002.013           native         99A3210-002.014           native         99A3210-003.015           bedrock         99A3210-003.016           native         99A3210-003.017           native         99A3210-004.016           bedrock         99A3210-004.017           native         99A3210-004.017           native         99A3210-004.017           native         99A4102-001.009           99A4102-001.012           native         99A3210-004.014           99A3210-001.012           native         99A3210-001.012           99A3210-001.013           native         99A3210-001.013           99A3210-001.013           native         99A3210-001.014           99A3210-001.013           native         99A3210-001.014           99A3210-001.013           native         99A3210-001.014           99A3210-001.013

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Sample		el#o8/teo/2/Mid	lab_result_ qualifier_	NAPHTHALENE	O-DICHLOROBENZENE	P- DICHLOROBENZENE	SEC-BUTYLBENZENE	STYRENE	TERT- BUTYLBENZENE
8 8.4	native	99A6307-002.002	<u> </u>	5.2	5.2	(37.3)			5.2
96998 12.4-12.7	native	99A6824-003.002	Ω	5.6	5.6	5.6	5.6	5.6	5.6
96998 17.2-17.8	bedrock	99A6824-004.002	n	5.7	5.7	5.7	5.7	5.7	5.7
96998 4.4-4.8	native	99A6824-001.002	n	5.3	5.3	5.3			5.3
96998 8.4-8.8	native	99A6824-002.002	Ω	5.2	5.2	5.2			5.2
97098 12.4-12.6	native	99A6308-003.003	n	5.1	5.1	5.1	5.1	5.1	5.1
97098 16.5-17.0	bedrock	99A6308-004.003	n	. 5.7	5.7	5.7		***************************************	5.7
97098 4.2-4.7	native	99A6308-001.003	Ω	5.5	5.5	5.5		00.00000000000000000000000000000000000	5.5
97098 8.4-8.8	native	99A6308-002.003	Ω	5.8	5.8	5.8	5.8		5.8
97198 12.4-12.8	native	99A4102-002.009	n				650	650	650
97198 15.5-16.1	native	99A4102-002.012	∩				740		740
97198 20.4-20.8	native	99A4102-002.015	Ω	670			920		670
97198 24.4-24.8	bedrock	99A4102-002.018	Ω	200			200		200
97198 4.4-4.8	native	99A4102-002.006	<b>n</b>		A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O		200	700	700
97198 7.3-7.6	native	99A4102-002.003	Ω				650	2007/Z23000.000000000000000000000000000000000	059
97298 12.4-12.8	native	99A6825-003.002	Ω	5.3	5.3	5.3			5.3
97298 16.4-17.0	native	99A6825-004.002	n	5.4	5.4	5.4	5.4	5.4	5.4
97298 17.7-18.2	bedrock	99A6825-005.002	n	6.1	6.1	6.1	6.1	6.1	6.1
97298 4.0-4.4	native	99A6825-001.002	Ω	5.4	5.4	5.4		5.4	5.4
97298 8.4-8.8	native	99A6825-002.002	_	5.7	5.7	5.7	5.7	5.7	5.7
97698 11.2-11.6	native	99A8275-003.002	Ω	5.2	5.2	5.2		5.2	5.2
97698 13.5-13.9	native	99A8275-004.002	Ω	5.4	5.4	5.4		5.4	5.4
97698 16.3-16.7	native	99A8275-005.002	⊃	5.3	5.3	5.3	5.3	5.3	5.3
97698 18.2-18.8	native	99A8275-008.002	П	5.6	5.6	5.6		5.6	5.6
97698 19.4-19.8	native	99A8275-009.002	Ω	5.7	5.7	5.7	5.7	5.7	5.7
97698 4.6-5.8	native	99A8275-001.002	n	5.3	5.3	5.3			5.3
97698 8.2-8.6	native	99A8275-002.002	n	5.3	5.3	5.3	5.3	5.3	5.3

Sample Interval	Materia	RIN/Event/Bottle	lab_result_ qualifier_ codes	TETRACHLOROETHENE (ug/kg)	TOLUENE (ug/kg)	TOLUENE-D8 (ug/kg)	Total Xylene (ug/kg)	TRANS-1,2- DICHLOROETHENE (ug/kg)	TRANS-1,3- DICHLOROPROPENE (ug/kg)
83.	native	98A2015-001.010		9100	WWW. Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color Color C	180	A CONTRACTOR OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY O		endinanananianininininininininininininini
91198 11.6-11.9	native	98A1091-001.035				CS	philades are at the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the c		личиния политичения иличения перевория положения положения положения положения положения положения положения п
91198 15.5-15.8	native	98A1091-001.036			Vilidia dia matampanya o coccasso co cassoren	06			SALUNISA A A ANTAR EN ENTREPRENENTE DE MANAGEMENT DE MANAGEMENT DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONT
91198 19.1-19.5	native	98A1091-001.037				88	***************************************		VODERANDO DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRAC
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92598 16.0-16.75	-	98A1092-001.036				91		***************************************	**************************************
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|                               | Borehole         | 80888                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               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Material Intervent/Bottle         Coodes         (ug/kg)         (ug/kg)           native         9948275-004.002         E         (ug/kg)         (ug/kg)           native         9948275-003.002         J         (ug/kg)         (ug/kg)           native         9948275-003.002         J         (ug/kg)         (ug/kg)           native         9947799-003.002         J         (ug/kg)         (ug/kg)           native         9947799-003.002         J         (ug/kg)         (ug/kg)           native         9947799-001.002         J         (ug/kg)         (ug/kg)           native         9944102-001.003         J         (ug/kg)         (ug/kg)         (ug/kg)           native         9944102-001.003         J         (ug/kg)	b codes (ug/kg)  E E  J  J  J  J  L  J  L  J  L  J  L  L  L	(ug/kg) (ug	(ug/kg) (ug/kg)	(ug/kg)	(ng/kg)
native 99A8275-004-002 E  native 99A8775-005-002 E  native 99A8775-005-002 J  native 99A7799-003-002 J  native 99A7799-003-002 J  native 99A7799-003-002 J  native 99A87790-001-002 J  native 99A87790-001-002 J  native 99A81700-001-003 J  native 99A81700-001-003 J  native 99A81700-001-002 J  native 99A81700-001-002 J  native 99A8617-002-002 J  native 99A8617-002-002 J  native 99A8617-002-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A8650-003-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A86300-001-002 J  native 99A825-002-002 J  native 99A825-002-002 J  native 99A825-002-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J  native 99A8275-004-002 J		SO C			
native 99A2215-005.002 E		SO C			
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native         99A7799-005 002         J           bedrock         99A7799-006 002         J           native         99A4799-001 002         J           native         99A4102-001 003         J           native         99A4102-001 003         J           native         99A4102-001 003         J           native         99A817-003 002         J           native         99A6817-003 002         J           native         99A6817-002 002         J           native         99A6817-002 002         J           native         99A6850-003 002         J           native         99A6850-003 002         J           native         99A6850-003 002         J           native         99A6850-003 002         J           native         99A6850-002 002         J           native         99A6850-002 002         J           native         99A6850-002 002         J           native         99A6850-002 002         J           native         99A6850-002 003         J           native         99A6850-002 003         J           native         99A6820-002 003         J           native         99A6		96 C			
bedrock         99A7799-006.002         J           native         99A7799-001.002         J           native         99A3210-003.013         J           bedrock         99A4102-001.009         J           pedrock         99A4102-001.013         J           native         99A6817-003.002         J           pedrock         99A6817-003.002         J           native         99A6817-002.002         J           native         99A68517-002.002         J           native         99A6850-003.002         J           native         99A6850-002.002         J           native         99A6850-002.003         J           native         99A6824-001.002         J           native         99A6826-002.003         J           native         99A68262-002.003         J           native <t< td=""><td></td><td>95 C</td><td></td><td></td><td></td></t<>		95 C			
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native         99A3210-003.013         J           native         99A4102-001.009         J           bedrock         99A4102-001.012         J           native         99A4102-001.006         J           native         99A46170-001.013         J           native         99A6817-002.002         J           bedrock         99A6817-003.002         J           native         99A6817-003.002         J           native         99A6817-003.002         J           native         99A66817-003.002         J           native         99A6650-003.002         J           native         99A6650-003.002         J           native         99A6650-004.002         J           native         99A6650-004.002         J           native         99A6650-004.002         J           native         99A6650-003.002         J           native         99A6650-004.002         J           native         99A6650-003.003         J           native         99A6650-003.003         J           native         99A6650-003.003         J           native         99A66825-003.002         J           native <td< td=""><td></td><td>95 C</td><td></td><td></td><td></td></td<>		95 C			
native         99A4102-001.009         J           bedrock         99A4102-001.012         J           native         99A4102-001.003         J           native         99A4102-001.005         J           native         99A6817-003.002         J           bedrock         99A6817-006.002         J           native         99A6817-006.002         J           native         99A6817-006.002         J           native         99A6817-006.002         J           native         99A650-003.002         J           native         99A650-003.002         J           native         99A650-004.002         J           native         99A650-004.002         J           native         99A650-004.002         J           native         99A6650-004.002         J           native         99A6650-003.002         J           native         99A6824-001.002         J           native         99A6824-002.002         J           native         99A6825-003.002         J           native         99A6825-003.002         J           native         99A6825-003.002         J           native         99A6825		95 C			
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Sample			lab_result_ qualifier_	TETRACHLOROETHENE	TOLUENE	TOLUENE-D8	Total Xylene	TRANS-1,2- DICHLOROETHENE	TRANS-1,3- DICHLOROPROPENE
Borehole Interval	Material		codes	(ng/kg)	(ng/kg)	(ng/kg)	(ng/kg)	(ug/kg)	(ng/kg)
91198 11.6-11.9	native		В						
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97298 16.4-17.0	native		JB						
97298 17.7-18.2	bedrock		JB						
97698 19.4-19.8	native		JB						
90998 3.8-4.0	native		<b>-</b>					790	790
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91198 7.7-8.0	native		n	089				089	089
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92598 16.0-16.75	bedrock		Ω	720				720	720
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Sample Interval	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	TETRACHLOROETHENE (ug/kg)	TOLUENE (ug/kg)	TOLUENE-D8 (ug/kg)	Total Xylene (ug/kg)	TRANS-1,2- DICHLOROETHENE (ug/kg)	TRANS-1,3- DICHLOROPROPENE (ug/kg)
95998 8.4-8.8	native	99A7799-002.002	D	5.2	5.2				
96098 12.5-13.0	native	99A3210-002.015	Ŋ	00/	700			200	700
96098 16.0-16.2	bedrock	99A3210-002.016	n	002	7007			700	700
96098 4.5-4.8	native	99A3210-002.013	n	730	730			730	730
96098 8.5-8.8	native	99A3210-002.014	Ŋ	069	069			069	069
96198 12.0-12.5	native	99A3210-003.015	Ω	092	760			760	760
96198 15.8-16.2	bedrock	99A3210-003.016	n	. 700	700	0.000		200	. 700
96198 4.4-4.7	native	99A3210-003.013	n	200	700		Š	2007	700
96198 8.1-8.5	native	99A3210-003.014	n	920	670			670	9.79
96298 12.25-12.75 native	native	99A3210-004.016	n	092	750	Control Communication and Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Cont	9	750	75(
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96298 4.3-4.7	native	99A3210-004.013	)	700	700			2007	700
96298 8.0-9.0	native	99A3210-004.014	n	0.29	670		÷	029	029
96398 12.4-12.7	native	99A4102-001.009	n	710	710			710	710
96398 16.2-16.4	bedrock	99A4102-001.012	D	730	730			730	730
96398 4.3-4.8	native	99A4102-001.003	Ω	700	700			700	700
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Total Xylene (ug/kg)			977777777777777777777777777777777777777			SALA ALAMAN MANAGAMAN AND AND AND AND AND AND AND AND AND A																					
TOLUENE-D8 (ug/kg)			***************************************							**************************************																	
TOLUENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	4225707070707070707000000000000000000000	TITLE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE	WWW.	650	740	670	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7		5.3
TETRACHLOROETHENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	950	740	670	002	200	. 650	5.3	5.4		5.4	Little a reservation of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second se						5.3	
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RIN/Event/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	native
Sample	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	36896	3696	3696	36696	36696	92098	9208	92098	36026	97198	97198	97198	97198	97198	97198	97298	97298	97298	97298	97298	36926	36926	36926	36926	36926	36926	36926

ole	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	TRANS-1,3- DICHLOROPROPYLENE (ug/kg)	TRICHLOROETHENE (ug/kg)	TRICHLOROFLUORO METHANE (ug/kg)	TRICHLOROTRIFLUO ROETHANE (ug/kg)	VINYL CHLORIDE (ug/kg)	XYLENE (TOTAL)	XYLENES (TOTAL) (ug/kg)
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91198 11.6-11.9 native		98A1091-001.035								- Annihamman de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction de construction d
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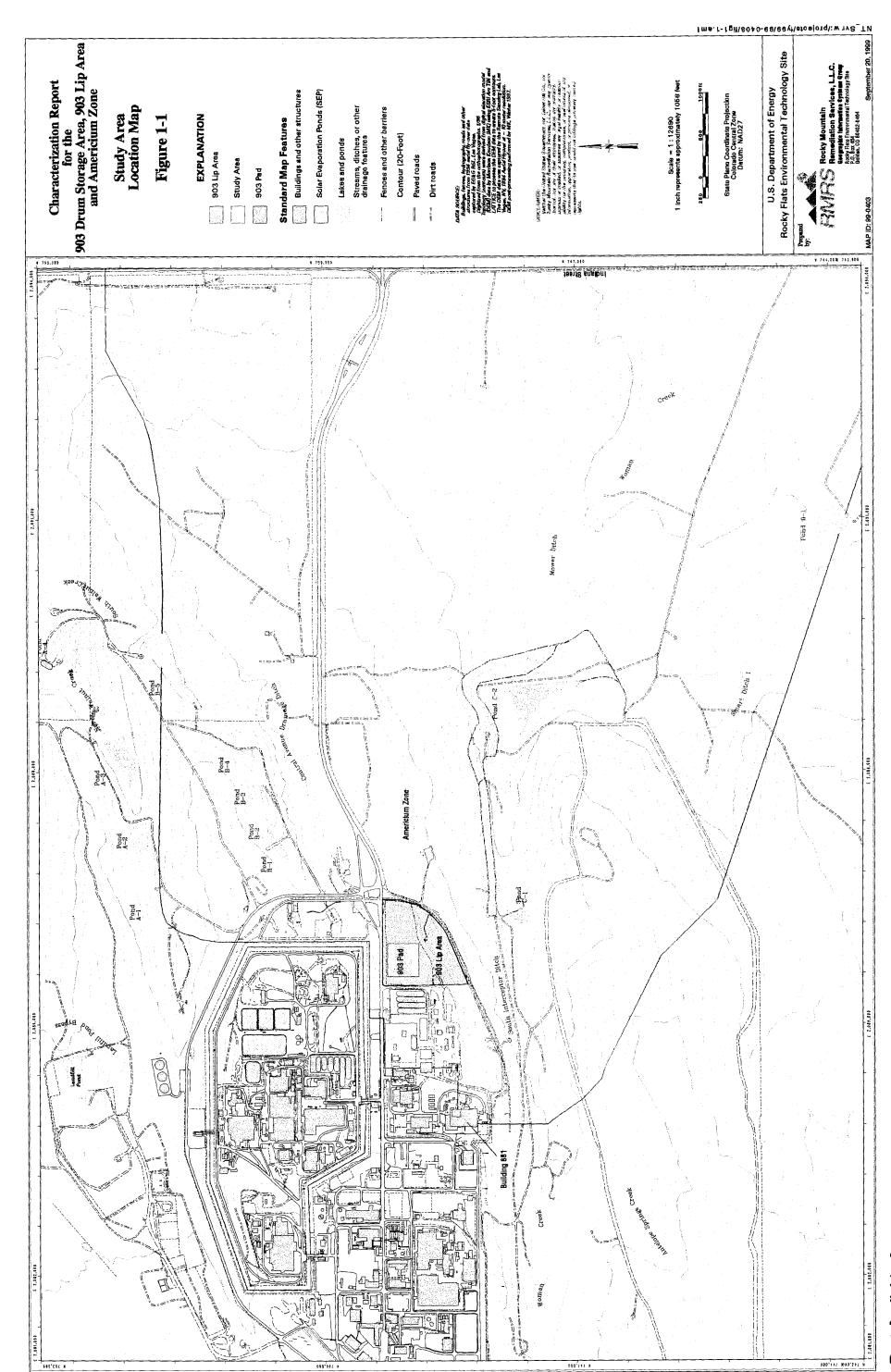
Sample Borehole Interval	Material	RIN/Event/Bottle	lab_result_ qualifier_ codes	TRANS-1,3- DICHLOROPROPYLENE (ug/kg)	TRICHLOROETHENE (ug/kg)	TRICHLOROFLUORO METHANE (ug/kg)	TRICHLOROTRIFLUO ROETHANE (ug/kg)	VINYL CHLORIDE (ug/kg)	XYLENE XYLENES (TOTAL) (19/kg)	KYLENES (TOTAL) (ug/kg)
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TRANS-1,3- DICHLOROPROPYLENE (ug/kg)				**************************************										adjunction and the commencer of the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer and the commencer 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Material	native	native	native	native	native	bedrock	bedrock	native	native	native	native	native	native	native	native	native	bedrock	native	native	native	bedrock	native	native	bedrock	native	bedrock	native	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native
Sample Interval	91198 11.6-11.9	91198 15.5-15.8	3.1-3.4	7.7-8.0	92598 12.0-12.5	92598 16.0-16.75	96598 22.3-22.7	96698 12.4-12.8	4.2-4.6	3.2-8.6	96798 12.5-12.9	96798 16.0-16.4	96798 20.4-20.8	1.4-4.8	3.4-8.8	96898 12.3-12.6	96898 17.1-17.4	4.4-4.7			96998 17.2-17.8	4.4-4.8	8.4-8.8	97098 16.5-17.0	97298 16.4-17.0	97298 17.7-18.2		6		91198 19.1-19.5	91198 19.5-19.8	3.1-3.4	7.7-8.0	1	92598 16.0-16.75	3.5-4.0	7.5-8.0	95998 12.4-12.8	95998 14.8-15.2	95998 17.7-18.2	95998 24.6-25.0	5.0-5.6
Borehole	91198	91198	91198 3.1-3.4	91198 7.7-8.0	92298	92298	96598	96998	96698 4.2-4.6	96698 8.2-8.6	86798	96798	. 96798	96798 4.4-4.8	96798 8.4-8.8	96898	96898	96898 4.4-4.7	96898 8.4-8.7	96998	96698	96998 4.4-4.8	96998 8.4-8.8	96026	97298	97298	9/698 19.4-19	91198	91198	91198	91198	91198 3.1-3.4	91198 7.7-8.0	92298	92298	92598 3.5-4.0	92598 7.5-8.0	95998	92998	92998	95998	95998 5.0-5.6

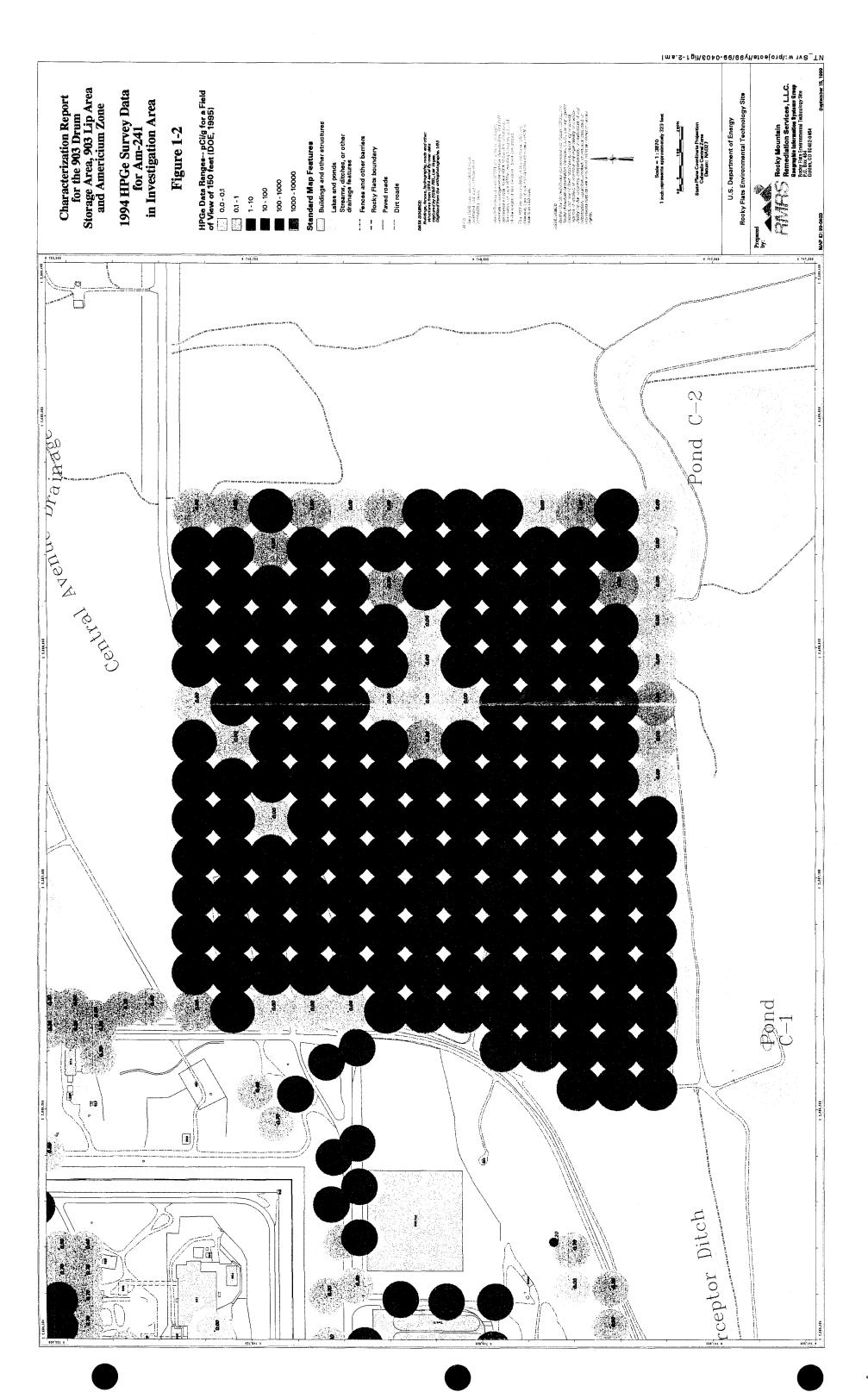
XYLENES (TOTAL) (ug/kg)	5.2		and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s	WC-thromeone and an an an an an an an an an an an an an							***************************************	700000000000000000000000000000000000000	777777777777777777777777777777777777777									***************************************	7 7	t. (9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
XYLENE ) (TOTAL) (ug/kg)	~~~~	700	700	730	069	760	700	700	670	750	720	700	670	710	730	700	710	1300	1300	1300	1500	1500	0061		**************************************	***************************************																
	5.2	700	700	730	069	760	700.	700	670	750	720	700	670	710	730	700	710	1300	1300	1300	1500	1500	2000	ŗΘ	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	5.7	5.6	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
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TRICHLOROFLUORO METHANE (ug/kg)	5.2	700	700	730	069	760	200	700	670	750	720	700	670	710	730	700	710			***************************************		***************************************	A 2	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4	6.4	2.7	9.9	6.2	7.2	7.4	5.3	6.3	6.4	5.3	5.2
TRICHLOROETHENE (ug/kg)	5.2	700	700	730	069	760	700	200	670	750	720	700	929	710	730	700	710	1300	1300	1300	1500	1500	P 5	9	5.3	6.2	5.7	5.3	5.9	5.6	5.4		5.7	5.6	6.2	7.2		5.3	6.3	6.4	5.3	5.2
TRANS-1,3- DICHLOROPROPYLENE (ug/kg)	5.2					- St. Sp. of t. S. S. S. S. S. S. S. S. S. S. S. S. 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lab_result_ qualifier_ codes		n	<b>⊃</b>	)	n	ח	n		n		⊃	⊃	⊃	<b>D</b>	n	D.	n	n	n	<b>o</b> :	n i	o :=	> =	n	n	n	Ω	_	n	<b>-</b>	n	<b>-</b>	n	n	ر ر	n	n	D	D	D	D.	n
RIN/Event/Bottle	99A7799-002.002	99A3210-002.015	99A3210-002.016	99A3210-002.013	99A3210-002.014	99A3210-003.015	99A3210-003.016	99A3210-003.013	99A3210-003.014	99A3210-004.016	99A3210-004.017	99A3210-004.013	99A3210-004.014	99A4102-001.009	99A4102-001.012	99A4102-001.003	99A4102-001.006	99A3210-001.015	99A3210-001.016	99A3210-001.017	99A3210-001.018	99A3210-001.013	9946817-003 002	99A6817-004.002	99A6817-005.002	99A6817-006.002	99A6817-001.002	99A6817-002.002	99A6649-003.002	99A7930-001.002	99A7930-002.002	99A7930-003.002	99A6649-001.002	99A6649-002.002	99A6650-003.002	99A6650-004.002	99A6650-005.002	99A6650-001.002	99A6650-002.002	99A6307-003.002	99A6307-004.002	99A6307-001.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	bedrock	native	bedrock	native							
Sample Borehole Interval	95998 8.4-8.8	96098 12.5-13.0	96098 16.0-16.2	96098 4.5-4.8	96098 8.5-8.8	96198 12.0-12.5	96198 15.8-16.2	96198 4.4-4.7	96198 8.1-8.5	35	96298 16.1-16.5			7	4.						ري.	96498 4.8-5.2	_			96598 22.3-22.7					96698 20.2-20.6	96698 22.4-22.8					ω.		96798 8.4-8.8	96898 12.3-12.6	96898 17.1-17.4	96898 4.4-4.7

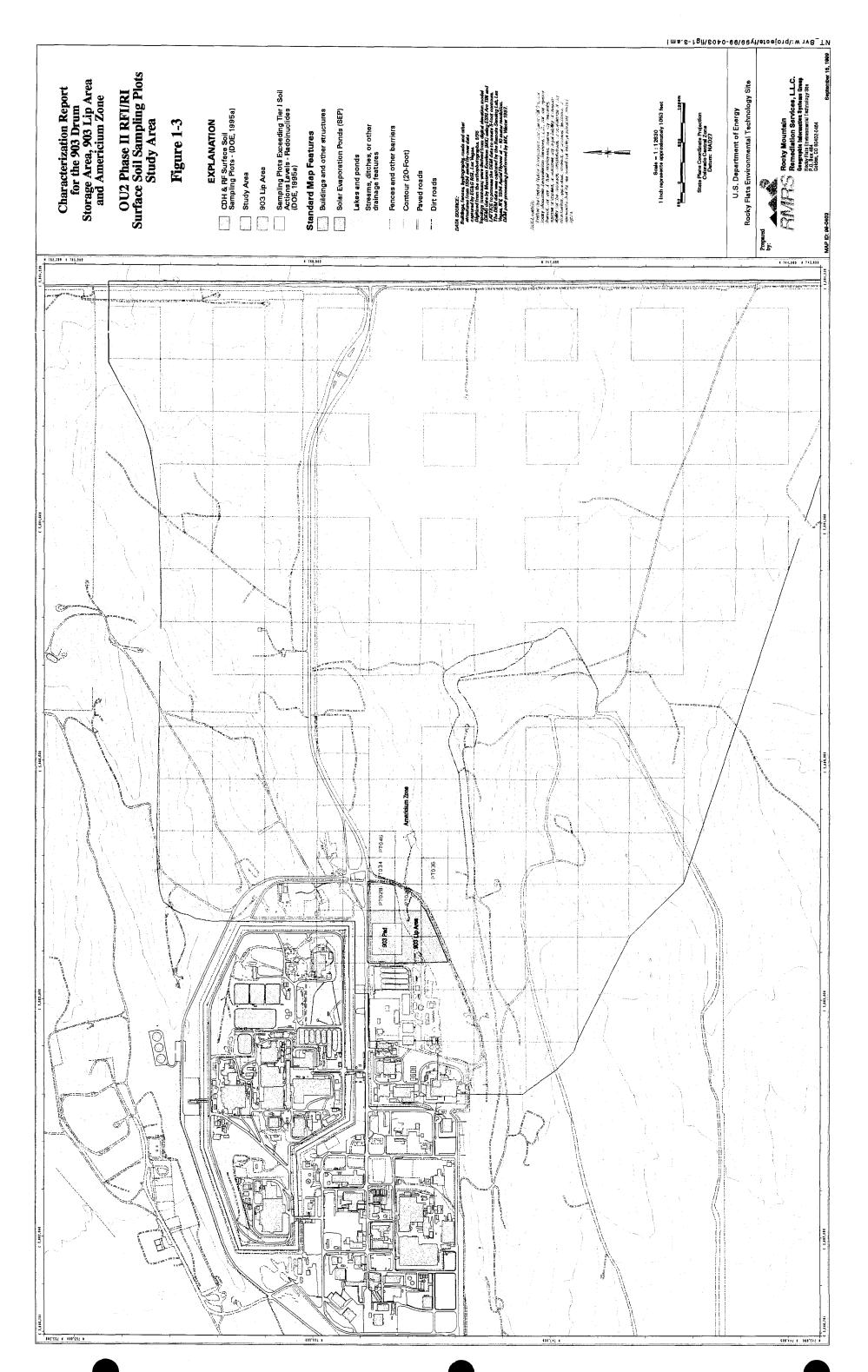
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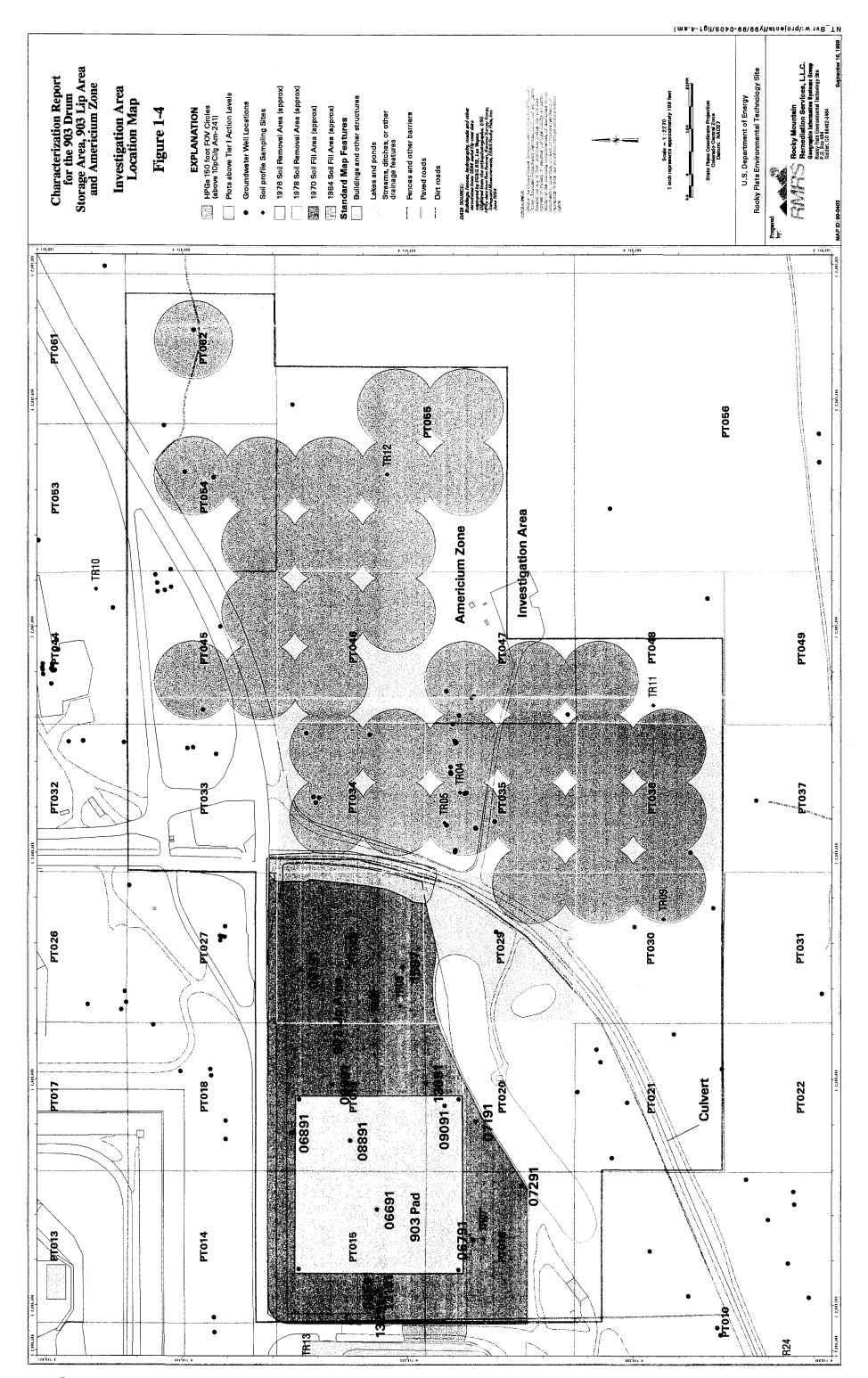
XYLENES (TOTAL) (ug/kg)	5.2	5.6	2.7	5.3	5.2	5.1	.5.7	5.5	5.8		-	AT				5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
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XYLENE (TOTAL) (ug/kg)			0.000								000000000000000000000000000000000000000				TORONO CONTRACTOR											2000	
VINYL CHLORIDE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	670	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
TRICHLOROTRIFLUO ROETHANE (ug/kg)	5.2	11.5	11.5	5.3	5.2	5.1	5.7	1	5.8	Commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission of the commission 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TRICHLOROFLUORO METHANE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	650	740	920	700	700	650	5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
TRICHLOROETHENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	. 5.7	5.5	5.8	920	740	670	2007	700Z	650	5.3	5.4	6.1	5.4	5.7	5.2	in description of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second o	5.3	5.6	12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-1 12 mm-	5.3	5.3
TRANS-1,3- DICHLOROPROPYLENE (ug/kg)	5.2	5.6	5.7	5.3	5.2	5.1	5.7	5.5	5.8	TO DESCRIPTION OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY				1000000 00000000 000000000000000000000		5.3	5.4	6.1	5.4	5.7	5.2	5.4	5.3	5.6	5.7	5.3	5.3
lab_result_ qualifier_ codes	n	n	ח	n	n	n	n	n	n	n	n	n	ם	n	n	n	n	n	n	n	n	n	ח	n	n	n	n
RIN/Event/Bottle	99A6307-002.002	99A6824-003.002	99A6824-004.002	99A6824-001.002	99A6824-002.002	99A6308-003.003	99A6308-004.003	99A6308-001.003	99A6308-002.003	99A4102-002.009	99A4102-002.012	99A4102-002.015	99A4102-002.018	99A4102-002.006	99A4102-002.003	99A6825-003.002	99A6825-004.002	99A6825-005.002	99A6825-001.002	99A6825-002.002	99A8275-003.002	99A8275-004.002	99A8275-005.002	99A8275-008.002	99A8275-009.002	99A8275-001.002	99A8275-002.002
Material	native	native	bedrock	native	native	native	bedrock	native	native	native	native	native	bedrock	native	native	native	native	bedrock	native	native	native	native	native	native	native	native	native
Sample Interval	96898 8.4-8.7	96998 12.4-12.7	96998 17.2-17.8	96998 4.4-4.8	96998 8.4-8.8	97098 12.4-12.6	97098 16.5-17.0	97098 4.2-4.7	97098 8.4-8.8	97198 12.4-12.8	97198 15.5-16.1	97198 20.4-20.8	97198 24.4-24.8	97198 4.4-4.8	97198 7.3-7.6	97298 12.4-12.8	97298 16.4-17.0	97298 17.7-18.2	97298 4.0-4.4	97298 8.4-8.8	97698 11.2-11.6	97698 13.5-13.9	97698 16.3-16.7	97698 18.2-18.8	97698 19.4-19.8	97698 4.6-5.8	97698 8.2-8.6
Borehole	36896	36696	36696	36696	36696	97098	35026	97098	97098	97198	97198	97198	97198	97198	97198	97298	97298	97298	97298	97298	97698	97698	97698	97698	36926	97698	97698

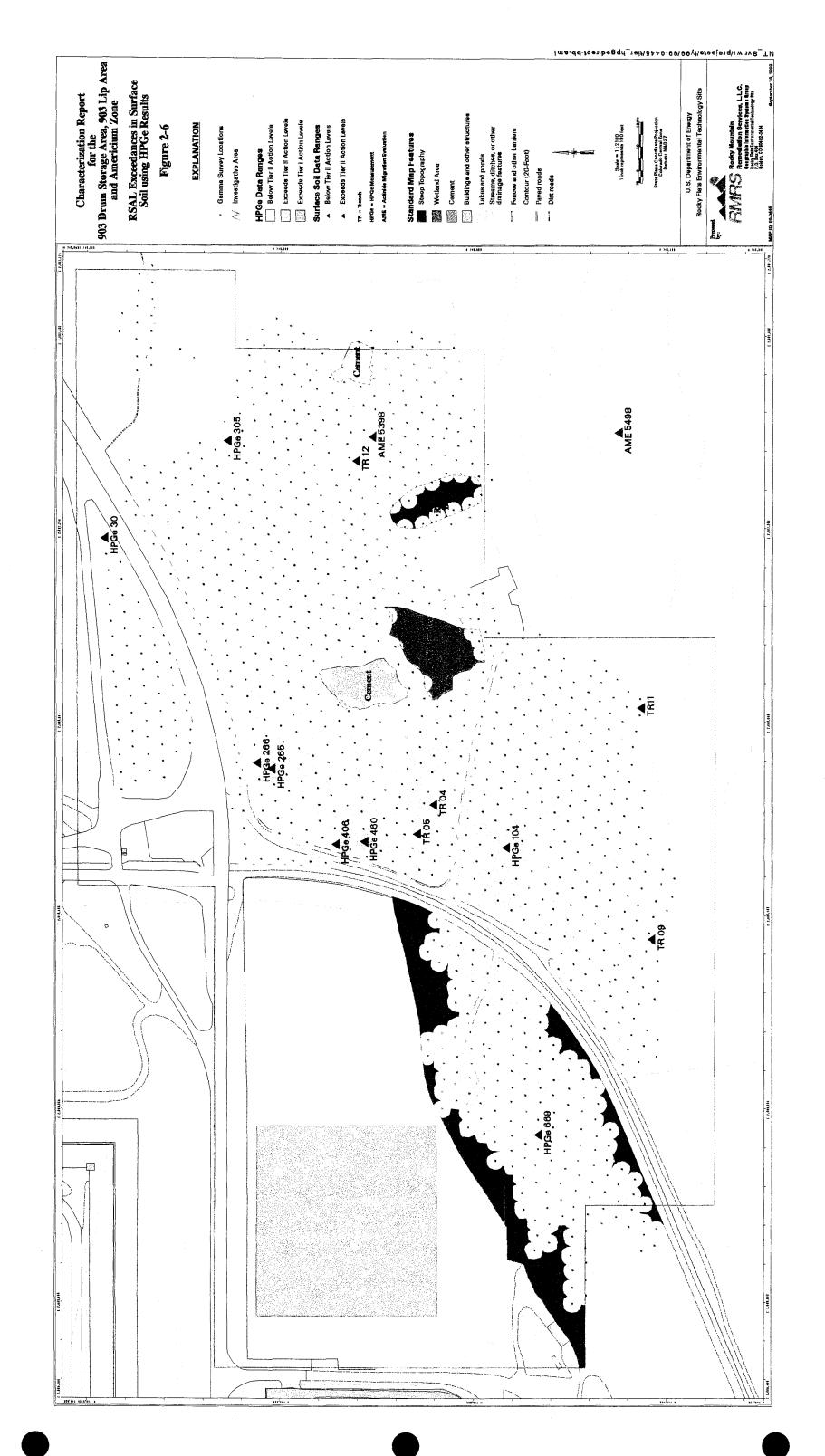


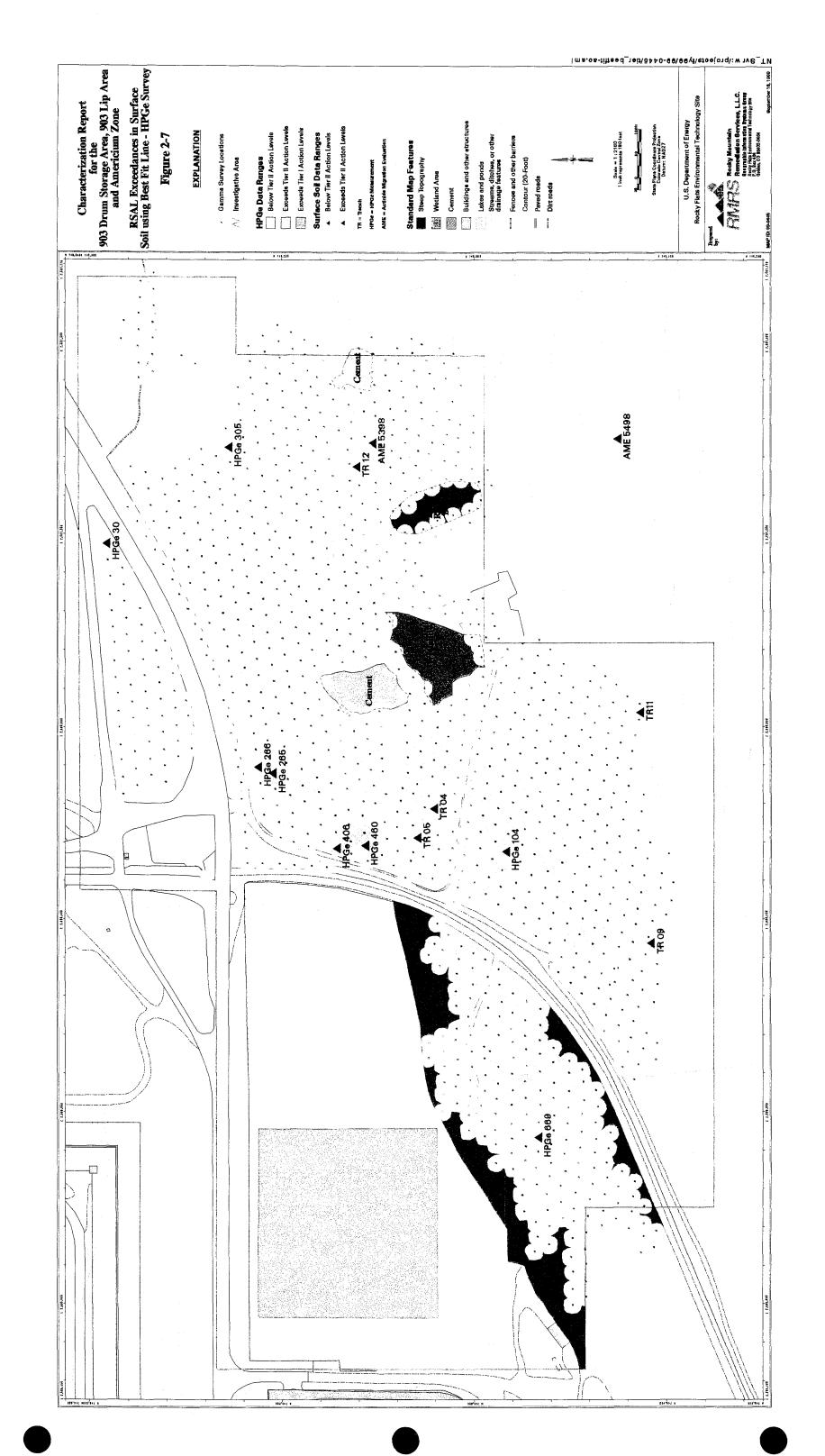
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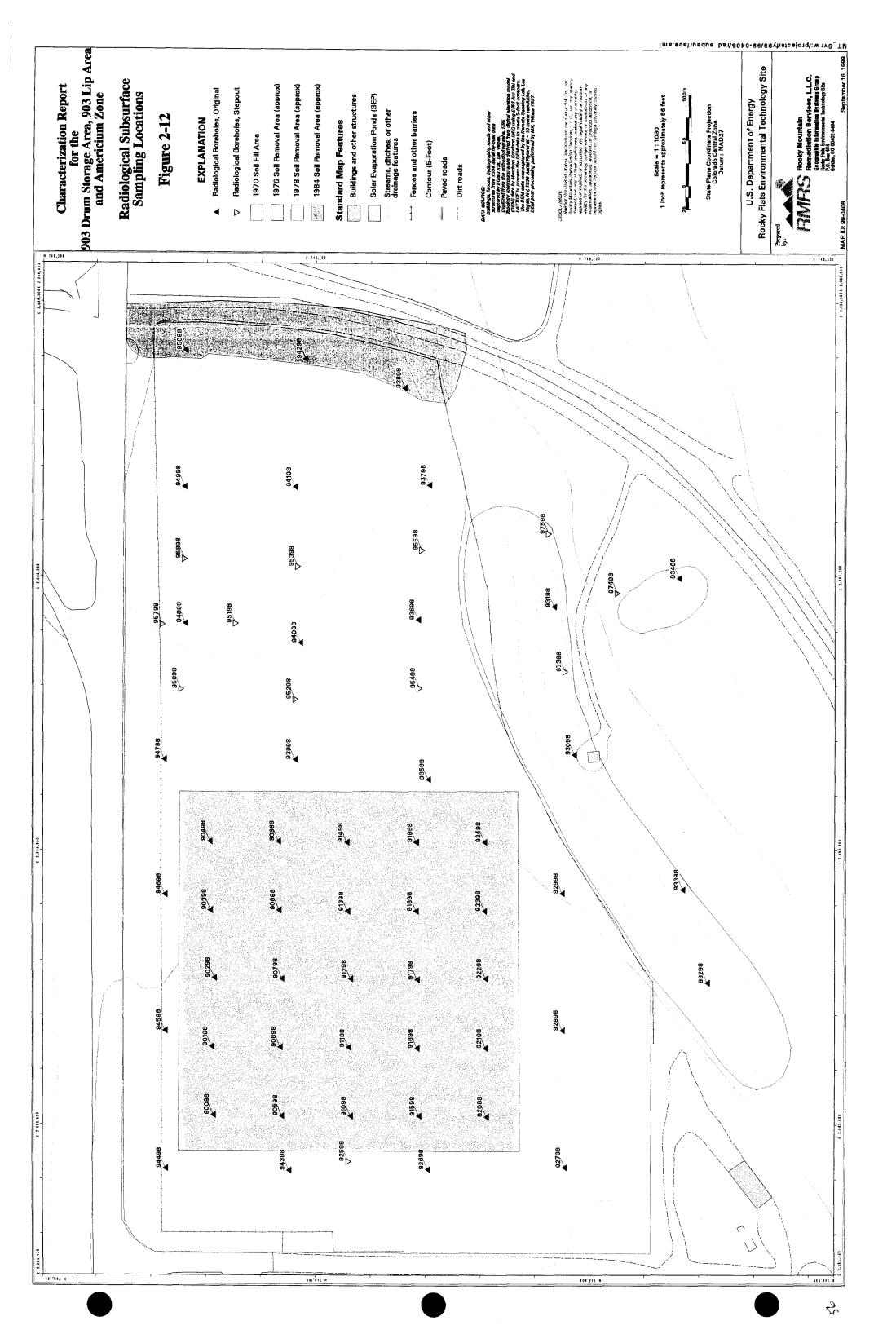


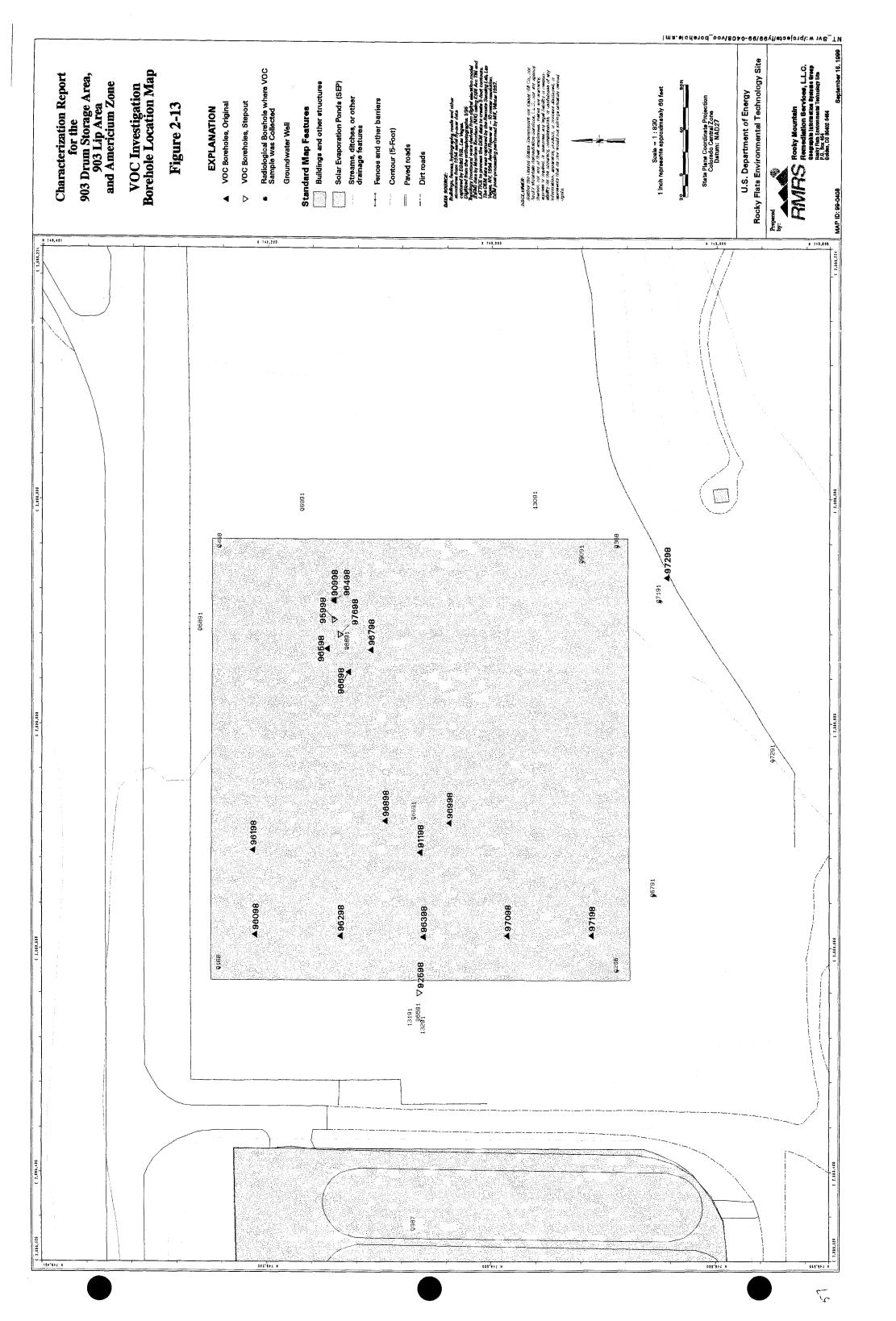




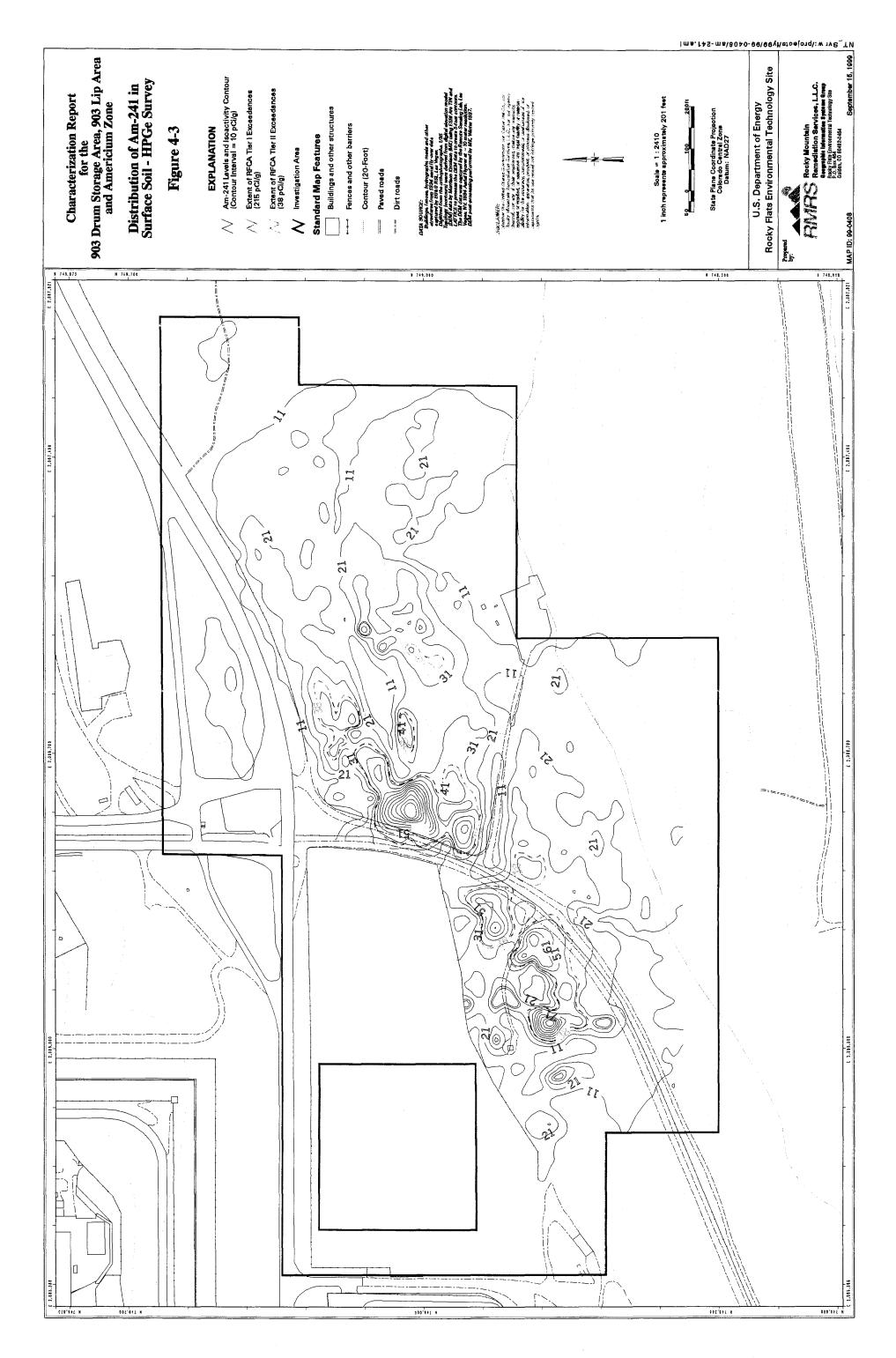


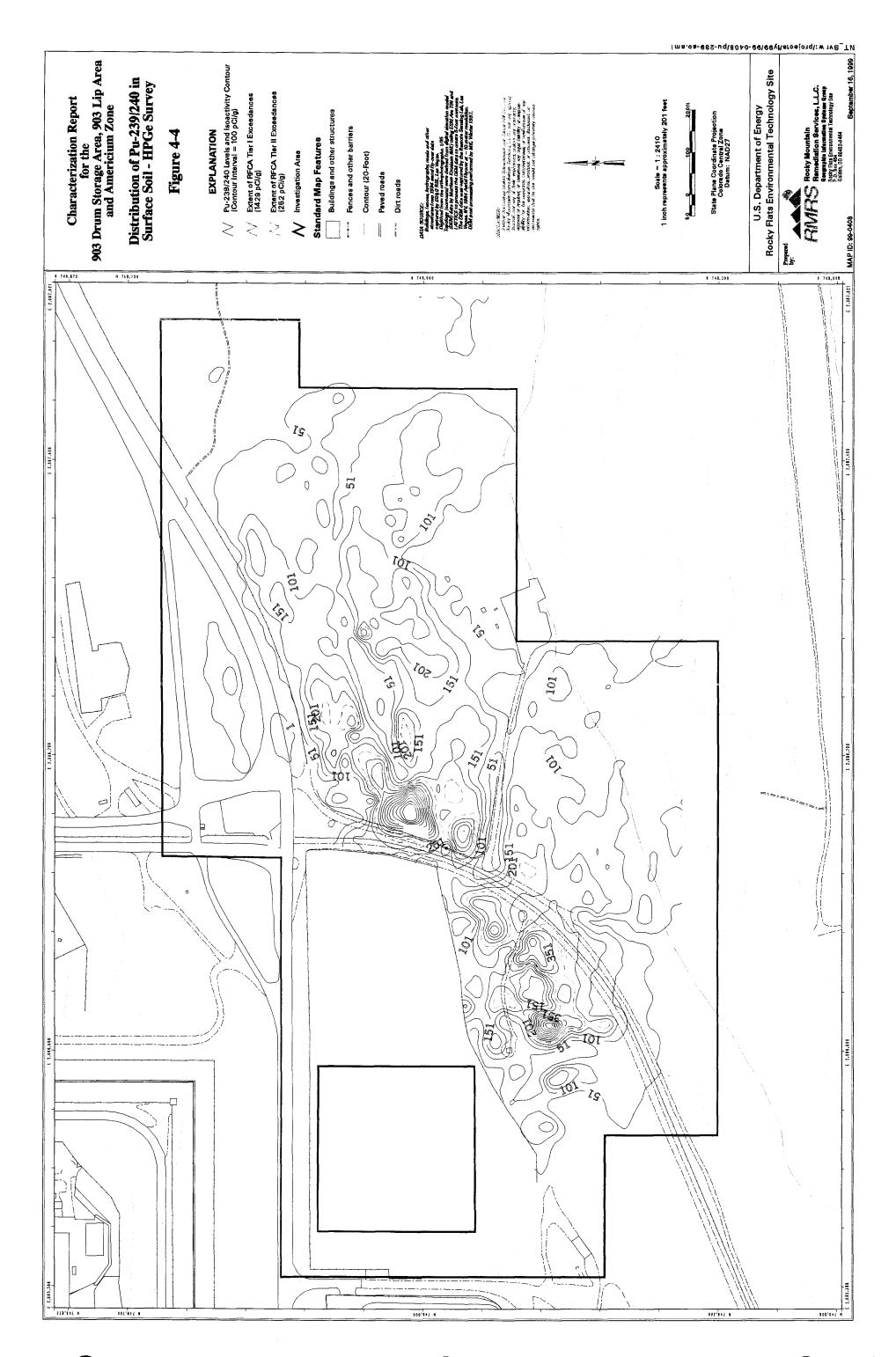


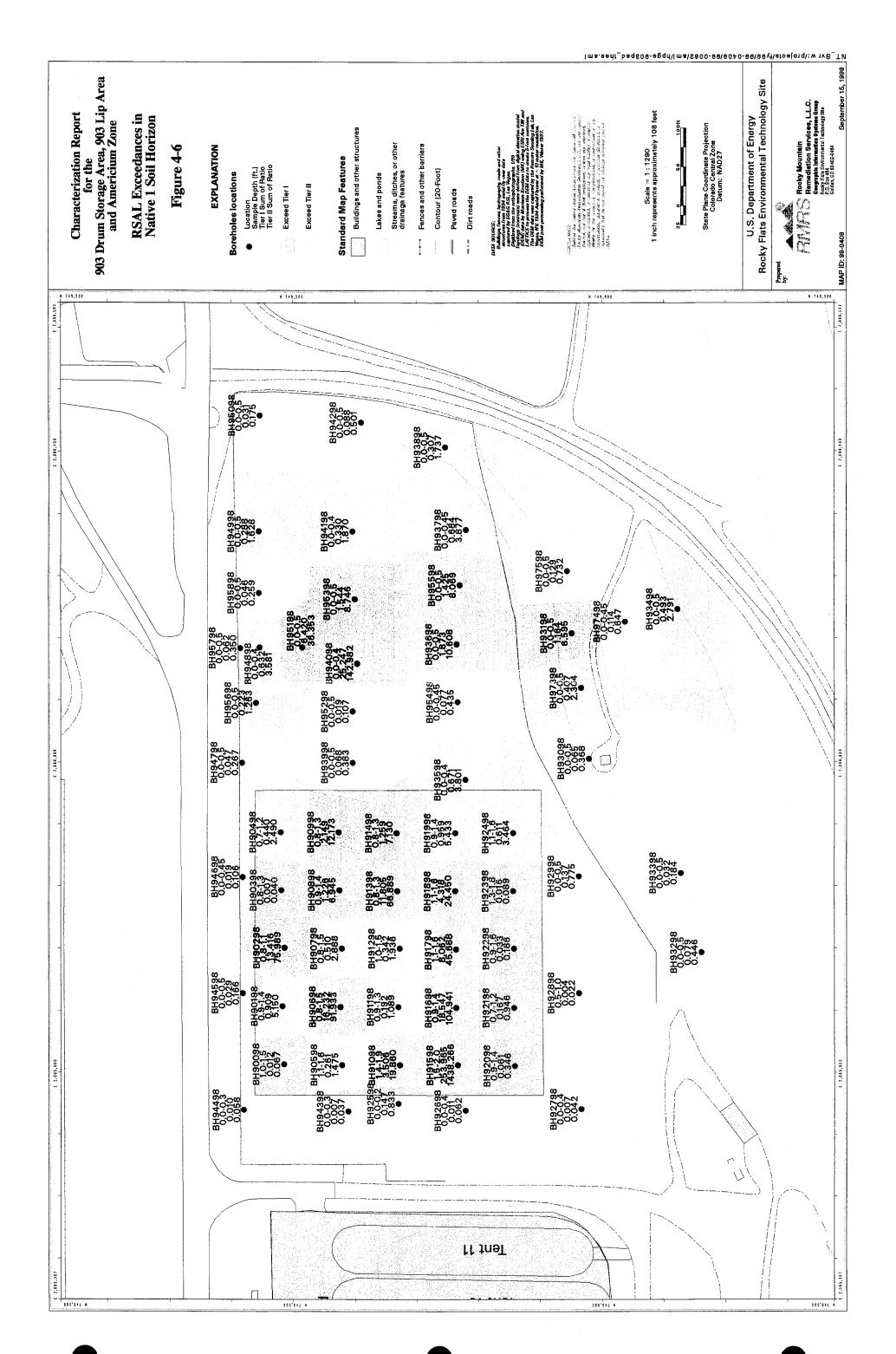


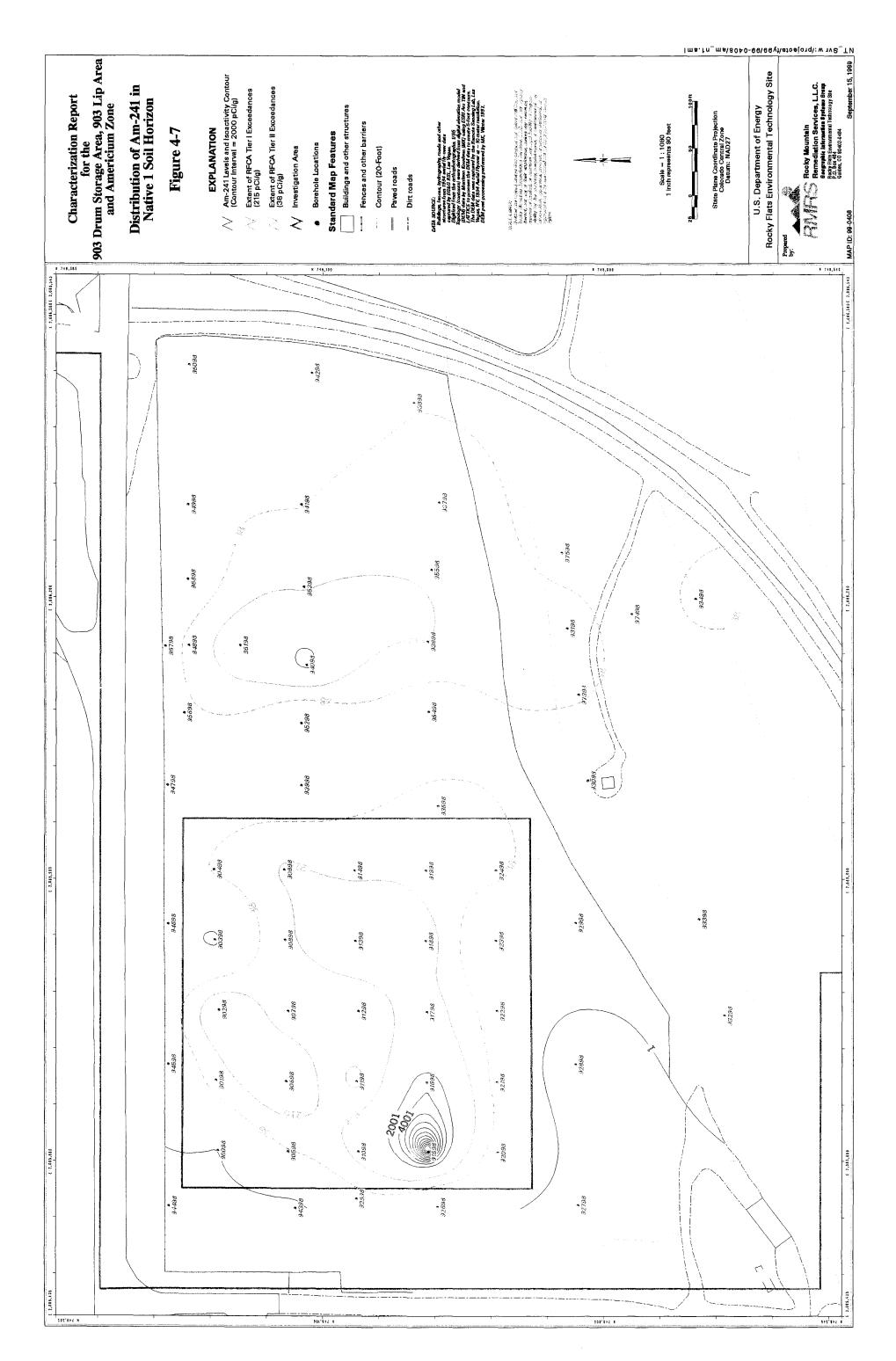


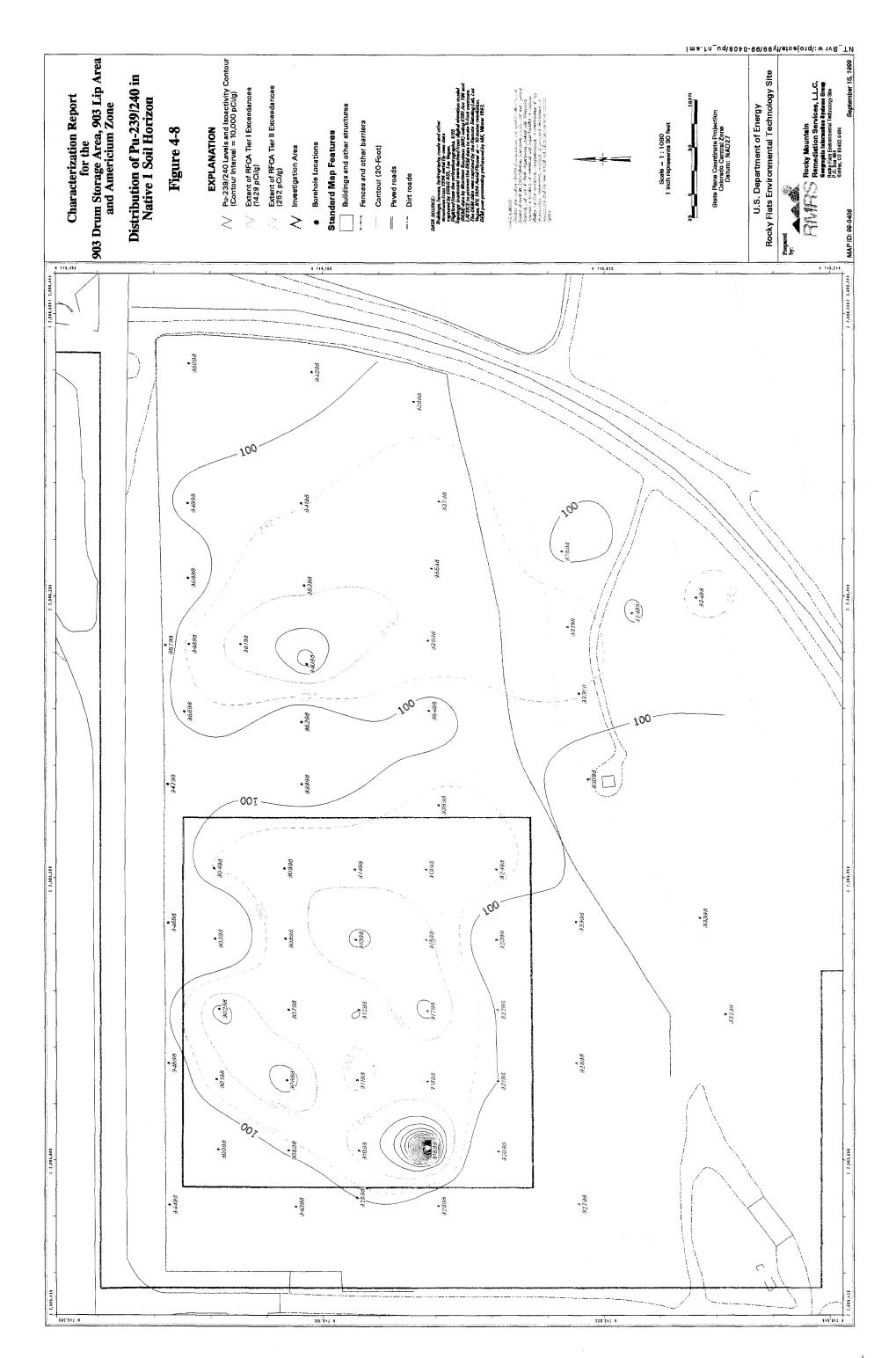


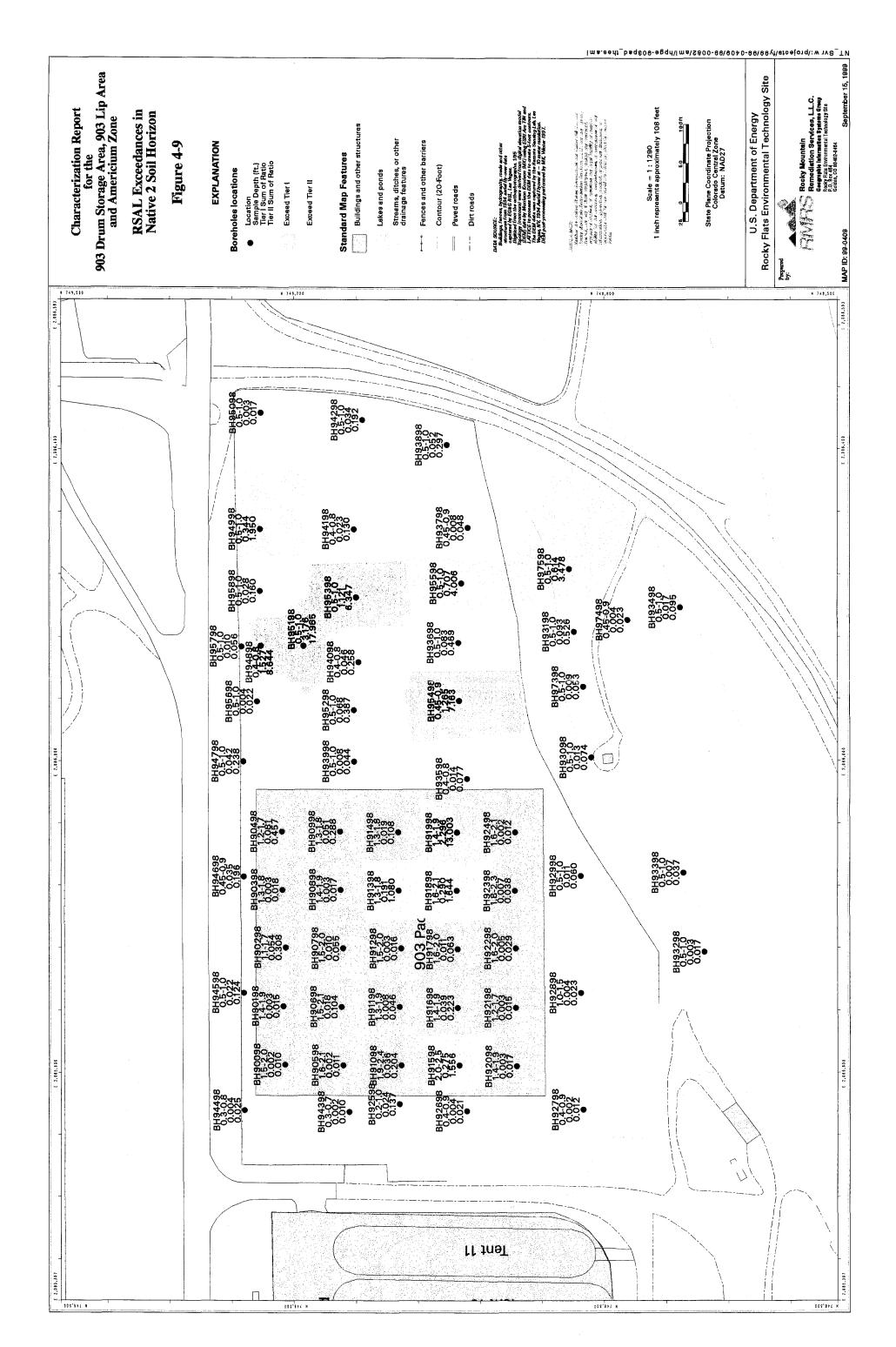






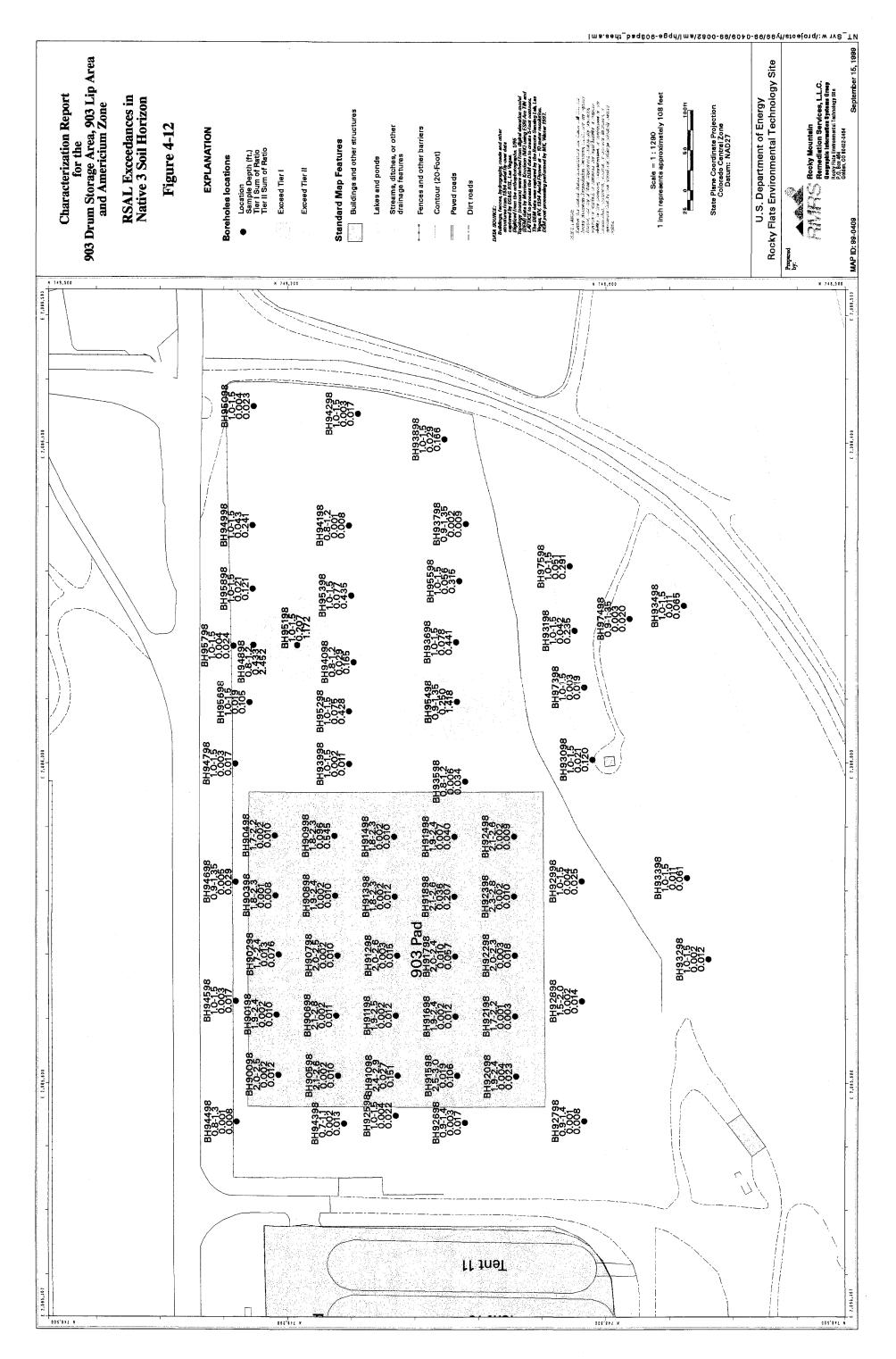


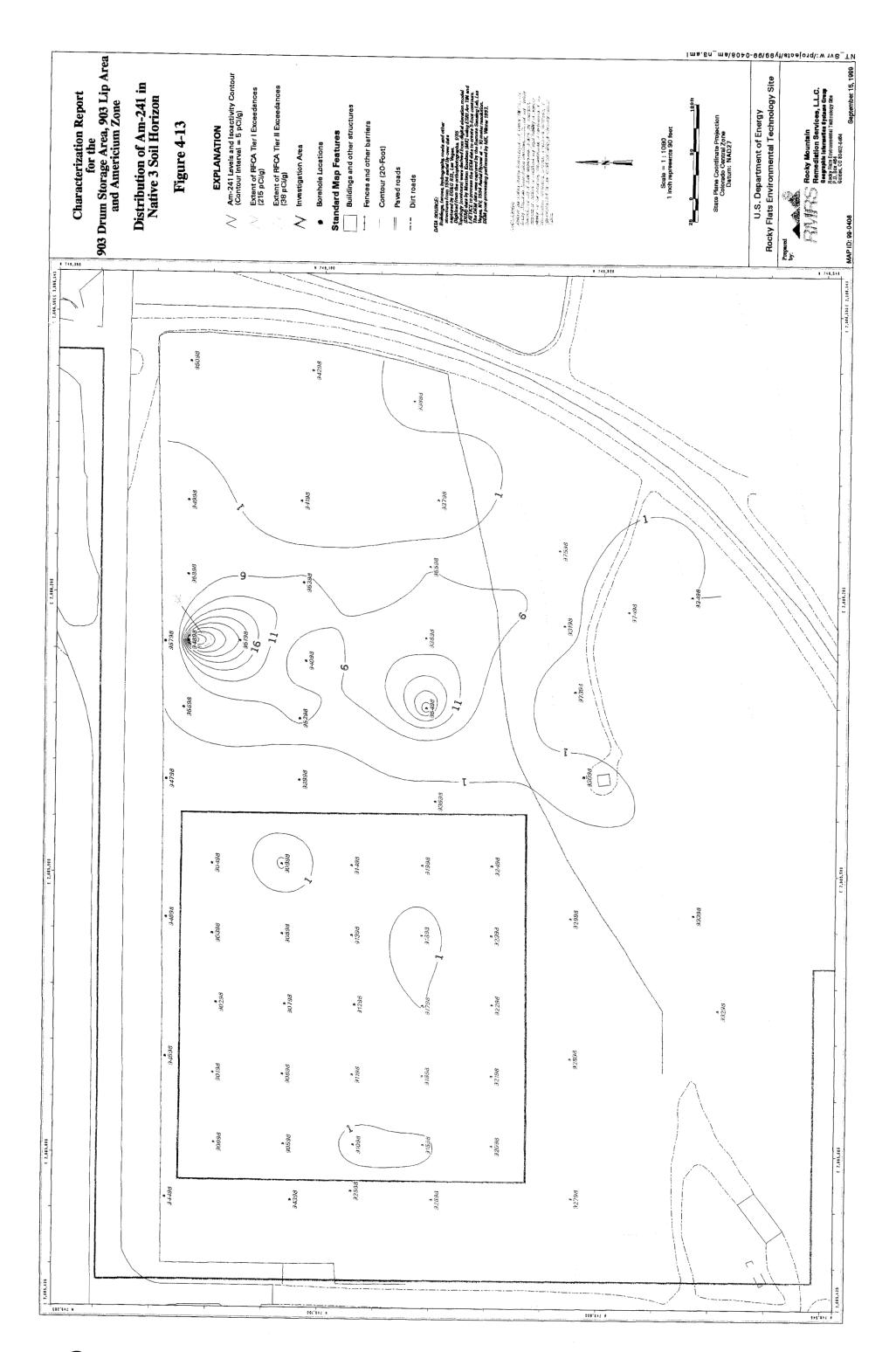


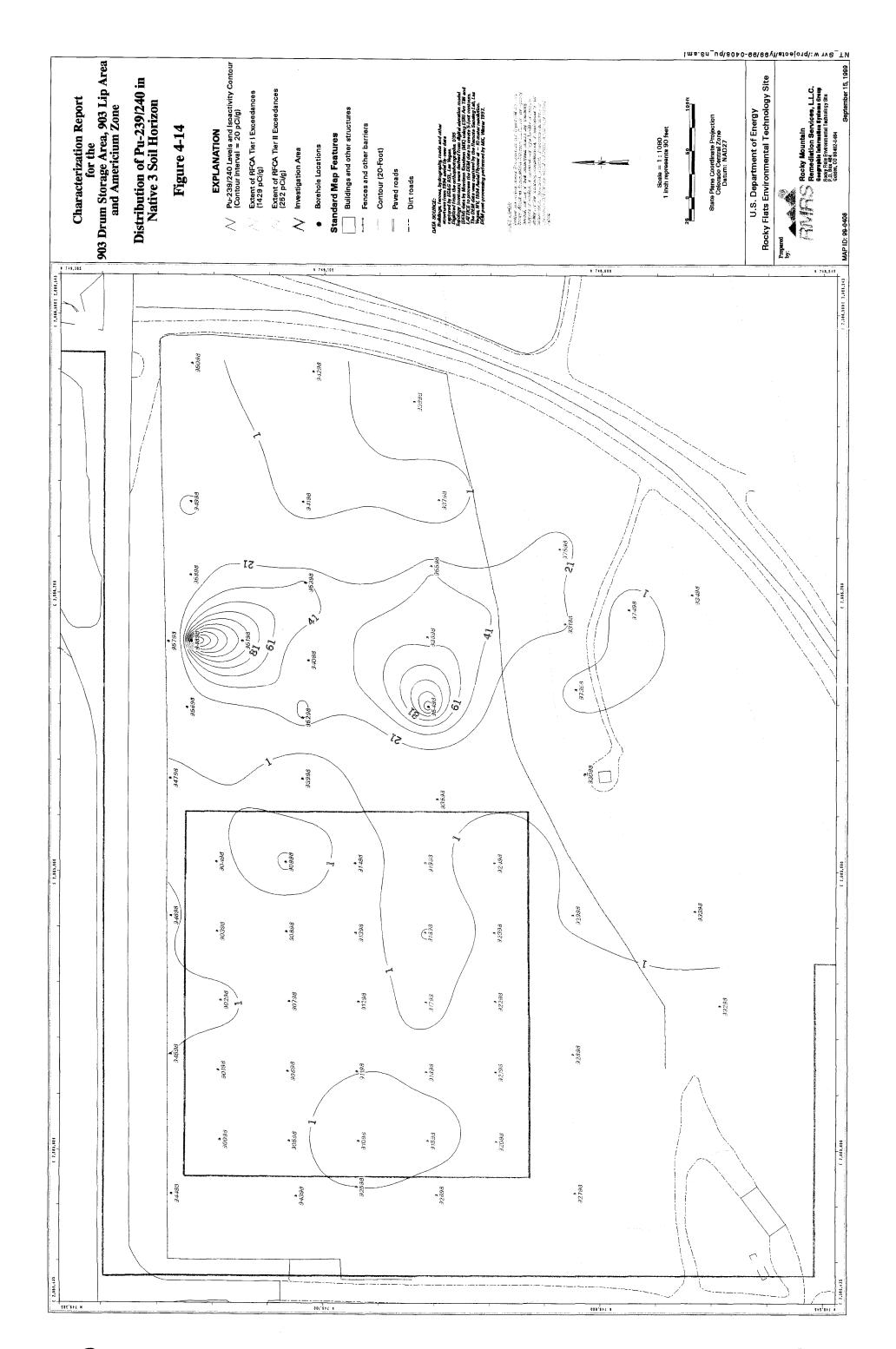


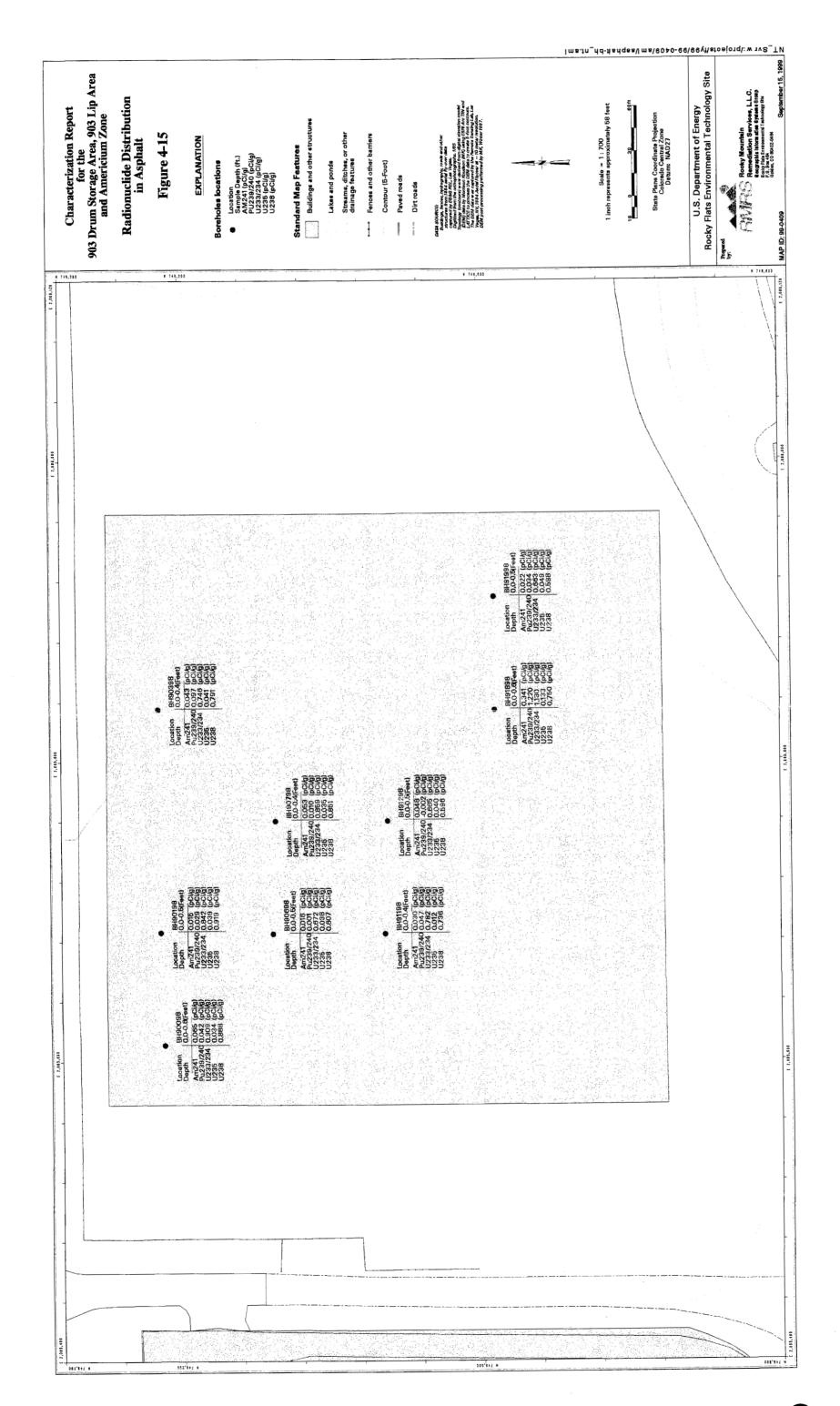


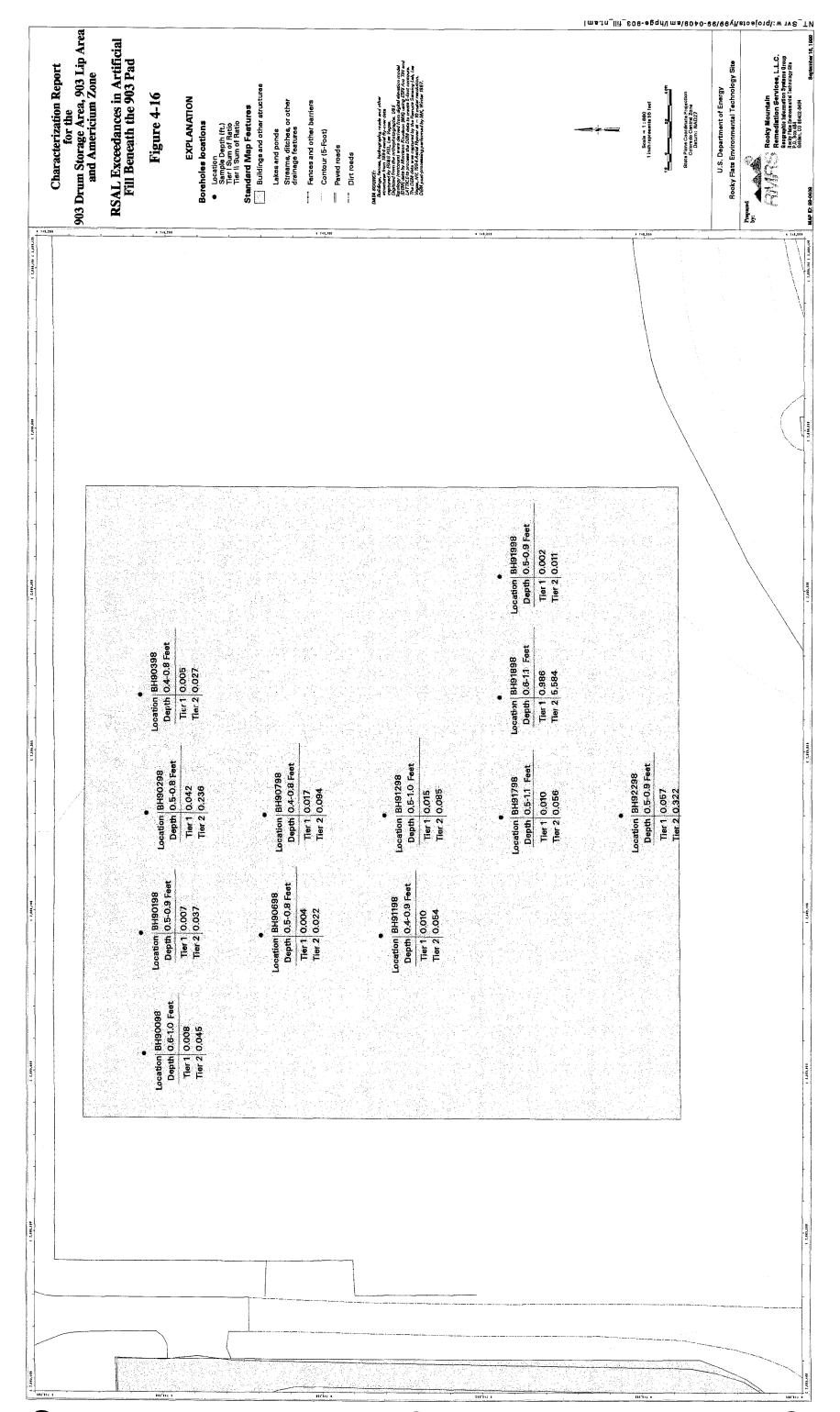


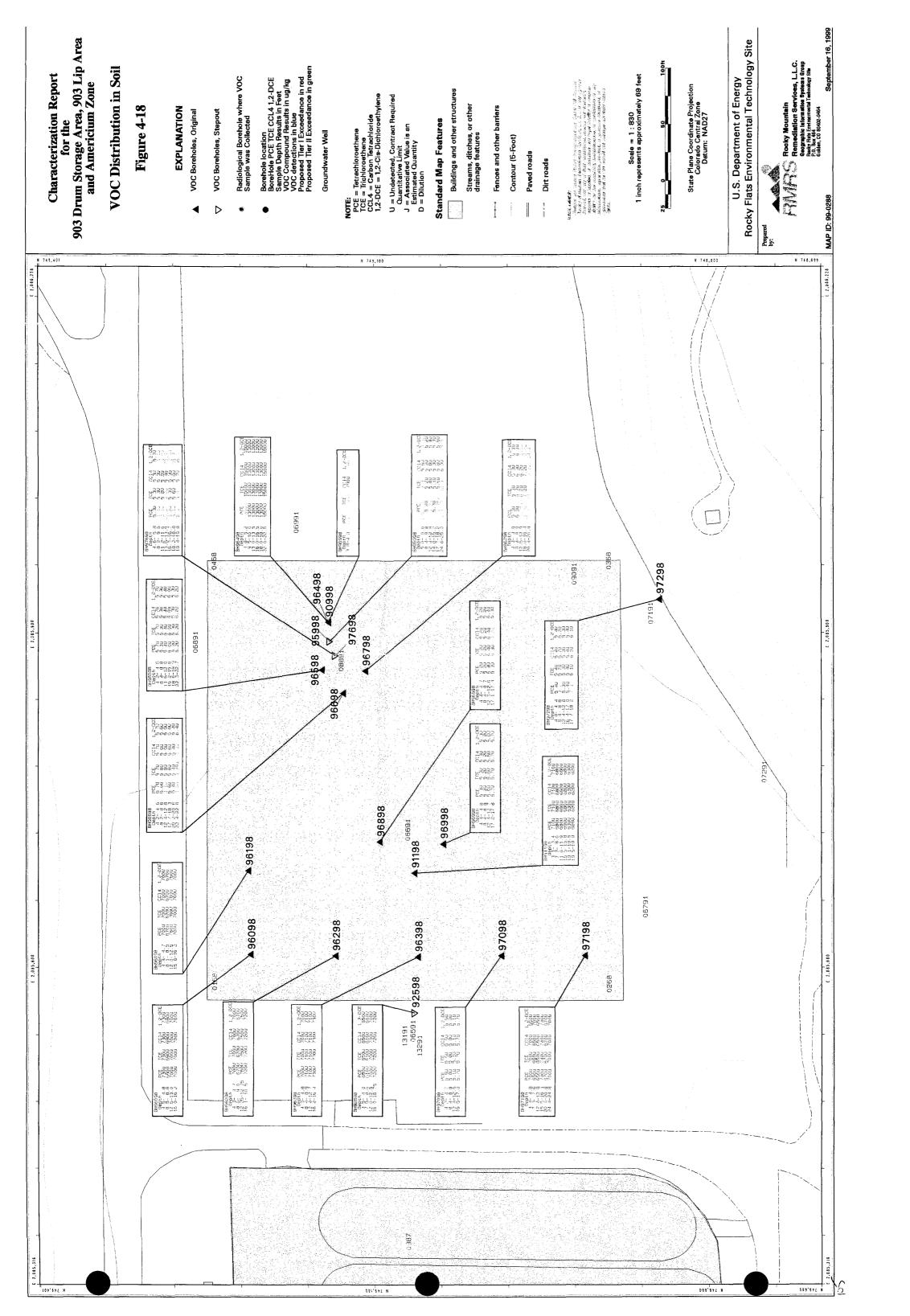




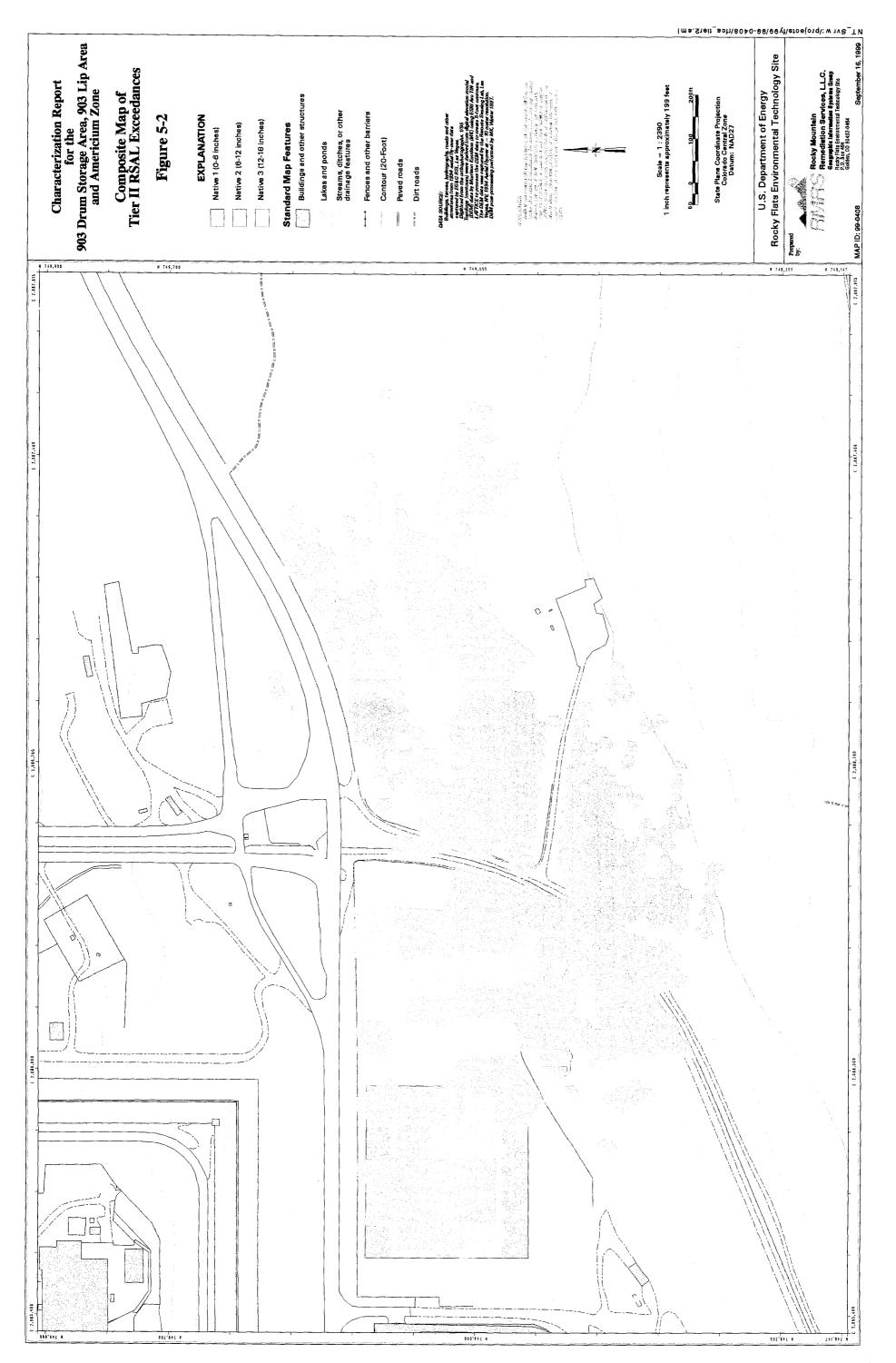


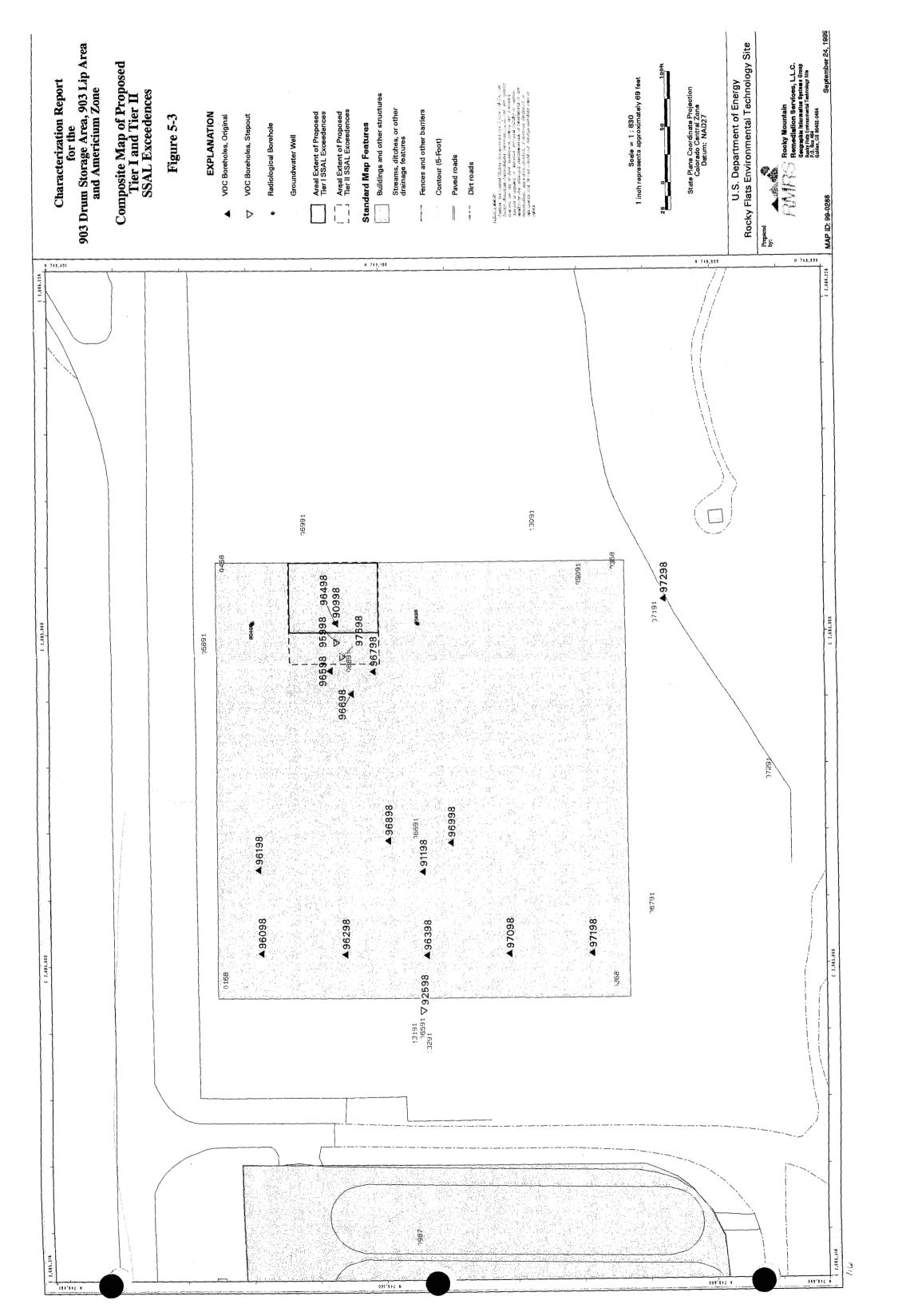














903 Drum Storage Area, 903 Lip Area and Americium Zone Characterization Report for the

407/407

pack

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J-1117-A

**EXPLANATION** 

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3011/ 000

Streams, ditches, or drainage features

Fences and other barriers

State Plane Coordinate Projection Colorado Central Zone Datum: NAD27

U.S. Department of Energy Rocky Flats Environmental Technology Site

Rocky Mountain
Remediation Services, L.L.C.
Geographic Information Systems Group
Rocky Flats Environmental Technology Site
P.O. Box 464
Golden, CO 80402-0464

September 24, 1999

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